

**Derry Side Road Subdivision –
Beckwith, ON Conceptual
Stormwater Management
Report**



Prepared for:
Mr. Steve Smith

Prepared by:
Stantec Consulting Ltd.

September 25, 2017

Revision	Description	Prepared by		Reviewed by	
0	1 st Submission	Ana Paerez	2017/09/15	Kris Kilborn	2017/09/25



Sign-off Sheet

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Prepared by _____

(signature)

Ana M. Paerez, P. Eng.

DERRY SIDE ROAD SUBDIVISION – BECKWITH, ON CONCEPTUAL STORMWATER MANAGEMENT REPORT

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Introduction
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1.0 INTRODUCTION

Stantec Consulting Ltd. was retained by Mr. Steve Smith to complete a conceptual Stormwater Management (SWM) design for a new rural subdivision in the Township of Beckwith in the County of Lanark, Ontario. The site is legally described as part of Lot 20, Concession 4 and is located in the south-west corner of the intersection of Derry Side Road and Ferguson Road.

The proposed development comprises approximately 16.1 ha of land and comprises twenty-four (24) residential lots with average lot sizes of 0.6 ha (1.4 acres) and associated accessing infrastructure as shown on **Drawing SD-1**. The site is delimited to the northwest by Ferguson Road, to the northeast by Derry Side Road, to the east by a stable and to the south by forested land.

1.1 BACKGROUND AND REFERENCES

The following documents/ reports were referenced in the preparation of this conceptual SWM Report:

- *Hydrogeology, Terrain Analysis and Impact Assessment Report, Derry Side Road, Township of Beckwith, Ontario, exp Services Inc., June 22, 2017*
- *Preliminary Geotechnical Investigation Report, Proposed Residential Subdivision Part of Lot 20, Concession 4 Township of Beckwith, Ontario, exp Services Inc., July 21, 2017*
- *City of Ottawa Sewer Design Guidelines and Technical Bulletin Amendments, 1st Ed., City of Ottawa, November 2004 amended January 31st, 2012 and September 6, 2016*
- *Stormwater Management Planning and Design Manual, MOE (Ontario), March 2003*

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Stormwater Management Criteria and Objectives
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2.0 STORMWATER MANAGEMENT CRITERIA AND OBJECTIVES

This conceptual stormwater management (SWM) plan is submitted in support of an application for Draft Plan Approval for the subdivision. This conceptual SWM plan will identify the measures that will be implemented to meet the SWM criteria for the site.

2.1 CONCEPTUAL SWM CRITERIA

The stormwater management criteria for the site are based on the recommendations discussed during the pre-application meeting with County, Township and Rideau Valley Conservation Authority (RVCA) staff in combination with City of Ottawa Sewer Design Guidelines and Ministry of the Environment Stormwater Management Planning and Design Manual. The SWM criteria are summarized as follows:

- Post to pre-development (site in its current form) quantity control for the 2, 5 and 100-year design storms
- Provide adequate emergency overflow conveyance off-site
- Provide “Enhanced” water quality protection (80% TSS removal), as per MOE guidelines (2003)
- Storm drainage to be provided through roadside ditches, side-yard and rear-yard drainage swales
- Proposed under side of footing (USF) elevations be set above road side ditch inverts with foundation drains connected to the road side ditches and equipped with sump pumps and backwater valves
- Proposed culvert along the Leach municipal drain to be sized to convey the 100-year design storm
- Road crossing culverts to have a minimum diameter of 600 mm and to be sized to convey the 10-year design storm
- Driveway crossing culverts to have a minimum diameter of 400 mm and to be sized to convey the 5-year design storm

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Existing Conditions
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3.0 EXISTING CONDITIONS

The 16.1 ha site is relatively flat, slightly sloping towards the Leach Municipal Drain that traverses the centre of the property and borders the north-west property line (see **Drawing EX-1**). The drain conveys runoff from external rural areas west of the site as well as site areas towards an existing 800 mm diameter culvert crossing Derry Side Road. The drain is part of the King's Creek, Jock River watershed system.

The site is primarily dense woodland with the exception of an agricultural field located in the northern portion of the site.

The Geotechnical Investigation prepared for the development (exp, July 2017) found that the soil conditions encountered at the test hole locations consist of a topsoil layer underlain by silty sand (0.3 m to 0.8 m), followed by a layer of glacial till (1.0 m to 5.1 m deep). Refusal to augering/casing was met in all the boreholes at 1.0 m to 5.1 m depth on inferred bedrock.

Groundwater levels were measured during exp's geotechnical investigation in three (3) test pits and were found to range from 0.2 m to 1.9 m below ground surface.

3.1 TARGET PEAK OUTFLOWS

Drawing EX-1 shows the existing conditions drainage plan. A conceptual hydrologic modeling exercise was completed with SWMHYMO to generate pre-development and post development runoff response from the site area for storm events up to the 100-year storm. The NASHYD command was used to generate hydrographs from the total site area under existing conditions. Runoff from external areas will be conveyed through grassed swales to the Leach municipal drain (see **Drawing SD-1**) and as such, these areas have not been included in the existing condition hydrologic model.

The 3-hr Chicago and 12-hr SCS Type II distributions derived from City of Ottawa IDF parameters were used to generate runoff from the site area. The following assumptions were applied to the hydrologic model:

- Surficial soils within the subject site are defined as silty sand over glacial till based on the geotechnical investigation and were assumed to be within Hydrologic Soil Group C
- The SCS Method was used to calculate CN* values for the site area based on existing land use and available soil information (see **Appendix A1**)
- Land use across the site was obtained from aerial photographs which show dense woodland for most of the site, with the exception of the northern corner of the site that consists of agricultural crops

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- Time to peak (T_p) was calculated based on the relationship of $T_p = 0.67 \times T_c$ where T_c is the time of concentration. The time of concentration of each catchment was calculated using the Uplands Method (see **Appendix A1**)
- Initial abstraction equal to 4.67mm as per City of Ottawa guidelines
- Two (2) linear reservoirs

Table 3.1 shows the 100-year target peak outflows from the proposed site into the drain as obtained from the existing condition SWMHYMO model (see modeling files in **Appendix A2**).

Table 3.1 – Site Area Target Peak Outflows to Leach Municipal Drain

Site Peak Flows (m^3/s)			Site Peak Flows (m^3/s)		
12 hr SCS Type II Storm Distributions			3 hr Chicago Storm Distributions		
100-year	5-year	2-year	100-year	5-year	2-year
0.915	0.369	0.216	0.756	0.289	0.159

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Conceptual Stormwater Management Plan
September 25, 2017

4.0 CONCEPTUAL STORMWATER MANAGEMENT PLAN

The proposed Derry Road Subdivision consists of twenty-four (24) residential lots, two SWM easements, and associated access roads with rural cross section (see **Drawings SD-1 & GP-1**). The conceptual stormwater management (SWM) plan has been developed to provide “enhanced” quality treatment of runoff from the proposed site (80% TSS removal), and to restrict post development peak flows to pre-development levels up to the 100-year design storm as identified in **Table 3.1**.

4.1 CONCEPTUAL SWM STRATEGY

Under post development conditions, storm runoff from the site will be conveyed to the existing watercourse as follows:

- On-site storage for quantity control of runoff will be provided in two (2) separate linear dry detention areas, SWM-1 and SWM-2, controlled via pond outlet structures prior to discharging into the Leach municipal drain.
- Runoff from areas A1 and A2 will be directed to an oil/grit separator (OGS-1) through road side ditches and a ditch inlet catchbasin (DICB) to be treated to achieve 80% TSS removal. The OGS-1 unit will discharge into the storage area SWM-1.
- Quantity control for runoff from areas A1 and A2 will be provided in the proposed storage easement area SWM-1. Post development runoff from these areas will be conveyed through road side ditches to a DICB where runoff will pond and eventually spill into the drainage easement SWM-1.
- Runoff from areas A3, A4 and A5 will be directed to an oil/grit separator (OGS-2) through road side ditches and a ditch inlet catchbasin to be treated to achieve 80% TSS removal. The OGS-2 unit will discharge into the storage area SWM-2.
- Quantity control for runoff from areas A3, A4, and A5 will be provided in the proposed storage easement area SWM-2. Post development runoff from these areas will be conveyed through road side ditches to a DICB where runoff will pond and eventually spill into the drainage easement SWM-2.
- Areas UNC-1, UNC-2, UNC-3 and UNC-4 are expected to sheet drain uncontrolled towards the drain and the Ferguson Road and Derry Side Road roadside ditch. Runoff from these areas will be included in the overall peak flow calculations and storage requirement estimates.
- Runoff from external areas will be directed to the drain through grassed swales.

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Conceptual Stormwater Management Plan
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- Road side ditches will be set above the groundwater elevation.
- The culvert crossing at the proposed Street 1 and the Leach Municipal Drain will be sized during detailed design to convey the 100-year peak flows in the drain once the engineers report is revised.

4.2 CONCEPTUAL SITE HYDROLOGY

Rain runoff response from the proposed site was generated using the SWMHYMO hydrologic modeling software. The proposed site was subdivided in several sub-catchments based on whether they sheet drain towards the proposed SWM easements, or they sheet drain off site uncontrolled (see **Drawing SD-1**).

The NASHYD command was used to generate hydrographs from the subcatchments with total imperviousness values less than 20%, otherwise, the STANDHYD command was used (see detailed calculations in **Appendix B1**). Post development SWMHYMO input and output files have been provided in **Appendix B2**.

4.2.1 Water Quantity Control

The COMPUTE VOLUME command was used to estimate the volume required in the SWM storage areas to restrict the post development 100-year peak flows from the site to pre-development levels.

The outlet structure for each the SWM easements, pond configuration and required sizes for culverts an outlet pipes will be finalized during the detailed design stage. **Table 4.1** shows the results of the hydraulic analysis for the proposed storm drainage system.

Table 4.1: 100 Year Post Development Condition Release Rates

Storm Distribution	Uncontrolled Runoff (m ³ /s)	SWM-1 (Pond Bottom = 131.10m)		SWM-2 (Pond Bottom = 131.00m)		Total Discharge to the Drain (m ³ /s)	Allowable Release Rate (m ³ /s)
		SWM Pond Volume Required (m ³)	SWM Pond Discharge (m ³ /s)	SWM Pond Volume Required (m ³)	SWM Pond Discharge (m ³ /s)		
3-hr Chicago	0.465	480	0.145	1,047	0.145	0.756	0.756
12-hr SCS	0.545	494	0.185	1,106	0.185	0.915	0.915

The above table shows that quantity control can be provided through surface storage in the proposed dry ponds to meet the 100-year allowable release rates.

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4.3 WATER QUALITY CONTROL

4.3.1 Lot Level and Conveyance Control

The following lot level and conveyance best management practices will be implemented to promote infiltration and filter sediment.

- Roof leaders will be directed to grass surfaces.
- Road side ditches will be vegetated and constructed with minimum longitudinal slope where possible.

Quality control will be required for developed areas A1 to A5. Runoff from these areas will be conveyed through roadside ditches and directed to two separate ditch inlet catchbasins (DICBs) connected to oil/grit separator units that will be sized to provide 80% TSS removal prior to discharge to the Leach municipal drain. Preliminary sizing for the proposed OGS units is provided in **Appendix C**.

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Conclusions and Recommendations
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5.0 CONCLUSIONS AND RECOMMENDATIONS

Based on the preceding discussion, the following conclusions can be drawn:

- The proposed SWM storage areas SWM-1 and SWM-2 will provide sufficient storage to meet pre-development peak flows from site areas
- "Enhanced" water quality treatment will be provided through two OGS units that will be discharge into the SWM storage areas
- Runoff from external areas will be directed to the Leach municipal drain through grassed swales
- The proposed roadside ditches will be set above the groundwater table

Based on the findings of the report, the following recommendations are provided:

- Proposed under side of footing (USF) elevations be set above road side ditch inverts with foundation drains connected to the road side ditches and equipped with sump pumps and backwater valves
- The conceptual stormwater management plan be revised during the detailed design stage
- An erosion and sediment control plan be provided during the detailed design stage
- The engineers report for the Leach municipal drain be revised as a result of land use change in the catchment area
- The proposed road crossing culvert along the Leach Municipal Drain be sized during the detailed design stage to convey the 100-year storm event

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Appendix A Existing Conditions
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Appendix A EXISTING CONDITIONS

A.1 Existing Condition Parameters

A.2 Existing Condition SWMHYMO Modeling Files

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Appendix A Existing Conditions
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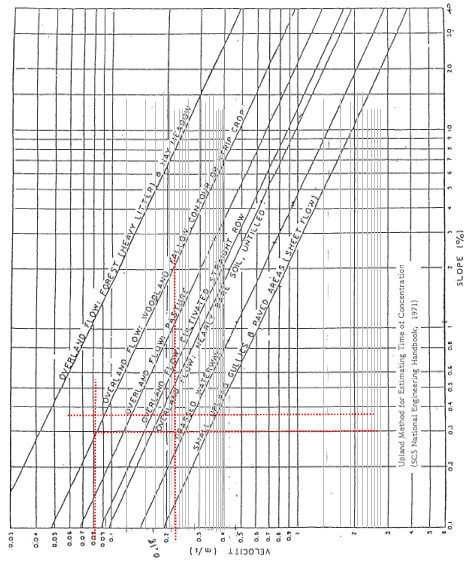
A.1 EXISTING CONDITION PARAMETERS

Model Catchment ID	Description	Area (ha)	Gradient (%)		XIMP (%)		Length (m)		Velocity (m/s)		Infiltration Method	CN	CN	Ia Per. (mm)	Ia Imp. (mm)	HYD Method
			Overland	Ditch	Overland	Ditch	Overland	Ditch	Overland	Ditch						
EX-1	Site Area (Overland/Woodland)	7.83	1.2%	-	0.0%	0.0%	368.0	0.0	0.18	-	SCS	75	76.6	4.67	1.57	NASHVD
EX-2	Site Area (Overland/Woodland)	8.32	0.4%	0.50%	0.0%	0.0%	230.0	137.0	0.10	0.32	SCS	75	76.5	4.67	1.57	NASHVD
Total Area		16.15														

Woodlot	Land Use Area (ha)					
	gravel	lawns	crop	fallow	pasture	meadow/residence
7.83	0.00	0.00	0.00	0.00	0.00	0.00
6.88	0.00	0.00	1.44	0.00	0.00	0.00

1) Standard City of Ottawa Data for Initial Abstraction Parameters, Tp determination, and Infiltration (CN) values

Uplands Method Velocity Determination



160401279: Derry Side Road Subdivision
 NRCS (SCS) Curve Number Determination
 Existing Drainage Areas

Site Soils: (as per exp [Geotechnical Investigation, July 21, 2017](#))

Soil Type

Hydrologic Soil Group

Silty sand with some gravel

C

TABLE OF CURVE NUMBERS (CN's)									
Land Use	Hydrologic Soil Type							Manning's 'n'	Source
	A	AB	B	BC	C	CD	D		
Meadow "Good"	30	44	58	64.5	71	74.5	78	0.40	MTO
Woodlot "Fair"	36	48	60	66.5	73	76	79	0.40	MTO
Gravel	76	80.5	85	87	89	90	91	0.30	City
Lawns "Good"	39	50	61	67.5	74	77	80	0.25	City
Pasture/Range	58	61.5	65	70.5	76	78.5	81	0.17	MTO
Crop	66	70	74	78	82	84	86	0.13	MTO
Fallow (Bare)	77	82	86	89	91	93	94	0.05	MTO
Low Density Residences	57	64.5	72	76.5	81	83.5	86	0.25	Chin
Streets, paved	98	98	98	98	98	98	98	0.01	City

1. MTO Drainage Manual (1997), Design Chart 1.09-Soil/Land Use Curve Numbers
2. Chin (2000), Water-Resources Engineering, Table 6.13-Curve Numbers for Various Urban Land Uses
3. City of Ottawa Sewer Design Guidelines (2012), Table 5.9 CN Values for Various Soil Groups

HYDROLOGIC SOIL TYPE (%) - External Areas							
Catchment	Hydrologic Soil Type						TOTAL
	A	AB	B	BC	C	CD	
EX-1					100		100
EX-2					100		100

LAND USE (%) - External Areas										
Catchment	Meadow	Woodlot	Gravel	Lawns	Pasture Range	Crop	Fallow (Bare)	Low Density Residences	Impervious	Total
EX-1		100.0								100.0
EX-2		82.7				17.3				100.0

CURVE NUMBER (CN) - External Areas										
Catchment	Meadow	Woodlot	Gravel	Lawns	Pasture Range	Crop	Fallow (Bare)	Low Density Residences	Impervious	Weighted CN
EX-1	0.0	73.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	73
EX-2	0.0	60.4	0.0	0.0	0.0	14.2	0.0	0.0	0.0	75

** AMC II assumed

** Hydrological Soil Group taken from MTO Drainage Manual for each soil type

160401279: Derry Side Road Subdivision

NRSC (SCS) Modified Curve Number Calculation: Existing Condition Areas

Input Values					
Step 1	Subcatchment: CN (AMC II):			EX-1 73	EX-2 75
2	CN (AMC III) =			87	88
3	100 Year Precipitation, P =	106.73	mm	106.73	106.73

$$Q = \frac{(P - la)^2}{(P - la) + S} \quad S = \frac{(P - la)^2}{Q} - (P - la)$$

Q = rainfall excess or runoff, mm

S = potential maximum retention or available storage, mm

$$CN = \frac{25400}{S + 254} \quad S = \frac{25400}{CN} - 254$$

CN* = modified SCS curve # that better reflects la conditions in Ontario

Output Values					
	Subcatchment:			EX-1	EX-2
	S _{III} =		mm	37.95	34.64
	SCS Assumption of 0.2 S = la =		mm	7.59	6.93
4	Q _{III} =		mm	71.69	74.09
	Preferred Initial Abstraction, la =	1.5	mm	1.5	1.5
5	S* _{III} =		mm	49.23	44.23
6	CN* _{III} =		mm	83.77	85.17
	CN* _{III} =		Rounded	84	85
	CN* _{II} =		converted	69	70
7	CN* _{II} =		0.9 CN* _{III}	75.6	76.5

Explanation of Procedure

- 1 Determine CN based on typical AMC II conditions (from our normal spreadsheet).
- 2 Convert CN from AMC II to AMC III conditions (standard SCS tables, as shown at
- 3 Get precipitation depth P for 100 year storm
- 4 Using CN_{III} with la = 0.2S, compute Q_{III} for 100 year precipitation
- 5 For the same Q_{III}, compute S*_{III} using la=1.5mm (or otherwise determined from stl
- 6 Compute CN*_{III} using S*_{III}
- 7 Calculate CN*_{II} using standard SCS conversion table or assume 0.9CN*_{III}

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Appendix A Existing Conditions
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A.2 EXISTING CONDITION SWMHYMO MODELING FILES

```

00001> =====
00002>
00003> SSSSS W W M M H H Y Y M M O O 999 999 =====
00004> S W W W M M M M H H Y Y M M M O O 9 9 9 9 9
00005> SSSSS W W M M M H H H H Y Y M M M O O ## 9 9 9 9 9 Ver 4.05
00006> S W W M M H H Y Y M M O O 9999 9999 Sept 2011
00007> SSSSS W W M M H H Y Y M M O O 9 9 9 9 =====
00008> # 3824306
00009> StormWater Management Hydrologic Model 999 999 =====
00010>
00011> *****
00012> ***** SWMHYMO Ver/4.05 *****
00013> ***** A single event and continuous hydrologic simulation model *****
00014> ***** based on the principles of HYMO and its successors *****
00015> ***** OTHYMO-83 and OTHYMO-89. *****
00016>
00017> ***** Distributed by: J.F. Sabourin and Associates Inc. *****
00018> ***** Ottawa, Ontario: (613) 836-3884 *****
00019> ***** Gatineau, Quebec: (819) 243-6858 *****
00020> ***** E-Mail: swmhyo@jfsa.Com *****
00021> *****
00022>
00023> *****
00024> ***** Licensed user: Stantec Consulting Ltd. 604 *****
00025> ***** Ottawa SERIAL#:3824306 *****
00026> *****
00027> *****
00028> *****
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00031> ***** Max. number of rainfall points: 105408 *****
00032> ***** Max. number of flow points : 105408 *****
00033> *****
00034>
00035> ***** DESCRIPTION SUMMARY TABLE HEADERS (units depend on METOUT in START) *****
00036> *****
00037> ***** ID: Hydrograph Identification numbers, (1-10). *****
00038> ***** NHD: Hydrograph reference numbers, (6 digits or characters). *****
00039> ***** AREA: Drainage area associated with hydrograph, (ac.) or (ha.). *****
00040> ***** QPEAK: Peak flow of simulated hydrograph, (ft3/s) or (m3/s). *****
00041> ***** TpeakDate_hh:mm is the date and time of the peak flow. *****
00042> ***** R.V.: Runoff Volume of simulated hydrograph, (in) or (mm). *****
00043> ***** R.C.: Runoff Coefficient of simulated hydrograph, (ratio). *****
00044> ***** *: see WARNING or NOTE message printed at end of run. *****
00045> ***** **: see ERROR message printed at end of run. *****
00046> *****
00047> *****
00048> *****
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00051> *****
00052> *****
00053> ***** SUMMARY OUTPUT *****
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00056> *****
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00058> * Output filename: C:\SWMHYMO\exist.out *
00059> * Summary filename: C:\SWMHYMO\exist.sum *
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00061> * 1: *
00062> * 2: *
00063> * 3: *
00064> *****
00065> *****
00066> *****
00067> # *****
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00069> # Date : 09-08-2017
00070> # Modeller : [AMP]
00071> # Company : Stantec Consulting Ltd. 604
00072> # License # : 3824306
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00086> [METOUT= 2 (1=imperial, 2=metric output)]
00087> [NSTORM= 1 ]
00088> [NRUN = 2 ]
00089> *****
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00091> # Date : 09-08-2017
00092> # Modeller : [AMP]
00093> # Company : Stantec Consulting Ltd. 604
00094> # License # : 3824306
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00271> #-----
00272> # - Average CN values for each catchment were initially calculated on typical
00273> # AMC II conditions based on hydrologic soil group and land use. CN values
00274> # were subsequently modified using the SCS Modified Curve Number Calculations
00275> # - Soils information for the site area was obtained from exp's
00276> # Geotechnical Investigation dated July 21, 2017.
00277> # - Land use across the site areas consist mostly of woodlands and a small por
00278> # of crops as obtained from aerial photographs
00279> # - Time to peak for each catchment was estimated based on Tp = 0.67*Tc and
00280> # Tc values were calculated using the Uplands Method
00281> #-----
00282> # SITE AREA EX-1
00283> #-----
00284> 100:0004-----ID:NHYD-----AREA---OPEAK-TpeakDate_hh:mm-----R.V.-
00285> DESIGN NASHYD 01:EX-1 7.83 .492 No_date 6:19 48.13
00286> [CN= 75.6; N= 2.00]
00287> [Tp= .38;DT= 1.00]
00288> #-----
00289> # SITE AREA EX-2
00290> #-----
00291> 100:0005-----ID:NHYD-----AREA---OPEAK-TpeakDate_hh:mm-----R.V.-
00292> DESIGN NASHYD 02:EX-2 8.32 .436 No_date 6:33 49.25
00293> [CN= 76.5; N= 2.00]
00294> [Tp= .53;DT= 1.00]
00295> 100:0006-----ID:NHYD-----AREA---OPEAK-TpeakDate_hh:mm-----R.V.-
00296> ADD HYD 01:EX-1 7.83 .492 No_date 6:19 48.13
00297> + 02:EX-2 8.32 .436 No_date 6:33 49.25
00298> [DT= 1.00] SUM= 03:EX-SITE 16.15 .915 No_date 6:26 48.71
00299> ** END OF RUN : 101
00300>
00301> #-----
00302>
00303>
00304>
00305>
00306>
00307> RUN:COMMAND#
00308> 102:0001-----
00309> START
00310> [TZERO = .00 hrs on 0]
00311> [METOUT= 2 (1=imperial, 2=metric output)]
00312> [NSTORM= 1]
00313> [NSUR= 10]
00314> #-----
00315> # Project Name: [Derry Side Road Subdivision] Project Number: [160401279]
00316> # Date : 09-08-2017
00317> # Modeller : [AMP]
00318> # Company : Stantec Consulting Ltd. 604
00319> # License # : 3824306
00320> #-----
00321> 102:0002-----
00322> #-----
00323> # DEFAULT VALUES
00324> # FileName = C:\SWHMYMO\OTTAWA.VAL
00325> # ICASEDv = 1 (read and print data)
00326> # FileTitle= File comment: [2005 City of Ottawa Sewer Design Guideline]
00327> # PARAMETERS USED IN THE DESIGN STANDHYD COMMAND FOR OTTAWA.
00328> # Horton's infiltration equation parameters:
00329> # [F= 76.20 mm/hr] [Fc=13.20 mm/hr] [DCAI= 4.14 /hr] [F= .00 mm]
00330> # Parameters for PERVIOUS surfaces in STANDHYD:
00331> # [IAper= 4.67 mm] [LGP=40.00 m] [MNP=.250]
00332> # Parameters for IMPERVIOUS surfaces in STANDHYD:
00333> # [IAimp= 1.57 mm] [CLI= 1.50] [MNI=.013]
00334> # Parameters used in NASHYD:
00335> # [Ias= 4.67 mm] [N= 2.00]
00336> 102:0003-----
00337> READ STORM
00338> # FileName = storm.001
00339> # Comment =
00340> [SDT=10.00;SDUR= 3.00;PTOT= 31.86]
00341> #-----
00342> # DERRY SIDE ROAD SUBDIVISION - EXISTING CONDITIONS
00343> #-----
00344> # STORM: 12hr SCS Storms, 3hr Chicago storms
00345> # City of Ottawa 2004 IDF Parameters
00346> #-----
00347> # - Average CN values for each catchment were initially calculated on typical
00348> # AMC II conditions based on hydrologic soil group and land use. CN values
00349> # were subsequently modified using the SCS Modified Curve Number Calculations
00350> # - Soils information for the site area was obtained from exp's
00351> # Geotechnical Investigation dated July 21, 2017.
00352> # - Land use across the site areas consist mostly of woodlands and a small por
00353> # of crops as obtained from aerial photographs
00354> # - Time to peak for each catchment was estimated based on Tp = 0.67*Tc and
00355> # Tc values were calculated using the Uplands Method
00356> #-----
00357> # SITE AREA EX-1
00358> #-----
00359> 102:0004-----ID:NHYD-----AREA---OPEAK-TpeakDate_hh:mm-----R.V.-
00360> DESIGN NASHYD 01:EX-1 7.83 .086 No_date 1:36 6.77
00361> [CN= 75.6; N= 2.00]
00362> [Tp= .38;DT= 1.00]
00363> #-----
00364> # SITE AREA EX-2
00365> #-----
00366> 102:0005-----ID:NHYD-----AREA---OPEAK-TpeakDate_hh:mm-----R.V.-
00367> DESIGN NASHYD 02:EX-2 8.32 .076 No_date 1:50 7.03
00368> [CN= 76.5; N= 2.00]
00369> [Tp= .53;DT= 1.00]
00370> 102:0006-----ID:NHYD-----AREA---OPEAK-TpeakDate_hh:mm-----R.V.-
00371> ADD HYD 01:EX-1 7.83 .086 No_date 1:36 6.77
00372> + 02:EX-2 8.32 .076 No_date 1:50 7.03
00373> [DT= 1.00] SUM= 03:EX-SITE 16.15 .159 No_date 1:42 6.90
00374> ** END OF RUN : 104
00375>
00376> #-----
00377>
00378>
00379>
00380>
00381>
00382> RUN:COMMAND#
00383> 105:0001-----
00384> START
00385> [TZERO = .00 hrs on 0]
00386> [METOUT= 2 (1=imperial, 2=metric output)]
00387> [NSTORM= 1]
00388> [NSUR= 10]
00389> #-----
00390> # Project Name: [Derry Side Road Subdivision] Project Number: [160401279]
00391> # Date : 09-08-2017
00392> # Modeller : [AMP]
00393> # Company : Stantec Consulting Ltd. 604
00394> # License # : 3824306
00395> #-----
00396> 105:0002-----
00397> #-----
00398> # DEFAULT VALUES
00399> # FileName = C:\SWHMYMO\OTTAWA.VAL
00400> # ICASEDv = 1 (read and print data)
00401> # FileTitle= File comment: [2005 City of Ottawa Sewer Design Guideline]
00402> # PARAMETERS USED IN THE DESIGN STANDHYD COMMAND FOR OTTAWA.
00403> # Horton's infiltration equation parameters:
00404> # [F= 76.20 mm/hr] [Fc=13.20 mm/hr] [DCAI= 4.14 /hr] [F= .00 mm]
00405> # Parameters for PERVIOUS surfaces in STANDHYD:
00406> # [IAper= 4.67 mm] [LGP=40.00 m] [MNP=.250]

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00406> Parameters for IMPERVIOUS surfaces in STANDHYD:
00407> [IAimp= 1.57 mm] [CLI= 1.50] [MNI=.013]
00408> Parameters used in NASHYD:
00409> [Ias= 4.67 mm] [N= 2.00]
00410>
00411> 105:0003-----
00412> READ STORM
00413> # FileName = storm.001
00414> # Comment =
00415> [SDT=10.00;SDUR= 3.00;PTOT= 42.51]
00416> #-----
00417> # DERRY SIDE ROAD SUBDIVISION - EXISTING CONDITIONS
00418> #-----
00419> # STORM: 12hr SCS Storms, 3hr Chicago Storms
00420> # City of Ottawa 2004 IDF Parameters
00421> #-----
00422> # - Average CN values for each catchment were initially calculated on typical
00423> # AMC II conditions based on hydrologic soil group and land use. CN values
00424> # were subsequently modified using the SCS Modified Curve Number Calculations
00425> # - Soils information for the site area was obtained from exp's
00426> # Geotechnical Investigation dated July 21, 2017.
00427> # - Land use across the site areas consist mostly of woodlands and a small por
00428> # of crops as obtained from aerial photographs
00429> # - Time to peak for each catchment was estimated based on Tp = 0.67*Tc and
00430> # Tc values were calculated using the Uplands Method
00431> #-----
00432> # SITE AREA EX-1
00433> #-----
00434> 105:0004-----ID:NHYD-----AREA---OPEAK-TpeakDate_hh:mm-----R.V.-
00435> DESIGN NASHYD 01:EX-1 7.83 .156 No_date 1:34 11.95
00436> [CN= 75.6; N= 2.00]
00437> [Tp= .38;DT= 1.00]
00438> #-----
00439> # SITE AREA EX-2
00440> #-----
00441> 105:0005-----ID:NHYD-----AREA---OPEAK-TpeakDate_hh:mm-----R.V.-
00442> DESIGN NASHYD 02:EX-2 8.32 .137 No_date 1:47 12.36
00443> [CN= 76.5; N= 2.00]
00444> [Tp= .53;DT= 1.00]
00445> 105:0006-----ID:NHYD-----AREA---OPEAK-TpeakDate_hh:mm-----R.V.-
00446> ADD HYD 01:EX-1 7.83 .156 No_date 1:34 11.95
00447> + 02:EX-2 8.32 .137 No_date 1:47 12.36
00448> [DT= 1.00] SUM= 03:EX-SITE 16.15 .289 No_date 1:39 12.16
00449> ** END OF RUN : 199
00450>
00451> #-----
00452>
00453>
00454>
00455>
00456>
00457> RUN:COMMAND#
00458> 200:0001-----
00459> START
00460> [TZERO = .00 hrs on 0]
00461> [METOUT= 2 (1=imperial, 2=metric output)]
00462> [NSTORM= 1]
00463> [NSUR= 20]
00464> #-----
00465> # Project Name: [Derry Side Road Subdivision] Project Number: [160401279]
00466> # Date : 09-08-2017
00467> # Modeller : [AMP]
00468> # Company : Stantec Consulting Ltd. 604
00469> # License # : 3824306
00470> #-----
00471> 200:0002-----
00472> #-----
00473> # DEFAULT VALUES
00474> # FileName = C:\SWHMYMO\OTTAWA.VAL
00475> # ICASEDv = 1 (read and print data)
00476> # FileTitle= File comment: [2005 City of Ottawa Sewer Design Guideline]
00477> # PARAMETERS USED IN THE DESIGN STANDHYD COMMAND FOR OTTAWA.
00478> # Horton's infiltration equation parameters:
00479> # [F= 76.20 mm/hr] [Fc=13.20 mm/hr] [DCAI= 4.14 /hr] [F= .00 mm]
00480> # Parameters for PERVIOUS surfaces in STANDHYD:
00481> # [IAper= 4.67 mm] [LGP=40.00 m] [MNP=.250]
00482> # Parameters for IMPERVIOUS surfaces in STANDHYD:
00483> # [IAimp= 1.57 mm] [CLI= 1.50] [MNI=.013]
00484> # Parameters used in NASHYD:
00485> # [Ias= 4.67 mm] [N= 2.00]
00486> 200:0003-----
00487> READ STORM
00488> # FileName = storm.001
00489> # Comment =
00490> [SDT=10.00;SDUR= 3.00;PTOT= 71.66]
00491> #-----
00492> # DERRY SIDE ROAD SUBDIVISION - EXISTING CONDITIONS
00493> #-----
00494> # STORM: 12hr SCS Storms, 3hr Chicago Storms
00495> # City of Ottawa 2004 IDF Parameters
00496> #-----
00497> # - Average CN values for each catchment were initially calculated on typical
00498> # AMC II conditions based on hydrologic soil group and land use. CN values
00499> # were subsequently modified using the SCS Modified Curve Number Calculations
00500> # - Soils information for the site area was obtained from exp's
00501> # Geotechnical Investigation dated July 21, 2017.
00502> # - Land use across the site areas consist mostly of woodlands and a small por
00503> # of crops as obtained from aerial photographs
00504> # - Time to peak for each catchment was estimated based on Tp = 0.67*Tc and
00505> # Tc values were calculated using the Uplands Method
00506> #-----
00507> # SITE AREA EX-1
00508> #-----
00509> 200:0004-----ID:NHYD-----AREA---OPEAK-TpeakDate_hh:mm-----R.V.-
00510> DESIGN NASHYD 01:EX-1 7.83 .412 No_date 1:31 30.13
00511> [CN= 75.6; N= 2.00]
00512> [Tp= .38;DT= 1.00]
00513> #-----
00514> # SITE AREA EX-2
00515> #-----
00516> 200:0005-----ID:NHYD-----AREA---OPEAK-TpeakDate_hh:mm-----R.V.-
00517> DESIGN NASHYD 02:EX-2 8.32 .355 No_date 1:44 30.95
00518> [CN= 76.5; N= 2.00]
00519> [Tp= .53;DT= 1.00]
00520> 200:0006-----ID:NHYD-----AREA---OPEAK-TpeakDate_hh:mm-----R.V.-
00521> ADD HYD 01:EX-1 7.83 .412 No_date 1:31 30.13
00522> + 02:EX-2 8.32 .355 No_date 1:44 30.95
00523> [DT= 1.00] SUM= 03:EX-SITE 16.15 .756 No_date 1:36 30.55
00524> 200:0002-----
00525> FINISH
00526> #-----
00527> #-----
00528> # WARNINGS / ERRORS / NOTES
00529> #-----
00530> Simulation ended on 2017-09-13 at 13:24:46
00531> #-----
00532>
00533>

```

DERRY SIDE ROAD SUBDIVISION – BECKWITH, ON CONCEPTUAL STORMWATER MANAGEMENT REPORT

Appendix B Proposed Conditions
September 25, 2017

Appendix B PROPOSED CONDITIONS

A.1 Proposed Condition Parameters

A.2 Proposed Condition SWMHYMO Modeling Files

DERRY SIDE ROAD SUBDIVISION – BECKWITH, ON CONCEPTUAL STORMWATER MANAGEMENT REPORT

Appendix B Proposed Conditions
September 25, 2017

B.1 PROPOSED CONDITION PARAMETERS

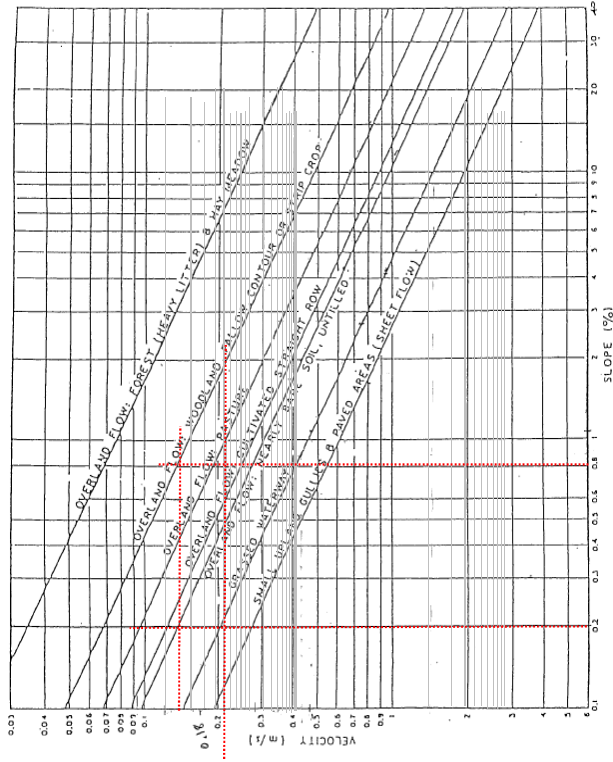
Model Catchment ID	Description	Area (ha)	Gradient (%)		XIMP (%)		TIMP (%)		Length (m)		Velocity (m/s)		Tp (hrs)	Tc (hrs)	Infiltration Method	CN	CN*	Ia Perv. (mm)	Ia Imp. (mm)	HYD Method
			Overland	Ditch	Overland	Ditch	Overland	Ditch	Overland	Ditch	Overland	Ditch								
A1	Developed (overland/ditch)	1.73	0.4%	0.5%	9.0%	0.5%	19.4%	0.5%	50	281	0.15	0.32	0.23	0.34	SCS	78	79.2	4.67	1.57	NASHYD
A2	Developed (overland/ditch)	1.88	0.4%	0.5%	7.0%	0.5%	11.8%	0.5%	90	281	0.15	0.32	0.28	0.41	SCS	76	78.3	4.67	1.57	NASHYD
A3	Developed (overland)	1.33	1.0%	0.5%	8.3%	0.5%	12.9%	0.5%	35	250	0.20	0.32	0.18	0.27	SCS	77	78.3	4.67	1.57	NASHYD
A4	Developed (overland/ditch)	2.71	0.6%	0.5%	6.2%	0.5%	11.8%	0.5%	98	132	0.17	0.32	0.18	0.27	SCS	76	78.3	4.67	1.57	NASHYD
A5	Developed (overland/ditch)	1.43	0.6%	0.5%	9.0%	0.5%	15.3%	0.5%	95	250	0.17	0.32	0.25	0.37	SCS	77	78.3	4.67	1.57	NASHYD
UNC-1	Developed (overland/ditch)	0.96	0.5%	-	6.4%	-	12.6%	-	110	0	0.13	-	0.24	0.24	SCS	77	78.3	4.67	1.57	NASHYD
UNC-2	Lawns and woodland (overland/ditch)	1.87	0.5%	-	0.0%	-	0.0%	-	104	0	0.10	-	0.29	0.19	SCS	73	75.6	4.67	1.57	NASHYD
UNC-3	Developed (overland/ditch)	0.55	0.4%	1.5%	13.3%	0.2%	24.2%	0.2%	50	45	0.15	0.52	0.12	0.08	SCS	74	76.5	4.67	1.57	STANDHYD
UNC-4	woodland (Overland/ditch)	3.65	0.8%	0.2%	0.3%	0.2%	1.2%	0.2%	197	232	0.16	0.20	0.45	0.66	SCS	74	76.5	4.67	1.57	NASHYD
Total Area		16.11			5.2%		9.7%													

0.097

1) Standard City of Ottawa Data for Initial Abstraction Parameters, Tp determination, and Infiltration (CN) values

OGS-1 3.61 ha 15.5%
 OGS-2 5.47 ha 13.0%

Uplands Method Velocity Determination



Source: Upland Method for Estimating Time of Concentration
 (SCS National Engineering Handbook, 1971)

Land Use Area (ha)														
woodlot	gravel	lawns	crop	fallow	pasture	meadow	residence	impervious	Roofs	Half Road	Driveways	Impervious Area	Site Area	Site %Imp
0.60	0.00	0.79	0.00	0.00	0.00	0.00	0.00	0.34	6.0	275.0	3.05	0.336	1.73	19.41%
1.31	0.00	0.35	0.00	0.00	0.00	0.00	0.22	0.22	3.0	290.0	3.05	0.222	1.88	11.83%
0.50	0.00	0.66	0.00	0.00	0.00	0.00	0.17	0.17	3.0	250.0	3.05	0.171	1.33	12.66%
1.00	0.00	1.39	0.00	0.00	0.00	0.00	0.32	0.32	5.0	260.0	3.05	0.319	2.71	11.78%
0.50	0.00	0.71	0.00	0.00	0.00	0.00	0.22	0.22	3.0	262.0	3.05	0.219	1.43	15.32%
0.37	0.00	0.47	0.00	0.00	0.00	0.00	0.12	0.12	2.0	114.0	3.05	0.121	0.96	12.62%
1.40	0.00	0.47	0.00	0.00	0.00	0.00	0.00	0.00	2.0	0.0	3.05	0.000	1.87	0.00%
0.07	0.00	0.35	0.00	0.00	0.00	0.00	0.13	0.13	2.0	90.0	3.05	0.133	0.55	24.19%
2.45	0.00	1.16	0.00	0.00	0.00	0.00	0.04	0.04	1.0	0.0	3.05	0.043	3.65	1.17%
													16.11	9.71%

Imperviousness

Impervious areas included when NASHYD command used

160401279: Derry Side Road Subdivision
 NRCS (SCS) Curve Number Determination
 Proposed Drainage Areas

Site Soils: (as per exp Geotechnical Investigation, July 21, 2017)

Soil Type

Hydrologic Soil Group

Silty sand with some gravel

C

TABLE OF CURVE NUMBERS (CN's)									
Land Use	Hydrologic Soil Type							Manning's 'n'	Source
	A	AB	B	BC	C	CD	D		
Meadow "Good"	30	44	58	64.5	71	74.5	78	0.40	MTO
Woodlot "Fair"	36	48	60	66.5	73	76	79	0.40	MTO
Gravel	76	80.5	85	87	89	90	91	0.30	City
Lawns "Good"	39	50	61	67.5	74	77	80	0.25	City
Pasture/Range	58	61.5	65	70.5	76	78.5	81	0.17	MTO
Crop	66	70	74	78	82	84	86	0.13	MTO
Fallow (Bare)	77	82	86	89	91	93	94	0.05	MTO
Low Density Residences	57	64.5	72	76.5	81	83.5	86	0.25	Chin
Streets, paved	98	98	98	98	98	98	98	0.01	City

1. MTO Drainage Manual (1997), Design Chart 1.09-Soil/Land Use Curve Numbers
2. Chin (2000), Water-Resources Engineering, Table 6.13-Curve Numbers for Various Urban Land Uses
3. City of Ottawa Sewer Design Guidelines (2004), Table 5.9 CN Values for Various Soil Groups

HYDROLOGIC SOIL TYPE (%)								
Catchment	Hydrologic Soil Type							TOTAL
	A	AB	B	BC	C	CD	D	
A1					100			100
A2					100			100
A3					100			100
A4					100			100
A5					100			100
UNC-1					100			100
UNC-2					100			100
UNC-3					100			100
UNC-4					100			100

LAND USE (%)										
Catchment	Meadow	Woodlot	Gravel	Lawns	Pasture Range	Crop	Fallow (Bare)	Low Density Residences	Impervious	Total
A1		34.7		45.9					19.4	100.0
A2		69.6		18.6					11.8	100.0
A3		37.6		49.5					12.9	100.0
A4		36.9		51.3					11.8	100.0
A5		35.0		49.7					15.3	100.0
UNC-1		38.5		48.8					12.6	100.0
UNC-2		74.9		25.1					0.0	100.0
UNC-3		16.8		83.2					24.2	100.0
UNC-4		67.1		31.7					1.2	100.0

Note: Where STANDHYD command used (shaded), impervious fraction is not considered in CN determination, since %Imp directly input in STANDHYD command

CURVE NUMBER (CN) - External Areas										
Catchment	Meadow	Woodlot	Gravel	Lawns	Pasture Range	Crop	Fallow (Bare)	Low Density Residences	Impervious	Weighted CN
A1	0.0	25.3	0.0	34.0	0.0	0.0	0.0	0.0	19.0	78
A2	0.0	50.8	0.0	13.8	0.0	0.0	0.0	0.0	11.6	76
A3	0.0	27.4	0.0	36.7	0.0	0.0	0.0	0.0	12.6	77
A4	0.0	26.9	0.0	38.0	0.0	0.0	0.0	0.0	11.5	76
A5	0.0	25.5	0.0	36.8	0.0	0.0	0.0	0.0	15.0	77
UNC-1	0.0	28.1	0.0	36.1	0.0	0.0	0.0	0.0	12.4	77
UNC-2	0.0	54.7	0.0	18.6	0.0	0.0	0.0	0.0	0.0	73
UNC-3	0.0	12.3	0.0	61.6	0.0	0.0	0.0	0.0	0.0	74
UNC-4	0.0	49.0	0.0	23.5	0.0	0.0	0.0	0.0	1.1	74

** AMC II assumed

** Hydrological Soil Group taken from MTO Drainage Manual for each soil type

NRSC (SCS) Modified Curve Number Calculation: Proposed Condition Areas

Step	Input Values	A1	A2	A3	A4	A5	UNC-1	UNC-2	UNC-3	UNC-4
1	Subcatchment: CN (AMC II):	78		76	77	76	77	77	73	74
2	CN (AMC III) =	90		89	89	89	89	89	87	88
3	100 Year Precipitation, P =	106.73	mm	106.73	106.73	106.73	106.73	106.73	106.73	106.73

$$Q = \frac{(P - I_a)^2}{(P - I_a) + S} \quad S = \frac{(P - I_a)^2}{Q} - (P - I_a)$$

Q = rainfall excess or runoff, mm

S = potential maximum retention or available storage, mm

$$CN = \frac{25400}{S + 254} \quad S = \frac{25400}{CN} - 254$$

CN* = modified SCS curve # that better reflects la conditions in Ontario

Step	Output Values	A1	A2	A3	A4	A5	UNC-1	UNC-2	UNC-3	UNC-4
4	Subcatchment: S _{II} = 28.22 mm SCS Assumption of 0.2 S = I _a = 5.64 mm Q _{II} = 79.02 mm		31.39 6.28 76.53	31.39 6.28 76.53	31.39 6.28 76.53	31.39 6.28 76.53	31.39 6.28 76.53	37.95 7.59 71.69	34.64 6.93 74.09	34.64 6.93 74.09
5	Preferred Initial Abstraction, I _a = 1.5 mm S* _{III} = 34.90 mm CN* _{III} = 87.92 mm	1.5	39.46 86.55	39.46 86.55	39.46 86.55	39.46 86.55	39.46 86.55	49.23 83.77	44.23 85.17	44.23 85.17
7	CN* _{II} = 88 CN* _I = 75 CN* _I = 79.2	88 75 79.2	87 73 78.3	87 73 78.3	87 73 78.3	87 73 78.3	87 73 78.3	84 69 75.6	85 70 76.5	85 70 76.5

Explanation of Procedure

- 1 Determine CN based on typical AMC II conditions (from our normal spreadsheet).
- 2 Convert CN from AMC II to AMC III conditions (standard SCS tables, as shown at side)
- 3 Get precipitation depth P for 100 year storm
- 4 Using CN_{III} with I_a = 0.2S, compute Q_{II} for 100 year precipitation
- 5 For the same Q_{II}, compute S*_{III} using I_a=1.5mm (or otherwise determined from studies)
- 6 Compute CN*_{III} using S*_{III}
- 7 Calculate CN*_{II} using standard SCS conversion table or assume 0.9CN*_{III}

DERRY SIDE ROAD SUBDIVISION – BECKWITH, ON CONCEPTUAL STORMWATER MANAGEMENT REPORT

Appendix B Proposed Conditions
September 25, 2017

B.2 PROPOSED CONDITION SWMHYMO MODELING FILES

```

00001> =====
00002>
00003> SSSSS W W M M H H Y Y M M O O 999 999
00004> S W W W M M M H H Y Y M M M O O 9 9 9 9
00005> SSSSS W W M M M H H H H Y Y M M M O O ## 9 9 9 9 Ver 4.05
00006> S W W M M M H H H Y Y M M O O 9999 9999 Sept 2011
00007> SSSSS W W M M H H Y Y M M O O 9 9 9
00008> StormWater Management Hydrologic Model 9 9 9 9
00009>
00010>
00011> *****
00012> ***** SWMHYMO Ver/4.05 *****
00013> ***** A single event and continuous hydrologic simulation model *****
00014> ***** based on the principles of HYMO and its successors *****
00015> ***** OTTHYMO-83 and OTTHYMO-89. *****
00016>
00017> ***** Distributed by: J.F. Sabourin and Associates Inc. *****
00018> ***** Ottawa, Ontario: (613) 836-3884 *****
00019> ***** Gatineau, Quebec: (819) 243-6858 *****
00020> ***** E-Mail: swmhyo@jfsa.Com *****
00021> *****
00022>
00023> *****
00024> ***** Licensed user: Stantec Consulting Ltd. 604 *****
00025> ***** Ottawa SERIAL#:3824306 *****
00026> *****
00027> *****
00028> *****
00029> ***** PROGRAM ARRAY DIMENSIONS *****
00030> ***** Maximum value for ID numbers : 10 *****
00031> ***** Max. number of rainfall points: 105408 *****
00032> ***** Max. number of flow points : 105408 *****
00033> *****
00034> *****
00035> *****
00036> ***** D E T A I L E D   O U T P U T *****
00037> *****
00038> ***** DATE: 2017-09-15 TIME: 09:45:29 RUN COUNTER: 000018 *****
00039> *****
00040> * Input filename: C:\SWMHYMO\post.dat *
00041> * Output filename: C:\SWMHYMO\post.out *
00042> * Summary filename: C:\SWMHYMO\post.sum *
00043> * User comments: *
00044> * 1: *
00045> * 2: *
00046> * 3: *
00047> *****
00048> *****
00049> *****
00050> 001:0001-----
00051> # *****
00052> # Project Name: [Derry Side Road Subdivision] Project Number: [160401279]
00053> # Date : 09-20-2017
00054> # Modeller : [AMP]
00055> # Company : Stantec Consulting Ltd. 604
00056> # License # : 3824306
00057> *****
00058> *****
00059> | START | Project dir.: C:\SWMHYMO\
00060> | Rainfall dir.: C:\SWMHYMO\
00061> | TZERO = .00 hrs on 0
00062> | METOUT= 2 (output = METRIC)
00063> | NRUN = 001
00064> | NSTORM= 1
00065> | # 1=O4CH25m.stm
00066> *****
00067> 001:0002-----
00068> *****
00069> | DEFAULT VALUES | Filename: C:\SWMHYMO\OTTAWA.VAL
00070> | ICASEdv = 1 (read and print data)
00071> | FileTitle= File comment: [2005 City of Ottawa Sewer Design Guideline]
00072> | PARAMETERS USED IN THE DESIGN STANDHYD COMMAND FOR OTTAWA.
00073> | Horton's infiltration equation parameters:
00074> | [Fo= 76.20 mm/hr] [Fc=13.20 mm/hr] [DCAV= 4.14 /hr] [F= .00 mm]
00075> | Parameters for PERVIOUS surfaces in STANDHYD:
00076> | [Iaper= 4.67 mm] [LGP=40.00 m] [MNP= .250]
00077> | Parameters for IMPERVIOUS surfaces in STANDHYD:
00078> | [Iimp= 1.57 mm] [CLI= 1.50] [MNI= .013]
00079> | Parameters used in NASHYD:
00080> | [Ia= 4.67 mm] [N= 2.00]
00081> *****
00082> 001:0003-----
00083> *****
00084> | READ STORM | Filename: 25mm CHICAGO STORM, 4hr, DT=20min
00085> | Ptotal= 25.00 mm | Comments: 25mm CHICAGO STORM, 4hr, DT=20min
00086> *****
00087> *****
00088> TIME RAIN | TIME RAIN | TIME RAIN | TIME RAIN
00089> hrs mm/hr | hrs mm/hr | hrs mm/hr | hrs mm/hr
00090> .33 1.809 | 1.33 38.428 | 2.33 3.108 | 3.33 1.665
00091> .67 2.746 | 1.67 8.899 | 2.67 2.391 | 3.67 1.455
00092> 1.00 6.715 | 2.00 4.539 | 3.00 1.957 | 4.00 1.295
00093> *****
00094> 001:0004-----
00095> *****
00096> # *****
00097> # DERRY SIDE ROAD SUBDIVISION - POST DEVELOPMENT CONDITIONS
00098> *****
00099> # STORM: 12hr SCS Storms, 3hr Chicago Storms
00100> # City of Ottawa 2004 IDF Parameters
00101> *****
00102> # - Average CN values for each catchment were initially calculated on typical
00103> # AMC II conditions based on hydrologic soil group and land use. CN values
00104> # were subsequently modified using the SCS Modified Curve Number Calculations
00105> # - Soils information for the site area was obtained from exp's
00106> # Geotechnical Investigation dated July 21, 2017.
00107> # - CN values calculated based on lawns, woodland and impervious areas
00108> # - NASHYD command used for catchments with TIME RUN COUNTER. CN values
00109> # - Time to peak for each catchment was estimated based on Tp = 0.67*Tc and
00110> # Tc values were calculated using the Uplands Method
00111> *****
00112> ***** AREA A1 TO SWM 1 *****
00113> *****
00114> *****
00115> | DESIGN NASHYD | Area (ha)= 1.73 Curve Number (CN)=79.20
00116> | 01:A1 DT= 1.00 | Ia (mm)= 4.670 # of Linear Res. (N)= 2.00
00117> | U.H. Tp (hrs)= .230
00118> *****
00119> Unit Hyd Qpeak (cms)= .195
00120> *****
00121> PEAK FLOW (cms)= .016 (i)
00122> TIME TO PEAK (hrs)= 1.650
00123> RUNOFF VOLUME (mm)= 4.749
00124> TOTAL RAINFALL (mm)= 25.002
00125> RUNOFF COEFFICIENT = .190
00126> *****
00127> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00128> *****
00129> *****
00130> 001:0005-----
00131> *****
00132> # ***** AREA A2 TO SWM 1 *****
00133> *****
00134> *****
00135> | DESIGN NASHYD | Area (ha)= 1.88 Curve Number (CN)=78.30

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00136> | 02:A2 DT= 1.00 | Ia (mm)= 4.670 # of Linear Res. (N)= 2.00
00137> | U.H. Tp (hrs)= .280
00138> *****
00139> Unit Hyd Qpeak (cms)= .174
00140> *****
00141> PEAK FLOW (cms)= .015 (i)
00142> TIME TO PEAK (hrs)= 1.717
00143> RUNOFF VOLUME (mm)= 4.556
00144> TOTAL RAINFALL (mm)= 25.002
00145> RUNOFF COEFFICIENT = .182
00146> *****
00147> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00148> *****
00149> *****
00150> 001:0006-----
00151> *****
00152> | ADD HYD (TOSWM1 ) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
00153> | (ha) (cms) (hrs) (mm) (cms)
00154> | ID1 01:A1 1.73 .016 1.65 4.75 .000
00155> | +ID2 02:A2 1.88 .015 1.72 4.56 .000
00156> | *****
00157> | SUM 06:TOSWM1 3.61 .031 1.68 4.65 .000
00158> *****
00159> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
00160> *****
00161> *****
00162> 001:0007-----
00163> *****
00164> | COMPUTE VOLUME |
00165> | ID:06 (TOSWM1) | DISCHARGE TIME
00166> | (cms) (hrs)
00167> *****
00168> *** WARNING: No storage required, RelRate > Inflow Qp.
00169> *****
00170> 001:0008-----
00171> # *****
00172> # ***** AREA A3 TO SWM 2 *****
00173> *****
00174> | DESIGN NASHYD | Area (ha)= 1.33 Curve Number (CN)=78.30
00175> | 01:A3 DT= 1.00 | Ia (mm)= 4.670 # of Linear Res. (N)= 2.00
00176> | U.H. Tp (hrs)= .180
00177> *****
00178> *****
00179> Unit Hyd Qpeak (cms)= .192
00180> *****
00181> PEAK FLOW (cms)= .014 (i)
00182> TIME TO PEAK (hrs)= 1.500
00183> RUNOFF VOLUME (mm)= 4.556
00184> TOTAL RAINFALL (mm)= 25.002
00185> RUNOFF COEFFICIENT = .182
00186> *****
00187> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00188> *****
00189> 001:0009-----
00190> # *****
00191> # ***** AREA A4 TO SWM 2 *****
00192> *****
00193> *****
00194> | DESIGN NASHYD | Area (ha)= 2.71 Curve Number (CN)=78.30
00195> | 02:A4 DT= 1.00 | Ia (mm)= 4.670 # of Linear Res. (N)= 2.00
00196> | U.H. Tp (hrs)= .180
00197> *****
00198> *****
00199> Unit Hyd Qpeak (cms)= .391
00200> *****
00201> PEAK FLOW (cms)= .028 (i)
00202> TIME TO PEAK (hrs)= 1.500
00203> RUNOFF VOLUME (mm)= 4.557
00204> TOTAL RAINFALL (mm)= 25.002
00205> RUNOFF COEFFICIENT = .182
00206> *****
00207> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00208> *****
00209> 001:0010-----
00210> # *****
00211> # ***** AREA A5 TO SWM 2 *****
00212> *****
00213> *****
00214> | DESIGN NASHYD | Area (ha)= 1.43 Curve Number (CN)=78.30
00215> | 03:A5 DT= 1.00 | Ia (mm)= 4.670 # of Linear Res. (N)= 2.00
00216> | U.H. Tp (hrs)= .250
00217> *****
00218> *****
00219> Unit Hyd Qpeak (cms)= .148
00220> *****
00221> PEAK FLOW (cms)= .012 (i)
00222> TIME TO PEAK (hrs)= 1.683
00223> RUNOFF VOLUME (mm)= 4.556
00224> TOTAL RAINFALL (mm)= 25.002
00225> RUNOFF COEFFICIENT = .182
00226> *****
00227> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00228> *****
00229> 001:0011-----
00230> *****
00231> | ADD HYD (TOSWM2 ) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
00232> | (ha) (cms) (hrs) (mm) (cms)
00233> | ID1 01:A3 1.33 .014 1.50 4.56 .000
00234> | +ID2 02:A4 2.71 .028 1.50 4.56 .000
00235> | +ID3 03:A5 1.43 .012 1.68 4.56 .000
00236> | *****
00237> | SUM 05:TOSWM2 5.47 .053 1.53 4.56 .000
00238> *****
00239> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
00240> *****
00241> *****
00242> 001:0012-----
00243> *****
00244> | COMPUTE VOLUME |
00245> | ID:05 (TOSWM2) | DISCHARGE TIME
00246> | (cms) (hrs)
00247> *****
00248> *** WARNING: No storage required, RelRate > Inflow Qp.
00249> *****
00250> 001:0013-----
00251> # *****
00252> # ***** UNCONTROLLED AREA UNC-1 *****
00253> *****
00254> | DESIGN NASHYD | Area (ha)= .96 Curve Number (CN)=78.30
00255> | 10:UNC-1 DT= 1.00 | Ia (mm)= 4.670 # of Linear Res. (N)= 2.00
00256> | U.H. Tp (hrs)= .160
00257> *****
00258> *****
00259> Unit Hyd Qpeak (cms)= .156
00260> *****
00261> PEAK FLOW (cms)= .011 (i)
00262> TIME TO PEAK (hrs)= 1.467
00263> RUNOFF VOLUME (mm)= 4.556
00264> TOTAL RAINFALL (mm)= 25.002
00265> RUNOFF COEFFICIENT = .182
00266> *****
00267> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00268> *****
00269> 001:0014-----
00270> # *****
00271> *****

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00271> *# UNCONTROLLED AREA UNC-2
00272> *#
00273>
00274> | DESIGN NASHYD | Area (ha)= 1.87 Curve Number (CN)=75.60
00275> | 09:UNC-2 DT= 1.00 | Ia (mm)= 4.670 # of Linear Res. (N)= 2.00
00276> | U.H. Tp(hrs)= .190
00277>
00278> Unit Hyd Qpeak (cms)= .255
00279>
00280> PEAK FLOW (cms)= .016 (i)
00281> TIME TO PEAK (hrs)= 1.533
00282> RUNOFF VOLUME (mm)= 4.040
00283> TOTAL RAINFALL (mm)= 25.002
00284> RUNOFF COEFFICIENT = .162
00285>
00286> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00287>
00288>
00289> 001:0015
00290> *#
00291> *# UNCONTROLLED AREA UNC-3
00292> *#
00293>
00294> | DESIGN STANDHYD | Area (ha)= .55
00295> | 08:UNC-3 DT= 1.00 | Total Imp(%)= 24.20 Dir. Conn.(%)= 13.30
00296>
00297>
00298> Surface Area (ha)= IMPERVIOUS PERVIOUS (i)
00299> Dep. Storage (mm)= 1.57 4.67
00300> Average Slope (%)= 1.00 1.00
00301> Length (m)= 60.55 40.00
00302> Mannings n = .013 .250
00303>
00304> Max. eff. Inten. (mm/hr)= 38.43 7.65
00305> over (min) 3.00 27.00
00306> Storage Coeff. (min)= 2.77 (ii) 27.07 (ii)
00307> Unit Hyd. Tpeak (min)= 3.00 27.00
00308> Unit Hyd. peak (cms)= .39 .04
00309>
00310> PEAK FLOW (cms)= .01 .00
00311> TIME TO PEAK (hrs)= 1.33 1.75
00312> RUNOFF VOLUME (mm)= 23.43 .44
00313> TOTAL RAINFALL (mm)= 25.00 25.00
00314> RUNOFF COEFFICIENT = .94 .02
00315>
00316> (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
00317> Fo (mm/hr)= 76.20 K (1/hr)= 4.14
00318> Fc (mm/hr)= 13.20 Cum. Inf. (mm)= .00
00319> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
00320> THAN THE STORAGE COEFFICIENT.
00321> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00322>
00323>
00324> 001:0016
00325> *#
00326> *# UNCONTROLLED AREA UNC-4
00327> *#
00328>
00329> | DESIGN NASHYD | Area (ha)= 3.65 Curve Number (CN)=76.50
00330> | 07:UNC-4 DT= 1.00 | Ia (mm)= 4.670 # of Linear Res. (N)= 2.00
00331> | U.H. Tp(hrs)= .450
00332>
00333> Unit Hyd Qpeak (cms)= .211
00334>
00335> PEAK FLOW (cms)= .020 (i)
00336> TIME TO PEAK (hrs)= 2.000
00337> RUNOFF VOLUME (mm)= 4.203
00338> TOTAL RAINFALL (mm)= 25.003
00339> RUNOFF COEFFICIENT = .168
00340>
00341> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00342>
00343>
00344> 001:0017
00345> *#
00346> | ADD HYD (UNC ) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
00347> | ICASEdv = 1 (read and print data) (ha) (cms) (hrs) (mm) (cms)
00348> +ID1 10:UNC-1 1.87 .016 1.47 4.56 .000
00349> +ID2 09:UNC-2 1.87 .016 1.53 4.04 .000
00350> +ID3 08:UNC-3 .55 .008 1.33 3.49 .000
00351> +ID4 07:UNC-4 3.65 .020 2.00 4.20 .000
00352>
00353> SUM 04:UNC 7.03 .045 1.67 4.15 .000
00354>
00355> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
00356>
00357>
00358> 001:0018
00359> ** END OF RUN : 1
00360>
00361>
00362>
00363>
00364>
00365>
00366>
00367>
00368> | STAR | Project dir.: C:\SWMHYMO\
00369> | Rainfall dir.: C:\SWMHYMO\
00370> TZERO = .00 hrs on 0
00371> METOUT= 2 (output = METRIC)
00372> NRUN = 002
00373> NSTORM= 1
00374> # 1=012SC2yr.stm
00375>
00376> 002:0002
00377> *#
00378> *# Project Name: [Derry Side Road Subdivision] Project Number: [160401279]
00379> *# Date : 09-13-2017
00380> *# Modeller : [AM]
00381> *# Company : Stantec Consulting Ltd. 604
00382> *# License # : 3824306
00383> *#
00384>
00385> 002:0002
00386>
00387> | DEFAULT VALUES | Filename: C:\SWMHYMO\OTTAWA.VAL
00388>
00389> FileTitle= File comment: [2005 City of Ottawa Sewer Design Guideline]
00390> PARAMETERS USED IN THE DESIGN STANDHYD COMMAND FOR OTTAWA.
00391> Horton's infiltration equation parameters:
00392> [Fo= 76.20 mm/hr] [Fc=13.20 mm/hr] [DCAV= 4.14 /hr] [F= .00 mm]
00393> Parameters for PERVIOUS surfaces in STANDHYD:
00394> [IaPerv= 4.67 mm] [LGP=40.00 m] [MNP= .250]
00395> Parameters for IMPERVIOUS surfaces in STANDHYD:
00396> [IaImp= 1.57 mm] [CLI= 1.50] [MNI= .013]
00397> Parameters used in NASHYD:
00398> [Ia= 4.67 mm] [N= 2.00]
00399>
00400> 002:0003
00401>
00402> | READ STORM | Filename: 2yr,12hr SCS STORM (Ottawa)
00403> | Ptotal= 42.34 mm | Comments: 2yr,12hr SCS STORM (Ottawa)
00404>
00405> TIME RAIN | TIME RAIN | TIME RAIN | TIME RAIN

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00406> hrs mm/hr | hrs mm/hr | hrs mm/hr | hrs mm/hr
00407> .50 1.270 | 3.50 1.694 | 6.50 9.230 | 9.50 1.270
00408> 1.00 .533 | 4.00 1.694 | 7.00 4.065 | 10.00 1.016
00409> 1.50 1.101 | 4.50 2.286 | 7.50 2.710 | 10.50 1.440
00410> 2.00 1.101 | 5.00 2.879 | 8.00 2.371 | 11.00 .931
00411> 2.50 1.440 | 5.50 4.573 | 8.50 1.863 | 11.50 .847
00412> 3.00 1.270 | 6.00 36.243 | 9.00 1.948 | 12.00 .847
00413>
00414>
00415> 002:0004
00416> *#
00417> *#
00418> *# DERRY SIDE ROAD SUBDIVISION - POST DEVELOPMENT CONDITIONS
00419> *#
00420> *# STORM: 12hr SCS Storms, 3hr Chicago Storms
00421> *# City of Ottawa 2004 IDF Parameters
00422> *#
00423> *# - Average CN values for each catchment were initially calculated on typical
00424> *# - CN values calculated based on hydrologic soil group and land use. CN values
00425> *# were subsequently modified using the SCS Modified Curve Number Calculations
00426> *# - Soils information for the site area was obtained from exp's
00427> *# Geotechnical Investigation dated July 21, 2017.
00428> *# - CN values calculated based on lawns, woodland and impervious areas
00429> *# - NASHYD command used for catchments with TIME=20%
00430> *# - Time to peak for each catchment was estimated based on Tp = 0.67*Tc and
00431> *# Tc values were calculated using the Uplands Method
00432> *#
00433> *# AREA A1 TO SWM 1
00434> *#
00435>
00436> | DESIGN NASHYD | Area (ha)= 1.73 Curve Number (CN)=79.20
00437> | 01:A1 DT= 1.00 | Ia (mm)= 4.670 # of Linear Res. (N)= 2.00
00438> | U.H. Tp(hrs)= .230
00439>
00440> Unit Hyd Qpeak (cms)= .195
00441>
00442> PEAK FLOW (cms)= .040 (i)
00443> TIME TO PEAK (hrs)= 6.133
00444> RUNOFF VOLUME (mm)= 13.595
00445> TOTAL RAINFALL (mm)= 42.340
00446> RUNOFF COEFFICIENT = .321
00447>
00448> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00449>
00450>
00451> 002:0005
00452> *#
00453> *# AREA A2 TO SWM 1
00454> *#
00455>
00456> | DESIGN NASHYD | Area (ha)= 1.88 Curve Number (CN)=78.30
00457> | 02:A2 DT= 1.00 | Ia (mm)= 4.670 # of Linear Res. (N)= 2.00
00458> | U.H. Tp(hrs)= .280
00459>
00460> Unit Hyd Qpeak (cms)= .174
00461>
00462> PEAK FLOW (cms)= .037 (i)
00463> TIME TO PEAK (hrs)= 6.200
00464> RUNOFF VOLUME (mm)= 13.131
00465> TOTAL RAINFALL (mm)= 42.340
00466> RUNOFF COEFFICIENT = .310
00467>
00468> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00469>
00470>
00471> 002:0006
00472>
00473> | ADD HYD (TOSWMI ) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
00474> (ha) (cms) (hrs) (mm) (cms)
00475> ID1 01:A1 1.73 .040 6.13 13.59 .000
00476> +ID2 02:A2 1.88 .037 6.20 13.13 .000
00477>
00478> SUM 06:TOSWMI 3.61 .077 6.17 13.35 .000
00479>
00480> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
00481>
00482>
00483>
00484>
00485> | COMPUTE VOLUME |
00486> | ID:06 (TOSWMI) | DISCHARGE TIME
00487> (cms) (hrs)
00488> *** WARNING: No storage required, RelRate > Inflow Qp.
00489>
00490> 002:0008
00491> *#
00492> *# AREA A3 TO SWM 2
00493> *#
00494>
00495> | DESIGN NASHYD | Area (ha)= 1.33 Curve Number (CN)=78.30
00496> | 01:A3 DT= 1.00 | Ia (mm)= 4.670 # of Linear Res. (N)= 2.00
00497> | U.H. Tp(hrs)= .180
00498>
00499> Unit Hyd Qpeak (cms)= .192
00500>
00501> PEAK FLOW (cms)= .034 (i)
00502> TIME TO PEAK (hrs)= 6.067
00503> RUNOFF VOLUME (mm)= 13.131
00504> TOTAL RAINFALL (mm)= 42.340
00505> RUNOFF COEFFICIENT = .310
00506>
00507> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00508>
00509>
00510> 002:0009
00511> *#
00512> *# AREA A4 TO SWM 2
00513> *#
00514>
00515> | DESIGN NASHYD | Area (ha)= 2.71 Curve Number (CN)=78.30
00516> | 02:A4 DT= 1.00 | Ia (mm)= 4.670 # of Linear Res. (N)= 2.00
00517> | U.H. Tp(hrs)= .180
00518>
00519> Unit Hyd Qpeak (cms)= .391
00520>
00521> PEAK FLOW (cms)= .070 (i)
00522> TIME TO PEAK (hrs)= 6.067
00523> RUNOFF VOLUME (mm)= 13.131
00524> TOTAL RAINFALL (mm)= 42.340
00525> RUNOFF COEFFICIENT = .310
00526>
00527> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00528>
00529>
00530> 002:0010
00531> *#
00532> *# AREA A5 TO SWM 2
00533> *#
00534>
00535> | DESIGN NASHYD | Area (ha)= 1.43 Curve Number (CN)=78.30
00536> | 03:A5 DT= 1.00 | Ia (mm)= 4.670 # of Linear Res. (N)= 2.00
00537> | U.H. Tp(hrs)= .250
00538>
00539> Unit Hyd Qpeak (cms)= .148
00540>

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00541> PEAK FLOW (cms)= .030 (i)
00542> TIME TO PEAK (hrs)= 6.150
00543> RUNOFF VOLUME (mm)= 13.131
00544> TOTAL RAINFALL (mm)= 42.340
00545> RUNOFF COEFFICIENT = .310
00546>
00547> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00548>
00549>
00550> 002:0011-----
00551>
00552> | ADD HYD (TOSWM2 ) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
00553> | (ha) (cms) (hrs) (mm) (cms)
00554> | I1 01:A3 1.33 .034 6.07 13.13 .000
00555> | +I2 02:A4 2.71 .070 6.07 13.13 .000
00556> | +I3 03:A5 1.43 .030 6.15 13.13 .000
00557>
00558> SUM 05:TOSWM2 5.47 .134 6.08 13.13 .000
00559>
00560> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
00561>
00562>
00563> 002:0012-----
00564>
00565> | COMPUTE VOLUME |
00566> | ID:05 (TOSWM2) | DISCHARGE TIME
00567> | (cms) (hrs)
00568>
00569> ** WARNING: No storage required, RelRate > Inflow Qp.
00570>
00571> 002:0013-----
00572> # UNCONTROLLED AREA UNC-1
00573> #
00574>
00575> | DESIGN NASHYD | Area (ha)= .96 Curve Number (CN)=78.30
00576> | 10:UNC-1 DT= 1.00 | Ia (mm)= 4.670 # of Linear Res. (N)= 2.00
00577> | U.H. Tp(hrs)= .160
00578>
00579> Unit Hyd Qpeak (cms)= .156
00580>
00581> PEAK FLOW (cms)= .027 (i)
00582> TIME TO PEAK (hrs)= 6.050
00583> RUNOFF VOLUME (mm)= 13.131
00584> TOTAL RAINFALL (mm)= 42.340
00585> RUNOFF COEFFICIENT = .310
00586>
00587> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00588>
00589>
00590> 002:0014-----
00591> # UNCONTROLLED AREA UNC-2
00592> #
00593>
00594>
00595> | DESIGN NASHYD | Area (ha)= 1.87 Curve Number (CN)=75.60
00596> | 09:UNC-2 DT= 1.00 | Ia (mm)= 4.670 # of Linear Res. (N)= 2.00
00597> | U.H. Tp(hrs)= .190
00598>
00599> Unit Hyd Qpeak (cms)= .255
00600>
00601> PEAK FLOW (cms)= .042 (i)
00602> TIME TO PEAK (hrs)= 6.083
00603> RUNOFF VOLUME (mm)= 11.860
00604> TOTAL RAINFALL (mm)= 42.340
00605> RUNOFF COEFFICIENT = .280
00606>
00607> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00608>
00609>
00610> 002:0015-----
00611> # UNCONTROLLED AREA UNC-3
00612> #
00613>
00614>
00615> | DESIGN STANDHYD | Area (ha)= .55
00616> | 08:UNC-3 DT= 1.00 | Total Imp(%)= 24.20 Dir. Conn.(%)= 13.30
00617>
00618> IMPERVIOUS PERVIOUS (i)
00619> Surface Area (ha)= .13 .42
00620> Dep. Storage (mm)= 1.57 4.67
00621> Average Slope (%)= 1.00 1.00
00622> Length (m)= 60.55 40.00
00623> Mannings n = .013 .250
00624>
00625> Max.eff.Inten.(mm/hr)= 36.24 15.51
00626> over (min) 3.00 21.00
00627> Storage Coeff. (min)= 2.84 (ii) 21.15 (iii)
00628> Unit Hyd. Tpeak (min)= 3.00 21.00
00629> Unit Hyd. peak (cms)= .39 .05
00630>
00631> PEAK FLOW (cms)= .01 .01 .013 (iii)
00632> TIME TO PEAK (hrs)= 6.00 6.23 6.017
00633> RUNOFF VOLUME (mm)= 40.77 4.82 9.597
00634> TOTAL RAINFALL (mm)= 42.34 42.34 42.340
00635> RUNOFF COEFFICIENT = .96 .11 .227
00636>
00637> (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
00638> Fo (mm/hr)= 76.20 K (1/hr)= 4.14
00639> Fc (mm/hr)= 13.20 Cum.Inf. (mm)= .00
00640> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
00641> THAN THE STORAGE COEFFICIENT.
00642> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00643>
00644>
00645> 002:0016-----
00646> # UNCONTROLLED AREA UNC-4
00647> #
00648>
00649>
00650> | DESIGN NASHYD | Area (ha)= 3.65 Curve Number (CN)=76.50
00651> | 07:UNC-4 DT= 1.00 | Ia (mm)= 4.670 # of Linear Res. (N)= 2.00
00652> | U.H. Tp(hrs)= .450
00653>
00654> Unit Hyd Qpeak (cms)= .211
00655>
00656> PEAK FLOW (cms)= .050 (i)
00657> TIME TO PEAK (hrs)= 6.533
00658> RUNOFF VOLUME (mm)= 12.265
00659> TOTAL RAINFALL (mm)= 42.340
00660> RUNOFF COEFFICIENT = .290
00661>
00662> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00663>
00664>
00665> 002:0017-----
00666>
00667> | ADD HYD (UNC ) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
00668> | (ha) (cms) (hrs) (mm) (cms)
00669> | I1 10:UNC-1 .96 .027 6.05 13.13 .000
00670> | +I2 09:UNC-2 1.87 .042 6.08 11.86 .000
00671> | +I3 08:UNC-3 .55 .013 6.02 9.60 .000
00672> | +I4 07:UNC-4 3.65 .050 6.53 12.26 .000
00673>
00674> SUM 04:UNC 7.03 .119 6.15 12.07 .000
00675>

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00676> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
00677>
00678>
00679> 002:0018-----
00680>
00681> 002:0002-----
00682> ** END OF RUN : 4
00683>
00684>
00685>
00686>
00687>
00688>
00689>
00690>
00691> | START | Project dir.: C:\SWMHYMO\
00692> | | Rainfall dir.: C:\SWMHYMO\
00693> | TZERO = .00 hrs on 0
00694> | METOUT= 2 (output = METRIC)
00695> | NRUN = 005
00696> | NSTORM= 1
00697> | # I=012SC5yr.stm
00698>
00699> 005:0002-----
00700> #
00701> * Project Name: [Derry Side Road Subdivision] Project Number: [160401279]
00702> * Date : 09-13-2017
00703> * Modeller : [AMP]
00704> * Company : Stantec Consulting Ltd. 604
00705> * License # : 3824306
00706> *
00707>
00708>
00709>
00710> | DEFAULT VALUES | Filename: C:\SWMHYMO\OTTAWA.VAL
00711> | | ICASEdv = 1 (read and print data)
00712> | | FileTitle= File comment: [2005 City of Ottawa Sewer Design Guideline]
00713> | | PARAMETERS USED IN THE DESIGN STANDHYD COMMAND FOR OTTAWA.
00714> | Horton's infiltration equation parameters:
00715> | [Fo= 76.20 mm/hr] [Fc=13.20 mm/hr] [DCAY= 4.14 /hr] [F= .00 mm]
00716> | Parameters for PERVIOUS surfaces in STANDHYD:
00717> | [IAPER= 4.67 mm] [LGP=40.00 m] [MNP=.250]
00718> | Parameters for IMPERVIOUS surfaces in STANDHYD:
00719> | [IAMP= 1.57 mm] [CLL= 1.50] [MNI=.013]
00720> | Parameters used in NASHYD:
00721> | [Ia= 4.67 mm] [N= 2.00]
00722>
00723> 005:0003-----
00724>
00725> | READ STORM | Filename: 5yr,12hr SCS STORM (Ottawa)
00726> | Ptotal= 56.17 mm | Comments: 5yr,12hr SCS STORM (Ottawa)
00727>
00728>
00729> | TIME RAIN | TIME RAIN | TIME RAIN | TIME RAIN
00730> | hrs mm/hr | hrs mm/hr | hrs mm/hr | hrs mm/hr
00731> | .50 1.685 | 3.50 2.247 | 6.50 12.245 | 9.50 1.685
00732> | 1.00 .786 | 4.00 2.247 | 7.00 5.392 | 10.00 1.348
00733> | 1.50 1.460 | 4.50 3.033 | 7.50 3.595 | 10.50 1.910
00734> | 2.00 1.460 | 5.00 3.820 | 8.00 3.146 | 11.00 1.236
00735> | 2.50 1.910 | 5.50 6.066 | 8.50 2.471 | 11.50 1.123
00736> | 3.00 1.685 | 6.00 48.082 | 9.00 2.584 | 12.00 1.123
00737>
00738>
00739> #
00740> #
00741> * DERRY SIDE ROAD SUBDIVISION - POST DEVELOPMENT CONDITIONS
00742> #
00743> # STORM: 12hr SCS Storms, 3hr Chicago Storms
00744> # City of Ottawa 2004 IDF Parameters
00745> #
00746> # - Average CN values for each catchment were initially calculated on typical
00747> # AMC II conditions based on hydrologic soil group and land use. CN values
00748> # were subsequently modified using the SCS Modified Curve Number Calculations
00749> # - Soils information for the site area was obtained from exp's
00750> # Geotechnical Investigation dated July 21, 2017.
00751> # - CN values calculated based on lawns, woodland and impervious areas
00752> # - NASHYD command used for catchments with TIMP<20%
00753> # - Time to peak for each catchment was estimated based on Tp = 0.67*Tc and
00754> # Tc values were calculated using the Uplands Method
00755> #
00756> * AREA A1 TO SWM 1
00757> #
00758>
00759> | DESIGN NASHYD | Area (ha)= 1.73 Curve Number (CN)=79.20
00760> | 01:A1 DT= 1.00 | Ia (mm)= 4.670 # of Linear Res. (N)= 2.00
00761> | U.H. Tp(hrs)= .230
00762>
00763> Unit Hyd Qpeak (cms)= .195
00764>
00765> PEAK FLOW (cms)= .068 (i)
00766> TIME TO PEAK (hrs)= 6.117
00767> RUNOFF VOLUME (mm)= 22.437
00768> TOTAL RAINFALL (mm)= 56.170
00769> RUNOFF COEFFICIENT = .399
00770>
00771> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00772>
00773>
00774> 005:0005-----
00775> #
00776> * AREA A2 TO SWM 1
00777> #
00778>
00779> | DESIGN NASHYD | Area (ha)= 1.88 Curve Number (CN)=78.30
00780> | 02:A2 DT= 1.00 | Ia (mm)= 4.670 # of Linear Res. (N)= 2.00
00781> | U.H. Tp(hrs)= .280
00782>
00783> Unit Hyd Qpeak (cms)= .174
00784>
00785> PEAK FLOW (cms)= .063 (i)
00786> TIME TO PEAK (hrs)= 6.183
00787> RUNOFF VOLUME (mm)= 21.759
00788> TOTAL RAINFALL (mm)= 56.170
00789> RUNOFF COEFFICIENT = .387
00790>
00791> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00792>
00793>
00794> 005:0006-----
00795>
00796> | ADD HYD (TOSWM1 ) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
00797> | (ha) (cms) (hrs) (mm) (cms)
00798> | I1 01:A1 1.73 .068 6.12 22.44 .000
00799> | +I2 02:A2 1.88 .063 6.18 21.76 .000
00800>
00801> SUM 06:TOSWM1 3.61 .131 6.15 22.08 .000
00802>
00803> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
00804>
00805>
00806> 005:0007-----
00807>
00808> | COMPUTE VOLUME |
00809> | ID:06 (TOSWM1) | DISCHARGE TIME
00810> | (cms) (hrs)

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00811> *** WARNING: No storage required, RelRate > Inflow Qp.
00812> -----
00813> 005:0008 *****
00814> #*****
00815> #* AREA A3 TO SWM 2
00816> #*****
00817> | DESIGN NASHYD | Area (ha)= 1.33 Curve Number (CN)=78.30
00819> | 01:A3 DT= 1.00 | Ia (mm)= 4.670 # of Linear Res.(N)= 2.00
00820> -----
00821> U.H. Tp(hrs)= .180
00822> Unit Hyd Qpeak (cms)= .192
00823> PEAK FLOW (cms)= .059 (i)
00825> TIME TO PEAK (hrs)= 6.067
00826> RUNOFF VOLUME (mm)= 21.758
00827> TOTAL RAINFALL (mm)= 56.170
00828> RUNOFF COEFFICIENT = .387
00829> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00830> -----
00831> 005:0009 *****
00832> #*****
00833> #* AREA A4 TO SWM 2
00834> #*****
00835> | DESIGN NASHYD | Area (ha)= 2.71 Curve Number (CN)=78.30
00839> | 02:A4 DT= 1.00 | Ia (mm)= 4.670 # of Linear Res.(N)= 2.00
00840> -----
00841> U.H. Tp(hrs)= .180
00842> Unit Hyd Qpeak (cms)= .391
00843> PEAK FLOW (cms)= .119 (i)
00845> TIME TO PEAK (hrs)= 6.067
00846> RUNOFF VOLUME (mm)= 21.759
00847> TOTAL RAINFALL (mm)= 56.170
00848> RUNOFF COEFFICIENT = .387
00849> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00850> -----
00851> 005:0010 *****
00852> #*****
00853> #* AREA A5 TO SWM 2
00854> #*****
00855> | DESIGN NASHYD | Area (ha)= 1.43 Curve Number (CN)=78.30
00859> | 03:A5 DT= 1.00 | Ia (mm)= 4.670 # of Linear Res.(N)= 2.00
00860> -----
00861> U.H. Tp(hrs)= .250
00862> Unit Hyd Qpeak (cms)= .148
00863> PEAK FLOW (cms)= .052 (i)
00865> TIME TO PEAK (hrs)= 6.150
00866> RUNOFF VOLUME (mm)= 21.758
00867> TOTAL RAINFALL (mm)= 56.170
00868> RUNOFF COEFFICIENT = .387
00869> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00870> -----
00871> 005:0011 *****
00872> | ADD HYD (TOSWM2 ) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
00876> (ha) (cms) (hrs) (mm) (cms)
00877> ID1 01:A3 1.33 .059 6.07 21.76 .000
00878> +ID2 02:A4 2.71 .119 6.07 21.76 .000
00879> +ID3 03:A5 1.43 .052 6.15 21.76 .000
00880> -----
00881> SUM 05:TOSWM2 5.47 .228 6.08 21.76 .000
00882> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
00883> -----
00884> 005:0012 *****
00885> #*****
00886> | COMPUTE VOLUME | DISCHARGE TIME
00889> (cms) (hrs)
00891> START CONTROLLING AT .022 5.563
00892> INFLOW HYD. PEAKS AT .228 6.083
00893> STOP CONTROLLING AT .185 6.315
00894> REQUIRED STORAGE VOLUME (ha.m.)= .0135
00896> TOTAL HYDROGRAPH VOLUME (ha.m.)= .1190
00897> % OF HYDROGRAPH TO STORE = 11.3729
00898> NOTE: Storage was computed to reduce the Inflow
00900> peak to .185 (cms).
00901> -----
00902> 005:0015 *****
00903> #*****
00904> #* UNCONTROLLED AREA UNC-1
00905> #*****
00906> | DESIGN NASHYD | Area (ha)= .96 Curve Number (CN)=78.30
00909> | 10:UNC-1 DT= 1.00 | Ia (mm)= 4.670 # of Linear Res.(N)= 2.00
00910> -----
00911> U.H. Tp(hrs)= .160
00912> Unit Hyd Qpeak (cms)= .156
00913> PEAK FLOW (cms)= .045 (i)
00915> TIME TO PEAK (hrs)= 6.050
00916> RUNOFF VOLUME (mm)= 21.758
00917> TOTAL RAINFALL (mm)= 56.170
00918> RUNOFF COEFFICIENT = .387
00919> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00920> -----
00921> 005:0014 *****
00922> #*****
00923> #* UNCONTROLLED AREA UNC-2
00924> #*****
00925> | DESIGN NASHYD | Area (ha)= 1.87 Curve Number (CN)=75.60
00929> | 09:UNC-2 DT= 1.00 | Ia (mm)= 4.670 # of Linear Res.(N)= 2.00
00930> -----
00931> U.H. Tp(hrs)= .190
00932> Unit Hyd Qpeak (cms)= .255
00933> PEAK FLOW (cms)= .072 (i)
00935> TIME TO PEAK (hrs)= 6.083
00936> RUNOFF VOLUME (mm)= 19.870
00937> TOTAL RAINFALL (mm)= 56.170
00938> RUNOFF COEFFICIENT = .354
00939> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00940> -----
00941> 005:0015 *****
00942> #*****
00943> #* UNCONTROLLED AREA UNC-3
00944> #*****
00945> #*****

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00946> #*****
00947> DESIGN STANDARD | Area (ha)= .55
00949> | 08:UNC-3 DT= 1.00 | Total Imp(%)= 24.20 Dir. Conn.(%)= 13.30
00950> -----
00951> IMPERVIOUS PERVIOUS (i)
00952> Surface Area (ha)= .13 .42
00953> Dep. Storage (mm)= 1.57 4.67
00954> Average Slope (%)= 1.00 1.00
00955> Length (m)= 60.55 40.00
00956> Mannings n = .013 .250
00957> Max. eff. Inten. (mm/hr)= 48.08 34.90
00958> over (min) = 3.00 16.00
00960> Storage Coeff. (min)= 2.53 (ii) 15.77 (ii)
00961> Unit Hyd. Tpeak (min)= 3.00 16.00
00962> Unit Hyd. peak (cms)= .42 .07
00963> PEAK FLOW (cms)= .01 .03 *TOTALS*
00965> TIME TO PEAK (hrs)= 5.97 6.10 6.017
00966> RUNOFF VOLUME (mm)= 54.60 12.76 18.322
00967> TOTAL RAINFALL (mm)= 56.17 56.17 56.170
00968> RUNOFF COEFFICIENT = .97 .23 .326
00969> (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
00971> Fo (mm/hr)= 76.20 K (1/hr)= 4.14
00972> Fc (mm/hr)= 13.20 Cum. Inf. (mm)= .00
00974> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
00975> THAN THE STORAGE COEFFICIENT.
00976> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00977> -----
00978> 005:0016 *****
00979> #*****
00980> #* UNCONTROLLED AREA UNC-4
00981> #*****
00982> | DESIGN NASHYD | Area (ha)= 3.65 Curve Number (CN)=76.50
00984> | 07:UNC-4 DT= 1.00 | Ia (mm)= 4.670 # of Linear Res.(N)= 2.00
00985> -----
00986> U.H. Tp(hrs)= .450
00987> Unit Hyd Qpeak (cms)= .211
00988> PEAK FLOW (cms)= .086 (i)
00990> TIME TO PEAK (hrs)= 6.500
00991> RUNOFF VOLUME (mm)= 20.476
00992> TOTAL RAINFALL (mm)= 56.170
00993> RUNOFF COEFFICIENT = .365
00994> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00995> -----
00996> 100:0002 *****
00997> | ADD HYD (UNC ) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
01001> (ha) (cms) (hrs) (mm) (cms)
01002> ID1 10:UNC-1 .96 .045 6.05 21.76 .000
01003> +ID2 09:UNC-2 1.87 .072 6.08 19.87 .000
01004> +ID3 08:UNC-3 .55 .034 6.02 18.32 .000
01005> +ID4 07:UNC-4 3.65 .086 6.50 20.48 .000
01006> -----
01007> SUM 04:UNC 7.03 .216 6.12 20.32 .000
01008> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
01009> -----
01010> 005:0018 *****
01011> ** END OF RUN : 99
01012> -----
01013> 005:0002 *****
01014> ** END OF RUN : 99
01015> -----
01016> 005:0002 *****
01017> ** END OF RUN : 99
01018> -----
01019> 100:0002 *****
01020> #*****
01021> | START | Project dir.: C:\SWMHYMO\
01027> | Rainfall dir.: C:\SWMHYMO\
01028> TZERO = .00 hrs on
01029> METOUT= 2 (output = METRIC)
01030> NRUN = 100
01031> NSTORM= 1
01032> # i=012SChyr.stm
01033> -----
01034> 100:0002 *****
01035> #*****
01036> #* Project Name: [Derry Side Road Subdivision] Project Number: [160401279]
01037> #* Date : 09-13-2017
01038> #* Modeller : [AMP]
01039> #* Stationer : Stantec Consulting Ltd. 604
01040> #* License # : 3824306
01041> #*****
01042> -----
01043> 100:0002 *****
01044> #*****
01045> | DEFAULT VALUES | Filename: C:\SWMHYMO\OTTAWA.VAL
01046> | ICASEdv = 1 (read and print data)
01047> FileTitle= File comment: [2005 City of Ottawa Sewer Design Guideline]
01048> PARAMETERS USED IN THE DESIGN STANDHYD COMMAND FOR OTTAWA.
01049> Horton's infiltration equation parameters:
01050> [Fo= 76.20 mm/hr] [Fc=13.20 mm/hr] [DCAY= 4.14 /hr] [F= .00 mm]
01051> Parameters for PERVIOUS surfaces in STANDHYD:
01052> [IAPER= 4.67 mm] [LGP=40.00 m] [MNP= .250]
01053> Parameters for IMPERVIOUS surfaces in STANDHYD:
01054> [IAIMP= 1.57 mm] [CLL= 1.50] [MNI= .013]
01055> Parameters used in NASHYD:
01056> [Ia= 4.67 mm] [N= 2.00]
01057> -----
01058> 100:0003 *****
01059> #*****
01060> | READ STORM | Filename: 100yr,12hr SCS STORM (Ottawa)
01061> | Ptotal= 96.00 mm | Comments: 100yr,12hr SCS STORM (Ottawa)
01062> -----
01063> TIME RAIN | TIME RAIN | TIME RAIN | TIME RAIN
01064> hrs mm/hr | hrs mm/hr | hrs mm/hr | hrs mm/hr
01065> .50 2.880 | 3.50 3.840 | 6.50 20.928 | 9.50 2.880
01066> 1.00 1.344 | 4.00 3.840 | 7.00 9.216 | 10.00 2.304
01067> 1.50 2.496 | 4.50 5.184 | 7.50 6.144 | 10.50 3.264
01068> 2.00 2.496 | 5.00 6.528 | 8.00 5.376 | 11.00 2.112
01069> 2.50 3.264 | 5.50 10.368 | 8.50 4.224 | 11.50 3.920
01070> 3.00 2.880 | 6.00 82.176 | 9.00 4.416 | 12.00 1.920
01071> -----
01072> 100:0004 *****
01073> #*****
01074> #* DERRY SIDE ROAD SUBDIVISION - POST DEVELOPMENT CONDITIONS
01075> #*
01076> #*
01077> #* STORM: 12hr SCS Storms, 3hr Chicago Storms
01078> #* City of Ottawa 2004 IDF Parameters
01079> #*
01080> #*

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01081> *# - Average CN values for each catchment were initially calculated on typical
01082> *# AMC II conditions based on hydrologic soil group and land use. CN values
01083> *# were subsequently modified using the SCS Modified Curve Number Calculations
01084> *# - Soils information for the site area was obtained from exp's
01085> *# Geotechnical Investigation dated July 21, 2017.
01086> *# - CN values calculated based on lawns, woodland and impervious areas
01087> *# - NASHVD command used for catchments with TIMP<200
01088> *# - Time to peak for each catchment was estimated based on Tp = 0.67*Tc and
01089> *# - Tc values were calculated using the Uplands Method
01090> *#-----
01091> *# AREA A1 TO SWM 1
01092> *#-----
01093> *#-----
01094> | DESIGN NASHVD | Area (ha)= 1.73 Curve Number (CN)=79.20
01095> | 01:A1 DT= 1.00 | Ia (mm)= 4.670 # of Linear Res. (N)= 2.00
01096> | U.H. Tp(hrs)= .230
01097>
01098> Unit Hyd Qpeak (cms)= .195
01099>
01100> PEAK FLOW (cms)= .166 (i)
01101> TIME TO PEAK (hrs)= 6.100
01102> RUNOFF VOLUME (mm)= 52.780
01103> TOTAL RAINFALL (mm)= 96.000
01104> RUNOFF COEFFICIENT = .550
01105>
01106> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
01107>
01108>-----
01109> 100:0005-----
01110> *#-----
01111> *# AREA A2 TO SWM 1
01112> *#-----
01113> *#-----
01114> | DESIGN NASHVD | Area (ha)= 1.88 Curve Number (CN)=78.30
01115> | 02:A2 DT= 1.00 | Ia (mm)= 4.670 # of Linear Res. (N)= 2.00
01116> | U.H. Tp(hrs)= .280
01117>
01118> Unit Hyd Qpeak (cms)= .174
01119>
01120> PEAK FLOW (cms)= .155 (i)
01121> TIME TO PEAK (hrs)= 6.167
01122> RUNOFF VOLUME (mm)= 51.577
01123> TOTAL RAINFALL (mm)= 96.000
01124> RUNOFF COEFFICIENT = .537
01125>
01126> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
01127>
01128>-----
01129> 100:0006-----
01130> *#-----
01131> | ADD HYD (TOSW1 ) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
01132> |-----|-----|-----|-----|-----|-----|
01133> | 01:A1 | 1.73 | .166 | 6.10 | 52.78 | .000
01134> | +D2 02:A2 | 1.88 | .155 | 6.17 | 51.58 | .000
01135> |-----|-----|-----|-----|-----|-----|
01136> | SUM 06:TOSW1 | 3.61 | .320 | 6.13 | 52.15 | .000
01137>
01138> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
01139>
01140>-----
01141> 100:0007-----
01142> *#-----
01143> | COMPUTE VOLUME | DISCHARGE TIME
01144> | ID:06 (TOSW1) | (cms) (hrs)
01145>-----|-----|-----|
01146> | START CONTROLLING AT | .028 | 5.513
01147> | INFLOW HYD. PEAKS AT | .320 | 6.133
01148> | STOP CONTROLLING AT | .185 | 6.738
01149>
01150> REQUIRED STORAGE VOLUME (ha.m.)= .0494
01151> TOTAL HYDROGRAPH VOLUME (ha.m.)= .1883
01152> % OF HYDROGRAPH TO STORE = 26.2343
01153>
01154> NOTE: Storage was computed to reduce the Inflow
01155> peak to .185 (cms).
01156>
01157>-----
01158> 100:0008-----
01159> *#-----
01160> *# AREA A3 TO SWM 2
01161> *#-----
01162> *#-----
01163> | DESIGN NASHVD | Area (ha)= 1.33 Curve Number (CN)=78.30
01164> | 01:A3 DT= 1.00 | Ia (mm)= 4.670 # of Linear Res. (N)= 2.00
01165> | U.H. Tp(hrs)= .180
01166>
01167> Unit Hyd Qpeak (cms)= .192
01168>
01169> PEAK FLOW (cms)= .143 (i)
01170> TIME TO PEAK (hrs)= 6.050
01171> RUNOFF VOLUME (mm)= 51.576
01172> TOTAL RAINFALL (mm)= 96.000
01173> RUNOFF COEFFICIENT = .537
01174>
01175> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
01176>
01177>-----
01178> 100:0009-----
01179> *#-----
01180> *# AREA A4 TO SWM 2
01181> *#-----
01182> *#-----
01183> | DESIGN NASHVD | Area (ha)= 2.71 Curve Number (CN)=78.30
01184> | 02:A4 DT= 1.00 | Ia (mm)= 4.670 # of Linear Res. (N)= 2.00
01185> | U.H. Tp(hrs)= .180
01186>
01187> Unit Hyd Qpeak (cms)= .391
01188>
01189> PEAK FLOW (cms)= .291 (i)
01190> TIME TO PEAK (hrs)= 6.050
01191> RUNOFF VOLUME (mm)= 51.577
01192> TOTAL RAINFALL (mm)= 96.000
01193> RUNOFF COEFFICIENT = .537
01194>
01195> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
01196>
01197>-----
01198> 100:0010-----
01199> *#-----
02000> *# AREA A5 TO SWM 2
02001> *#-----
02002> *#-----
02003> | DESIGN NASHVD | Area (ha)= 1.43 Curve Number (CN)=78.30
02004> | 03:A5 DT= 1.00 | Ia (mm)= 4.670 # of Linear Res. (N)= 2.00
02005> | U.H. Tp(hrs)= .250
02006>
02007> Unit Hyd Qpeak (cms)= .148
02008>
02009> PEAK FLOW (cms)= .127 (i)
02010> TIME TO PEAK (hrs)= 6.133
02011> RUNOFF VOLUME (mm)= 51.577
02012> TOTAL RAINFALL (mm)= 96.000
02013> RUNOFF COEFFICIENT = .537
02014>
02015> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

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02126>-----
02127> 100:0011-----
02128> *#-----
02129> | ADD HYD (TOSW2 ) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
02130> |-----|-----|-----|-----|-----|-----|
02131> | ID1 01:A3 | 1.33 | .143 | 6.05 | 51.58 | .000
02132> | +D2 02:A4 | 2.71 | .291 | 6.05 | 51.58 | .000
02133> | +D3 03:A5 | 1.43 | .127 | 6.13 | 51.58 | .000
02134> |-----|-----|-----|-----|-----|-----|
02135> | SUM 05:TOSW2 | 5.47 | .559 | 6.07 | 51.58 | .000
02136>
02137> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
02138>
02139>-----
02140> 100:0012-----
02141> *#-----
02142> | COMPUTE VOLUME | DISCHARGE TIME
02143> | ID:05 (TOSW2) | (cms) (hrs)
02144>-----|-----|-----|
02145> | START CONTROLLING AT | .044 | 5.502
02146> | INFLOW HYD. PEAKS AT | .559 | 6.067
02147> | STOP CONTROLLING AT | .185 | 6.884
02148>
02149> REQUIRED STORAGE VOLUME (ha.m.)= .1106
02150> TOTAL HYDROGRAPH VOLUME (ha.m.)= .2821
02151> % OF HYDROGRAPH TO STORE = 39.2112
02152>
02153> NOTE: Storage was computed to reduce the Inflow
02154> peak to .185 (cms).
02155>
02156>-----
02157> 100:0013-----
02158> *#-----
02159> *# UNCONTROLLED AREA UNC-1
02160> *#-----
02161> | AREA (ha)= .96 Curve Number (CN)=78.30
02162> | 10:UNC-1 DT= 1.00 | Ia (mm)= 4.670 # of Linear Res. (N)= 2.00
02163> | U.H. Tp(hrs)= .160
02164>
02165> Unit Hyd Qpeak (cms)= .156
02166>
02167> PEAK FLOW (cms)= .109 (i)
02168> TIME TO PEAK (hrs)= 6.033
02169> RUNOFF VOLUME (mm)= 51.576
02170> TOTAL RAINFALL (mm)= 96.000
02171> RUNOFF COEFFICIENT = .537
02172>
02173> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
02174>
02175>-----
02176> 100:0014-----
02177> *#-----
02178> *# UNCONTROLLED AREA UNC-2
02179> *#-----
02180> | AREA (ha)= 1.87 Curve Number (CN)=75.60
02181> | 09:UNC-2 DT= 1.00 | Ia (mm)= 4.670 # of Linear Res. (N)= 2.00
02182> | U.H. Tp(hrs)= .190
02183>
02184> Unit Hyd Qpeak (cms)= .255
02185>
02186> PEAK FLOW (cms)= .181 (i)
02187> TIME TO PEAK (hrs)= 6.067
02188> RUNOFF VOLUME (mm)= 48.129
02189> TOTAL RAINFALL (mm)= 96.000
02190> RUNOFF COEFFICIENT = .501
02191>
02192> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
02193>
02194>-----
02195> 100:0015-----
02196> *#-----
02197> *# UNCONTROLLED AREA UNC-3
02198> *#-----
02199> | AREA (ha)= .55
02200> | 08:UNC-3 DT= 1.00 | Total Imp(%)= 24.20 Dir. Conn.(%)= 13.30
02201>
02202> IMPERVIOUS PERVIOUS (i)
02203> Surface Area (ha)= .13 .42
02204> Dep. Storage (mm)= 1.57 4.67
02205> Average Slope (%)= 1.00 1.00
02206> Length (m)= 60.55 40.00
02207> Mannings n = .013 .250
02208>
02209> Max. eff. Inten. (mm/hr)= 82.18 79.52
02210> over (min) 2.00 12.00
02211> Storage Coeff. (min)= 2.05 (ii) 11.57 (ii)
02212> Unit Hyd. Tpeak (min)= 2.00 12.00
02213> Unit Hyd. peak (cms)= .55 .10
02214>
02215> PEAK FLOW (cms)= .02 .08 *TOTALS*
02216> TIME TO PEAK (hrs)= 5.90 6.03 (iii)
02217> RUNOFF VOLUME (mm)= 94.43 38.67 46.082
02218> TOTAL RAINFALL (mm)= 96.00 96.00 96.000
02219> RUNOFF COEFFICIENT = .98 .40 .480
02220>
02221> (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
02222> Fo (mm/hr)= 76.20 K (1/hr)= 4.14
02223> Fc (mm/hr)= 13.20 Cum. Inf. (mm)= .00
02224> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
02225> THAN THE STORAGE COEFFICIENT.
02226> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
02227>
02228>-----
02229> 100:0016-----
02230> *#-----
02231> *# UNCONTROLLED AREA UNC-4
02232> *#-----
02233> | AREA (ha)= 3.65 Curve Number (CN)=76.50
02234> | 07:UNC-4 DT= 1.00 | Ia (mm)= 4.670 # of Linear Res. (N)= 2.00
02235> | U.H. Tp(hrs)= .450
02236>
02237> Unit Hyd Qpeak (cms)= .211
02238>
02239> PEAK FLOW (cms)= .212 (i)
02240> TIME TO PEAK (hrs)= 6.450
02241> RUNOFF VOLUME (mm)= 49.252
02242> TOTAL RAINFALL (mm)= 96.000
02243> RUNOFF COEFFICIENT = .513
02244>
02245> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
02246>
02247>-----
02248> 100:0017-----
02249> *#-----
02250> | ADD HYD (UNC ) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
02251> |-----|-----|-----|-----|-----|-----|
02252> | ID1 10:UNC-1 | .96 | .109 | 6.03 | 51.58 | .000
02253> | +D2 09:UNC-2 | 1.87 | .181 | 6.07 | 48.13 | .000
02254> | +D3 08:UNC-3 | .55 | .095 | 6.00 | 46.08 | .000
02255> | +D4 07:UNC-4 | 3.65 | .212 | 6.45 | 49.25 | .000

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01351>
01352>
01353>
01354> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
01355>
01356>
01357> 100:0018-----
01358>
01359> 100:0002-----
01360>
01361> 100:0002-----
01362>
01363> 100:0002-----
01364> ** END OF RUN : 101
01365>
01366>
01367>
01368>
01369>
01370>
01371>
01372>
01373> | START | Project dir.: C:\SWMHYMO\
01374> | Rainfall dir.: C:\SWMHYMO\
01375> | TZERO = .00 hrs on 0
01376> | METOUT= 2 (output = METRIC)
01377> | NRUN = 102
01378> | NSTORM= 1
01379> | # 1=OT3CH2yr.stm
01380>
01381> 102:0002-----
01382> *****
01383> *# Project Name: [Derry Side Road Subdivision] Project Number: [160401279]
01384> *# Date : 09-13-2017
01385> *# Modeller : [AMF]
01386> *# Company : Stantec Consulting Ltd. 604
01387> *# License # : 3824306
01388> *****
01389>
01390> 102:0002-----
01391>
01392> | DEFAULT VALUES | Filename: C:\SWMHYMO\OTTAWA.VAL
01393> | ICASEd= 1 (read and print data)
01394> | FileTitle= File comment: [2005 City of Ottawa Sewer Design Guideline]
01395> | PARAMETERS USED IN THE DESIGN STANDHYD COMMAND FOR OTTAWA.
01396> | Horton's infiltration equation parameters:
01397> | [Fo= 76.20 mm/hr] [Foc=13.20 mm/hr] [DCAV= 4.14 /hr] [F= .00 mm]
01398> | Parameters for IMPERVIOUS surfaces in STANDHYD:
01399> | [IAPER= 4.67 mm] [LGP=40.00 m] [MNP=.250]
01400> | Parameters for IMPERVIOUS surfaces in STANDHYD:
01401> | [Iaimp= 1.57 mm] [CL= 1.50] [MNI= .013]
01402> | Parameters used in NASHYD:
01403> | [Ia= 4.67 mm] [N= 2.00]
01404>
01405> 102:0003-----
01406>
01407> | READ STORM | Filename: 2yr CHICAGO STORM, 3hr, DT=10min
01408> | Ptotal= 31.86 mm | Comments: 2yr CHICAGO STORM, 3hr, DT=10min
01409>
01410>
01411>
01412>
01413>
01414>
01415>
01416>
01417>
01418>
01419> 102:0004-----
01420> *****
01421> *#
01422> *# DERRY SIDE ROAD SUBDIVISION - POST DEVELOPMENT CONDITIONS
01423> *****
01424> *# STORM: 12hr SCS Storms, 3hr Chicago Storms
01425> *# City of Ottawa 2004 IDF Parameters
01426> *#
01427> *# - Average CN values for each catchment were initially calculated on typical
01428> *# AMC II conditions based on hydrologic soil group and land use. CN values
01429> *# were subsequently modified using the SCS Modified Curve Number Calculations
01430> *# - Soils information for the site area was obtained from exp's
01431> *# Geotechnical Investigation dated July 21, 2017.
01432> *# - CN values calculated based on lawns, woodland and impervious areas
01433> *# - NASHYD command used for catchments with TIME<208
01434> *# - Time to peak for each catchment was estimated based on Tp = 0.67*Tc and
01435> *# Tc values were calculated using the Uplands Method
01436> *****
01437> *# AREA A1 TO SWM 1
01438> *****
01439>
01440> | DESIGN NASHYD | Area (ha)= 1.73 Curve Number (CN)=79.20
01441> | 01:A1 DT= 1.00 | Ia (mm)= 4.670 # of Linear Res. (N)= 2.00
01442> | U.H. Tp(hrs)= .230
01443>
01444> Unit Hyd Qpeak (cms)= 7.195
01445>
01446> PEAK FLOW (cms)= .031 (i)
01447> TIME TO PEAK (hrs)= 1.350
01448> RUNOFF VOLUME (mm)= 7.873
01449> TOTAL RAINFALL (mm)= 31.860
01450> RUNOFF COEFFICIENT = .247
01451>
01452> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
01453>
01454>
01455> 102:0005-----
01456> *****
01457> *# AREA A2 TO SWM 1
01458> *****
01459>
01460> | DESIGN NASHYD | Area (ha)= 1.88 Curve Number (CN)=78.30
01461> | 02:A2 DT= 1.00 | Ia (mm)= 4.670 # of Linear Res. (N)= 2.00
01462> | U.H. Tp(hrs)= .280
01463>
01464> Unit Hyd Qpeak (cms)= .174
01465>
01466> PEAK FLOW (cms)= .028 (i)
01467> TIME TO PEAK (hrs)= 1.433
01468> RUNOFF VOLUME (mm)= 7.873
01469> TOTAL RAINFALL (mm)= 31.860
01470> RUNOFF COEFFICIENT = .238
01471>
01472> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
01473>
01474>
01475> 102:0006-----
01476>
01477> | ADD HYD (TOSW1) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
01478> | ID1 01:A1 | (ha) (cms) (hrs) (mm) (cms)
01479> | +ID2 02:A2 | 1.73 .031 1.35 7.87 .000
01480> | +ID2 02:A2 | 1.88 .028 1.43 7.58 .000
01481> |
01482> | SUM 06:TOSW1 | 3.61 .058 1.38 7.72 .000
01483>
01484> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
01485>

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01486>-----
01487> 102:0007-----
01488>
01489> | COMPUTE VOLUME |
01490> | ID:06 (TOSW1) | DISCHARGE TIME
01491> | (cms) (hrs)
01492> *** WARNING: No storage required, RelRate > Inflow Qp.
01493>
01494> 102:0008-----
01495> *****
01496> *# AREA A3 TO SWM 2
01497> *****
01498>
01499> | DESIGN NASHYD | Area (ha)= 1.33 Curve Number (CN)=78.30
01500> | 01:A3 DT= 1.00 | Ia (mm)= 4.670 # of Linear Res. (N)= 2.00
01501> | U.H. Tp(hrs)= .180
01502>
01503> Unit Hyd Qpeak (cms)= .192
01504>
01505> PEAK FLOW (cms)= .026 (i)
01506> TIME TO PEAK (hrs)= 1.250
01507> RUNOFF VOLUME (mm)= 7.576
01508> TOTAL RAINFALL (mm)= 31.860
01509> RUNOFF COEFFICIENT = .238
01510>
01511> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
01512>
01513>
01514> 102:0009-----
01515> *****
01516> *# AREA A4 TO SWM 2
01517> *****
01518>
01519> | DESIGN NASHYD | Area (ha)= 2.71 Curve Number (CN)=78.30
01520> | 02:A4 DT= 1.00 | Ia (mm)= 4.670 # of Linear Res. (N)= 2.00
01521> | U.H. Tp(hrs)= .180
01522>
01523> Unit Hyd Qpeak (cms)= .391
01524>
01525> PEAK FLOW (cms)= .053 (i)
01526> TIME TO PEAK (hrs)= 1.250
01527> RUNOFF VOLUME (mm)= 7.576
01528> TOTAL RAINFALL (mm)= 31.860
01529> RUNOFF COEFFICIENT = .238
01530>
01531> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
01532>
01533>
01534> 102:0010-----
01535> *****
01536> *# AREA A5 TO SWM 2
01537> *****
01538>
01539> | DESIGN NASHYD | Area (ha)= 1.43 Curve Number (CN)=78.30
01540> | 03:A5 DT= 1.00 | Ia (mm)= 4.670 # of Linear Res. (N)= 2.00
01541> | U.H. Tp(hrs)= .250
01542>
01543> Unit Hyd Qpeak (cms)= .148
01544>
01545> PEAK FLOW (cms)= .023 (i)
01546> TIME TO PEAK (hrs)= 1.383
01547> RUNOFF VOLUME (mm)= 7.576
01548> TOTAL RAINFALL (mm)= 31.860
01549> RUNOFF COEFFICIENT = .238
01550>
01551> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
01552>
01553>
01554> 102:0011-----
01555> *****
01556> | ADD HYD (TOSW2) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
01557> | ID1 01:A3 | (ha) (cms) (hrs) (mm) (cms)
01558> | +ID2 02:A4 | 1.33 .026 1.25 7.58 .000
01559> | +ID2 02:A4 | 2.71 .053 1.25 7.58 .000
01560> | +ID3 03:A5 | 1.43 .023 1.38 7.58 .000
01561> |
01562> | SUM 05:TOSW2 | 5.47 .101 1.28 7.58 .000
01563>
01564> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
01565>
01566>
01567> 102:0012-----
01568>
01569> | COMPUTE VOLUME |
01570> | ID:05 (TOSW2) | DISCHARGE TIME
01571> | (cms) (hrs)
01572> *** WARNING: No storage required, RelRate > Inflow Qp.
01573>
01574> 102:0013-----
01575> *****
01576> *# UNCONTROLLED AREA UNC-1
01577> *****
01578>
01579> | DESIGN NASHYD | Area (ha)= .96 Curve Number (CN)=78.30
01580> | 10:UNC-1 DT= 1.00 | Ia (mm)= 4.670 # of Linear Res. (N)= 2.00
01581> | U.H. Tp(hrs)= .160
01582>
01583> Unit Hyd Qpeak (cms)= .156
01584>
01585> PEAK FLOW (cms)= .020 (i)
01586> TIME TO PEAK (hrs)= 1.217
01587> RUNOFF VOLUME (mm)= 7.576
01588> TOTAL RAINFALL (mm)= 31.860
01589> RUNOFF COEFFICIENT = .238
01590>
01591> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
01592>
01593>
01594> 102:0014-----
01595> *****
01596> *# UNCONTROLLED AREA UNC-2
01597> *****
01598>
01599> | DESIGN NASHYD | Area (ha)= 1.87 Curve Number (CN)=75.60
01600> | 09:UNC-2 DT= 1.00 | Ia (mm)= 4.670 # of Linear Res. (N)= 2.00
01601> | U.H. Tp(hrs)= .190
01602>
01603> Unit Hyd Qpeak (cms)= .255
01604>
01605> PEAK FLOW (cms)= .031 (i)
01606> TIME TO PEAK (hrs)= 1.283
01607> RUNOFF VOLUME (mm)= 6.772
01608> TOTAL RAINFALL (mm)= 31.860
01609> RUNOFF COEFFICIENT = .213
01610>
01611> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
01612>
01613>
01614> 102:0015-----
01615> *****
01616> *# UNCONTROLLED AREA UNC-3
01617> *****
01618>
01619> | DESIGN STANDHYD | Area (ha)= .55
01620> | 08:UNC-3 DT= 1.00 | Total Imp(%)= 24.20 Dir. Conn.(%)= 13.30

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01621> -----
01622> Surface Area (ha)= 1.13 IMPERVIOUS PERVIOUS (i)
01623> Dep. Storage (mm)= 1.57 4.67
01625> Average Slope (%)= 1.00 1.00
01626> Length (m)= 60.55 40.00
01627> Mannings n = .013 .250
01628>
01629> Max.eff.Inten.(mm/hr)= 76.80 18.20
01630> over (min) 2.00 19.00
01631> Storage Coeff. (min)= 2.10 (ii) 19.28 (iii)
01632> Unit Hyd. Tpeak (min)= 2.00 19.00
01633> Unit Hyd. peak (cms)= .54 .06
01634>
01635> PEAK FLOW (cms)= .02 .01 .019 (iii)
01636> TIME TO PEAK (hrs)= 1.00 1.25 1.000
01637> RUNOFF VOLUME (mm)= 30.29 5.04 8.397
01638> TOTAL RAINFALL (mm)= 31.86 31.86 31.860
01639> RUNOFF COEFFICIENT = .95 .16 .264
01640>
01641> (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
01642> Fo (mm/hr)= 76.20 K (1/hr)= 4.14
01643> Fc (mm/hr)= 13.20 Cum.Inf. (mm)= .00
01644> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
01645> THAN THE STORAGE COEFFICIENT.
01646> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
01647>
01648> -----
01649> 102:0016-----
01650> *****
01651> # UNCONTROLLED AREA UNC-4
01652> -----
01653>
01654> | DESIGN NASHYD | Area (ha)= 3.65 Curve Number (CN)=76.50
01655> | 07:UNC-4 DT= 1.00 | Ia (mm)= 4.670 # of Linear Res. (N)= 2.00
01656> | U.H. Tp(hrs)= .450
01657>
01658> Unit Hyd Qpeak (cms)= .211
01659>
01660> PEAK FLOW (cms)= .037 (i)
01661> TIME TO PEAK (hrs)= 1.700
01662> RUNOFF VOLUME (mm)= 7.026
01663> TOTAL RAINFALL (mm)= 31.860
01664> RUNOFF COEFFICIENT = .221
01665>
01666> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
01667>
01668> -----
01669> 102:0017-----
01670> -----
01671> | ADD HYD (UNC ) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
01672> |-----|-----|-----|-----|-----|-----|
01673> | ID1 10:UNC-1 | (ha) (cms) (hrs) (mm) (cms)
01674> | +ID2 09:UNC-2 | 1.87 .031 1.28 6.77 .000
01675> | +ID3 08:UNC-3 | .55 .019 1.00 8.40 .000
01676> | +ID4 07:UNC-4 | 3.65 .037 1.70 7.03 .000
01677> |-----|-----|-----|-----|-----|
01678> | SUM 04:UNC | 7.03 .093 1.30 7.14 .000
01679>
01680> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
01681>
01682> -----
01683> 102:0018-----
01684> -----
01685> 102:0002-----
01686> -----
01687> 102:0002-----
01688> -----
01689> 102:0002-----
01690> -----
01691> 102:0002-----
01692> ** END OF RUN : 104
01693> -----
01694> *****
01695> -----
01696> -----
01697> -----
01698> -----
01699> -----
01700> -----
01701> | START | Project dir.: C:\SWMHYM\
01702> |-----| Rainfall dir.: C:\SWMHYM\
01703> |-----| TZERO = 00 hrs on 0
01704> | METOUT= 2 (output = METRIC)
01705> | NRUN = 105
01706> | NSTORM= 1
01707> |-----| # 1=OT3CH5yr.stm
01708> -----
01709> 105:0002-----
01710> *****
01711> # Project Name: [Derry Side Road Subdivision] Project Number: [160401279]
01712> # Date : 09-13-2017
01713> # Modeler : [RMS]
01714> # Company : Stantec Consulting Ltd. 604
01715> # License # : 3824306
01716> *****
01717> -----
01718> 105:0002-----
01719> -----
01720> | DEFAULT VALUES | Filename: C:\SWMHYM\OTTAWA.VAL
01721> |-----| ICASEdsv = 1 (read and print data)
01722> |-----| FileTitle= File comment: [2005 City of Ottawa Sewer Design Guideline]
01723> |-----| PARAMETERS USED IN THE DESIGN STANDHYD COMMAND FOR OTTAWA.
01724> |-----| Horton's infiltration equation parameters:
01725> |-----| [Fo= 76.20 mm/hr] [Fc=13.20 mm/hr] [DCAY= 4.14 /hr] [F= .00 mm]
01726> |-----| Parameters for PERVIOUS surfaces in STANDHYD:
01727> |-----| [IAPER= 4.67 mm] [LGP=40.00 m] [MNP= .250]
01728> |-----| Parameters for IMPERVIOUS surfaces in STANDHYD:
01729> |-----| [IAIMPS= 1.57 mm] [CL1=1.50] [MNI= .013]
01730> |-----| Parameters used in NASHYD:
01731> |-----| [Ia= 4.67 mm] [N= 2.00]
01732> -----
01733> 105:0003-----
01734> -----
01735> | READ STORM | Filename: 5yr CHICAGO STORM, 3hr, DT=10min
01736> | Ptotal= 42.51 mm | Comments: 5yr CHICAGO STORM, 3hr, DT=10min
01737> -----
01738> TIME RAIN | TIME RAIN | TIME RAIN | TIME RAIN
01739> hrs mm/hr | hrs mm/hr | hrs mm/hr | hrs mm/hr
01740> .17 3.682 | 1.00 104.193 | 1.83 6.689 | 2.67 3.510
01741> .33 4.582 | 1.17 32.037 | 2.00 5.628 | 2.83 3.220
01742> .50 6.151 | 1.33 16.337 | 2.17 4.872 | 3.00 2.978
01743> .67 9.614 | 1.50 10.965 | 2.33 4.305 |
01744> .83 24.170 | 1.67 8.287 | 2.50 3.864 |
01745> -----
01746> -----
01747> 105:0004-----
01748> *****
01749> -----
01750> # DERRY SIDE ROAD SUBDIVISION - POST DEVELOPMENT CONDITIONS
01751> *****
01752> # STORM: 12hr SCS Storms, 3hr Chicago Storms
01753> # City of Ottawa 2004 IDF Parameters
01754> -----
01755> # - Average CN values for each catchment were initially calculated on typical

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01756> #* AMC II conditions based on hydrologic soil group and land use. CN values
01757> #* were subsequently modified using the SCS Modified Curve Number Calculations
01758> #* - Soils information for the site area was obtained from exp's
01759> #* Geotechnical Investigation dated July 21, 2017.
01760> #* - CN values calculated based on lawns, woodland and impervious areas
01761> #* - NASHYD command used for catchments with TAMP<20%
01762> #* - Time to peak for each catchment was estimated based on Tp = 0.67*Tc and
01763> #* Tc values were calculated using the Uplands Method
01764> *****
01765> #* AREA A1 TO SWM 1
01766> *****
01767>
01768> | DESIGN NASHYD | Area (ha)= 1.73 Curve Number (CN)=79.20
01769> | 01:A1 DT= 1.00 | Ia (mm)= 4.670 # of Linear Res. (N)= 2.00
01770> |-----| U.H. Tp (hrs)= .230
01771>
01772> Unit Hyd Qpeak (cms)= .195
01773>
01774> PEAK FLOW (cms)= .056 (i)
01775> TIME TO PEAK (hrs)= 1.333
01776> RUNOFF VOLUME (mm)= 13.698
01777> TOTAL RAINFALL (mm)= 42.514
01778> RUNOFF COEFFICIENT = .322
01779>
01780> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
01781>
01782> -----
01783> 105:0005-----
01784> *****
01785> #* AREA A2 TO SWM 1
01786> *****
01787>
01788> | DESIGN NASHYD | Area (ha)= 1.98 Curve Number (CN)=78.30
01789> | 02:A2 DT= 1.00 | Ia (mm)= 4.670 # of Linear Res. (N)= 2.00
01790> |-----| U.H. Tp (hrs)= .280
01791>
01792> Unit Hyd Qpeak (cms)= .174
01793>
01794> PEAK FLOW (cms)= .051 (i)
01795> TIME TO PEAK (hrs)= 1.400
01796> RUNOFF VOLUME (mm)= 13.232
01797> TOTAL RAINFALL (mm)= 42.514
01798> RUNOFF COEFFICIENT = .311
01799>
01800> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
01801>
01802> -----
01803> 105:0006-----
01804> -----
01805> | ADD HYD (TOSWM1 ) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
01806> |-----|-----|-----|-----|-----|-----|
01807> | ID1 01:A1 | (ha) (cms) (hrs) (mm) (cms)
01808> | +ID2 02:A2 | 1.73 .056 1.33 13.70 .000
01809> | +ID3 03:A3 | 1.88 .051 1.40 13.23 .000
01810> |-----|-----|-----|-----|-----|
01811> | SUM 06:TOSWM1 | 3.61 .106 1.35 13.46 .000
01812>
01813> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
01814>
01815> 105:0007-----
01816> -----
01817> | COMPUTE VOLUME |
01818> | ID:06 (TOSWM1) | DISCHARGE TIME
01819> |-----|-----|-----|-----|
01820> |-----| (cms) (hrs)
01821> *** WARNING: No storage required, RelRate > Inflow Qp.
01822> 105:0008-----
01823> *****
01824> #* AREA A3 TO SWM 2
01825> *****
01826>
01827> | DESIGN NASHYD | Area (ha)= 1.33 Curve Number (CN)=78.30
01828> | 01:A3 DT= 1.00 | Ia (mm)= 4.670 # of Linear Res. (N)= 2.00
01829> |-----| U.H. Tp (hrs)= .180
01830>
01831> Unit Hyd Qpeak (cms)= .192
01832>
01833> PEAK FLOW (cms)= .048 (i)
01834> TIME TO PEAK (hrs)= 1.233
01835> RUNOFF VOLUME (mm)= 13.232
01836> TOTAL RAINFALL (mm)= 42.514
01837> RUNOFF COEFFICIENT = .311
01838>
01839> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
01840>
01841> -----
01842> 105:0009-----
01843> *****
01844> #* AREA A4 TO SWM 2
01845> *****
01846>
01847> | DESIGN NASHYD | Area (ha)= 2.71 Curve Number (CN)=78.30
01848> | 02:A4 DT= 1.00 | Ia (mm)= 4.670 # of Linear Res. (N)= 2.00
01849> |-----| U.H. Tp (hrs)= .180
01850>
01851> Unit Hyd Qpeak (cms)= .391
01852>
01853> PEAK FLOW (cms)= .098 (i)
01854> TIME TO PEAK (hrs)= 1.233
01855> RUNOFF VOLUME (mm)= 13.232
01856> TOTAL RAINFALL (mm)= 42.514
01857> RUNOFF COEFFICIENT = .311
01858>
01859> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
01860>
01861> -----
01862> 105:0010-----
01863> *****
01864> #* AREA A5 TO SWM 2
01865> *****
01866>
01867> | DESIGN NASHYD | Area (ha)= 1.43 Curve Number (CN)=78.30
01868> | 03:A5 DT= 1.00 | Ia (mm)= 4.670 # of Linear Res. (N)= 2.00
01869> |-----| U.H. Tp (hrs)= .250
01870>
01871> Unit Hyd Qpeak (cms)= .148
01872>
01873> PEAK FLOW (cms)= .042 (i)
01874> TIME TO PEAK (hrs)= 1.350
01875> RUNOFF VOLUME (mm)= 13.232
01876> TOTAL RAINFALL (mm)= 42.514
01877> RUNOFF COEFFICIENT = .311
01878>
01879> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
01880>
01881> -----
01882> 105:0011-----
01883> *****
01884> | ADD HYD (TOSWM2 ) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
01885> |-----|-----|-----|-----|-----|-----|
01886> | ID1 01:A3 | (ha) (cms) (hrs) (mm) (cms)
01887> | +ID2 02:A4 | 1.33 .048 1.23 13.23 .000
01888> | +ID3 03:A5 | 2.71 .098 1.23 13.23 .000
01889> |-----|-----|-----|-----|-----|
01890> | SUM 05:TOSWM2 | 5.47 .186 1.25 13.23 .000

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01891> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
 01892>
 01893>-----
 01894>-----
 01895> 105:0012-----
 01896>-----
 01897> | COMPUTE VOLUME |
 01898> | ID:05 (TOSW2) | DISCHARGE TIME
 01899> (cms) (hrs)
 01900> START CONTROLLING AT .019 .901
 01901> INFLOW HYD. PEAKS AT .186 1.250
 01902> STOP CONTROLLING AT .185 1.286
 01903>-----
 01904> REQUIRED STORAGE VOLUME (ha.m.)= .0040
 01905> TOTAL HYDROGRAPH VOLUME (ha.m.)= .0724
 01906> % OF HYDROGRAPH TO STORE = 5.4687
 01907>-----
 01908> NOTE: Storage was computed to reduce the inflow
 01909> peak to .185 (cms).
 01910>-----
 01911>-----
 01912> 105:0013-----
 01913> *-----
 01914> *# UNCONTROLLED AREA UNC-1
 01915> *-----
 01916>-----
 01917> | DESIGN NASHYD | Area (ha)= .96 Curve Number (CN)=78.30
 01918> | 10:UNC-1 DT= 1.00 | Ia (mm)= 4.670 # of Linear Res. (N)= 2.00
 01919> | U.H. Tp(hrs)= .160
 01920>-----
 01921> Unit Hyd Qpeak (cms)= .156
 01922>-----
 01923> PEAK FLOW (cms)= .037 (i)
 01924> TIME TO PEAK (hrs)= 1.200
 01925> RUNOFF VOLUME (mm)= 13.231
 01926> TOTAL RAINFALL (mm)= 42.514
 01927> RUNOFF COEFFICIENT = .311
 01928>-----
 01929> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
 01930>-----
 01931>-----
 01932> 105:0014-----
 01933> *-----
 01934> *# UNCONTROLLED AREA UNC-2
 01935> *-----
 01936>-----
 01937> | DESIGN NASHYD | Area (ha)= 1.87 Curve Number (CN)=75.60
 01938> | 09:UNC-2 DT= 1.00 | Ia (mm)= 4.670 # of Linear Res. (N)= 2.00
 01939> | U.H. Tp(hrs)= .190
 01940>-----
 01941> Unit Hyd Qpeak (cms)= .255
 01942>-----
 01943> PEAK FLOW (cms)= .058 (i)
 01944> TIME TO PEAK (hrs)= 1.250
 01945> RUNOFF VOLUME (mm)= 11.952
 01946> TOTAL RAINFALL (mm)= 42.514
 01947> RUNOFF COEFFICIENT = .281
 01948>-----
 01949> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
 01950>-----
 01951>-----
 01952> 105:0015-----
 01953> *-----
 01954> *# UNCONTROLLED AREA UNC-3
 01955> *-----
 01956>-----
 01957> | DESIGN STANDHYD | Area (ha)= .55 Curve Number (CN)=79.20
 01958> | 08:UNC-3 DT= 1.00 | Total Imp(%)= 24.20 Dir. Conn.(%)= 13.30
 01959>-----
 01960>-----
 01961> Surface Area (ha)= .13 IMPERVIOUS .42 PERVIOUS (i)
 01962> Dep. Storage (mm)= 1.57 4.67
 01963> Average Slope (%)= 1.00 1.00
 01964> Length (m)= 60.55 40.00
 01965> Mannings n = .013 .250
 01966>-----
 01967> Max. eff. Inten. (mm/hr)= 104.19 55.23
 01968> over (min) 2.00 13.00
 01969> Storage Coeff. (min)= 1.86 (ii) 12.88 (ii)
 01970> Unit Hyd. Tpeak (min)= 2.00 13.00
 01971> Unit Hyd. peak (cms)= .58 .09
 01972>-----
 01973> PEAK FLOW (cms)= .02 .04 *TOTALS*
 01974> TIME TO PEAK (hrs)= 1.00 1.15 1.150 (iii)
 01975> RUNOFF VOLUME (mm)= 40.94 11.27 15.217
 01976> TOTAL RAINFALL (mm)= 42.51 42.51 42.514
 01977> RUNOFF COEFFICIENT = .96 .27 .358
 01978>-----
 01979> (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 01980> Fo (mm/hr)= 76.20 Cum. Inf. (mm)= 4.14
 01981> Fc (mm/hr)= 13.20
 01982> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 01983> THAN THE STORAGE COEFFICIENT.
 01984> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
 01985>-----
 01986>-----
 01987> 105:0016-----
 01988> *-----
 01989> *# UNCONTROLLED AREA UNC-4
 01990> *-----
 01991>-----
 01992> | DESIGN NASHYD | Area (ha)= 3.65 Curve Number (CN)=76.50
 01993> | 07:UNC-4 DT= 1.00 | Ia (mm)= 4.670 # of Linear Res. (N)= 2.00
 01994> | U.H. Tp(hrs)= .450
 01995>-----
 01996> Unit Hyd Qpeak (cms)= .211
 01997>-----
 01998> PEAK FLOW (cms)= .067 (i)
 01999> TIME TO PEAK (hrs)= 1.667
 02000> RUNOFF VOLUME (mm)= 12.360
 02001> TOTAL RAINFALL (mm)= 42.514
 02002> RUNOFF COEFFICIENT = .291
 02003>-----
 02004> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
 02005>-----
 02006>-----
 02007> 105:0017-----
 02008> *-----
 02009> | ADD HYD (UNC) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
 02010> (ha) (cms) (hrs) (mm) (cms)
 02011> ID1 10:UNC-1 .96 .037 1.20 13.23 .000
 02012> +ID2 09:UNC-2 1.87 .058 1.25 11.95 .000
 02013> +ID3 08:UNC-3 .55 .043 1.15 15.22 .000
 02014> +ID4 07:UNC-4 3.65 .067 1.67 12.36 .000
 02015>-----
 02016> SUM 04:UNC 7.03 .175 1.20 12.59 .000
 02017>-----
 02018> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
 02019>-----
 02020>-----
 02021> 105:0018-----
 02022>-----
 02023> 105:0002-----
 02024>-----
 02025> 105:0002-----

02026>-----
 02027> 105:0002-----
 02028>-----
 02029> 105:0002-----
 02030>-----
 02031> 105:0002-----
 02032> ** END OF RUN : 199
 02033>-----
 02034>-----
 02035>-----
 02036>-----
 02037>-----
 02038>-----
 02039>-----
 02040>-----
 02041> | START | Project dir.: C:\SWMHYM\ |
 02042> | TZERO = .00 hrs on | Rainfall dir.: C:\SWMHYM\ |
 02043>-----
 02044> METOUT= 2 (output = METRIC)
 02045> NRUN = 200
 02046> NSTORM= 1
 02047> # I=OT3CHydr.stm
 02048>-----
 02049> 200:0002-----
 02050> *-----
 02051> *# Project Name: [Derry Side Road Subdivision] Project Number: [160401279]
 02052> *# Date : 09-13-2017
 02053> *# Modeller : [AMP]
 02054> *# Company : Stantec Consulting Ltd. 604
 02055> *# License # : 3824306
 02056> *-----
 02057>-----
 02058>-----
 02059>-----
 02060> | DEFAULT VALUES | Filename: C:\SWMHYM\OTTAWA.VAL
 02061>-----
 02062> ICASEdv = 1 (read and print data)
 02063> FileTitle= File comment: [2005 City of Ottawa Sewer Design Guideline]
 02064> PARAMETERS USED IN THE DESIGN STANDHYD COMMAND FOR OTTAWA.
 02065> Horton's infiltration equation parameters:
 02066> [Fo= 76.20 mm/hr] [Fc=13.20 mm/hr] [DCAY= 4.14 /hr] [F= .00 mm]
 02067> Parameters for PERVIOUS surfaces in STANDHYD:
 02068> [IApe= 4.67 mm] [LGP=40.00 m] [MNP=.250]
 02069> Parameters for IMPERVIOUS surfaces in STANDHYD:
 02070> [IAimp= 1.57 mm] [CLL= 1.50] [MNI=.013]
 02071> Parameters used in NASHYD:
 02072> [Ia= 4.67 mm] [N= 2.00]
 02073>-----
 02074> 200:0003-----
 02075> | READ STORM | Filename: 100yr CHICAGO STORM, 3hr, DT=10min
 02076> | Ptotal= 71.66 mm | Comments: 100yr CHICAGO STORM, 3hr, DT=10min
 02077>-----
 02078>-----
 02079> TIME RAIN | TIME RAIN | TIME RAIN | TIME RAIN
 02080> hrs mm/hr | hrs mm/hr | hrs mm/hr | hrs mm/hr
 02081> .17 6.046 | 1.00 178.559 | 1.83 11.059 | 2.67 5.760
 02082> .33 7.542 | 1.17 54.049 | 2.00 9.285 | 2.83 5.280
 02083> .50 10.159 | 1.33 27.319 | 2.17 8.024 | 3.00 4.879
 02084> .67 15.969 | 1.50 18.240 | 2.33 7.060 |
 02085> .83 40.655 | 1.67 13.737 | 2.50 6.347 |
 02086>-----
 02087> 200:0004-----
 02088> *-----
 02089> *#-----
 02090> *# DERRY SIDE ROAD SUBDIVISION - POST DEVELOPMENT CONDITIONS
 02091> *#-----
 02092> *# STORM: 12hr SCS Storms, 3hr Chicago Storms
 02093> *# City of Ottawa 2004 IDF Parameters
 02094> *#-----
 02095> *# - Average CN values for each catchment were initially calculated on typical
 02096> *# AMC II conditions based on hydrologic soil group and land use. CN values
 02097> *# were subsequently modified using the SCS Modified Curve Number Calculations
 02098> *# - Soils information for the site area was obtained from exp's
 02099> *# Geotechnical Investigation dated July 21, 2017.
 02100> *# - CN values calculated based on lawns, woodland and impervious areas
 02101> *# - NASHYD command used for catchments with TIMP<20%
 02102> *# - Time to peak for each catchment was estimated based on Tp = 0.67*Tc and
 02103> *# Tc values were calculated using the Uplands Method
 02104> *#-----
 02105> *# AREA A1 TO SWM 1
 02106> *#-----
 02107>-----
 02108> | DESIGN NASHYD | Area (ha)= 1.73 Curve Number (CN)=79.20
 02109> | 01:A1 DT= 1.00 | Ia (mm)= 4.670 # of Linear Res. (N)= 2.00
 02110> | U.H. Tp(hrs)= .230
 02111>-----
 02112> Unit Hyd Qpeak (cms)= .195
 02113>-----
 02114> PEAK FLOW (cms)= .145 (i)
 02115> TIME TO PEAK (hrs)= 1.283
 02116> RUNOFF VOLUME (mm)= 33.569
 02117> TOTAL RAINFALL (mm)= 71.665
 02118> RUNOFF COEFFICIENT = .468
 02119>-----
 02120> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
 02121>-----
 02122>-----
 02123> 200:0005-----
 02124> *-----
 02125> *# AREA A2 TO SWM 1
 02126> *#-----
 02127>-----
 02128> | DESIGN NASHYD | Area (ha)= 1.88 Curve Number (CN)=78.30
 02129> | 02:A2 DT= 1.00 | Ia (mm)= 4.670 # of Linear Res. (N)= 2.00
 02130> | U.H. Tp(hrs)= .280
 02131>-----
 02132> Unit Hyd Qpeak (cms)= .174
 02133>-----
 02134> PEAK FLOW (cms)= .134 (i)
 02135> TIME TO PEAK (hrs)= 1.367
 02136> RUNOFF VOLUME (mm)= 32.669
 02137> TOTAL RAINFALL (mm)= 71.665
 02138> RUNOFF COEFFICIENT = .456
 02139>-----
 02140> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
 02141>-----
 02142>-----
 02143> 200:0006-----
 02144> *-----
 02145> | ADD HYD (TOSW1) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
 02146> (ha) (cms) (hrs) (mm) (cms)
 02147> ID1 01:A1 1.73 .145 1.28 33.57 .000
 02148> +ID2 02:A2 1.88 .134 1.37 32.67 .000
 02149>-----
 02150> SUM 06:TOSW1 3.61 .277 1.33 33.10 .000
 02151>-----
 02152> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
 02153>-----
 02154>-----
 02155> 200:0007-----
 02156>-----
 02157> | COMPUTE VOLUME |
 02158> | ID:06 (TOSW1) | DISCHARGE TIME
 02159> (cms) (hrs)
 02160> START CONTROLLING AT .011 .849

```

02161> INFLOW HYD. PEAKS AT .277 1.333
02162> STOP CONTROLLING AT .185 1.784
02163>
02164> REQUIRED STORAGE VOLUME (ha.m.)= .0362
02165> TOTAL HYDROGRAPH VOLUME (ha.m.)= .1195
02166> % OF HYDROGRAPH TO STORE = 30.2814
02167>
02168> NOTE: Storage was computed to reduce the Inflow
02169> peak to .185 (cms).
02170>
-----
02172> 200:0008-----
02173> *#-----
02174> *# AREA A3 TO SWM 2
02175> *#-----
02176>
02177> | DESIGN NASHYD | Area (ha)= 1.33 Curve Number (CN)=78.30
02178> | 01:A3 DT= 1.00 | Ia (mm)= 4.670 # of Linear Res. (N)= 2.00
02179> | U.H. Tp(hrs)= .180
02180>
02181> Unit Hyd Qpeak (cms)= .192
02182>
02183> PEAK FLOW (cms)= .127 (i)
02184> TIME TO PEAK (hrs)= 1.217
02185> RUNOFF VOLUME (mm)= 32.669
02186> TOTAL RAINFALL (mm)= 71.665
02187> RUNOFF COEFFICIENT = .456
02188>
02189> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
02190>
-----
02192> 200:0009-----
02193> *#-----
02194> *# AREA A4 TO SWM 2
02195> *#-----
02196>
02197> | DESIGN NASHYD | Area (ha)= 2.71 Curve Number (CN)=78.30
02198> | 02:A4 DT= 1.00 | Ia (mm)= 4.670 # of Linear Res. (N)= 2.00
02199> | U.H. Tp(hrs)= .180
02200>
02201> Unit Hyd Qpeak (cms)= .391
02202>
02203> PEAK FLOW (cms)= .258 (i)
02204> TIME TO PEAK (hrs)= 1.217
02205> RUNOFF VOLUME (mm)= 32.669
02206> TOTAL RAINFALL (mm)= 71.665
02207> RUNOFF COEFFICIENT = .456
02208>
02209> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
02210>
-----
02212> 200:0010-----
02213> *#-----
02214> *# AREA A5 TO SWM 2
02215> *#-----
02216>
02217> | DESIGN NASHYD | Area (ha)= 1.43 Curve Number (CN)=78.30
02218> | 03:A5 DT= 1.00 | Ia (mm)= 4.670 # of Linear Res. (N)= 2.00
02219> | U.H. Tp(hrs)= .250
02220>
02221> Unit Hyd Qpeak (cms)= .148
02222>
02223> PEAK FLOW (cms)= .110 (i)
02224> TIME TO PEAK (hrs)= 1.333
02225> RUNOFF VOLUME (mm)= 32.669
02226> TOTAL RAINFALL (mm)= 71.665
02227> RUNOFF COEFFICIENT = .456
02228>
02229> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
02230>
-----
02232> 200:0011-----
02233> | ADD HYD (TOSW2 ) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
02235> | (ha) (cms) (hrs) (mm) (cms)
02236> | ID1 01:A3 1.33 .127 1.22 32.67 .000
02237> | +ID2 02:A4 2.71 .258 1.22 32.67 .000
02238> | +ID3 03:A5 1.43 .110 1.33 32.67 .000
02239> |
02240> | SUM 05:TOSW2 5.47 .491 1.23 32.67 .000
02241>
02242> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
02243>
-----
02245> 200:0012-----
02246>
02247> | COMPUTE VOLUME |
02248> | ID:05 (TOSW2) | DISCHARGE TIME
02249> | (cms) (hrs)
02250> | START CONTROLLING AT .011 .791
02251> | INFLOW HYD. PEAKS AT .491 1.233
02252> | STOP CONTROLLING AT .185 1.955
02253>
02254> REQUIRED STORAGE VOLUME (ha.m.)= .0888
02255> TOTAL HYDROGRAPH VOLUME (ha.m.)= .1787
02256> % OF HYDROGRAPH TO STORE = 49.6948
02257>
02258> NOTE: Storage was computed to reduce the Inflow
02259> peak to .185 (cms).
02260>
-----
02262> 200:0013-----
02263> *#-----
02264> *# UNCONTROLLED AREA UNC-1
02265> *#-----
02266>
02267> | DESIGN NASHYD | Area (ha)= .96 Curve Number (CN)=78.30
02268> | 10:UNC-1 DT= 1.00 | Ia (mm)= 4.670 # of Linear Res. (N)= 2.00
02269> | U.H. Tp(hrs)= .160
02270>
02271> Unit Hyd Qpeak (cms)= .156
02272>
02273> PEAK FLOW (cms)= .099 (i)
02274> TIME TO PEAK (hrs)= 1.183
02275> RUNOFF VOLUME (mm)= 32.668
02276> TOTAL RAINFALL (mm)= 71.665
02277> RUNOFF COEFFICIENT = .456
02278>
02279> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
02280>
-----
02282> 200:0014-----
02283> *#-----
02284> *# UNCONTROLLED AREA UNC-2
02285> *#-----
02286>
02287> | DESIGN NASHYD | Area (ha)= 1.87 Curve Number (CN)=75.60
02288> | 09:UNC-2 DT= 1.00 | Ia (mm)= 4.670 # of Linear Res. (N)= 2.00
02289> | U.H. Tp(hrs)= .190
02290>
02291> Unit Hyd Qpeak (cms)= .255
02292>
02293> PEAK FLOW (cms)= .157 (i)
02294> TIME TO PEAK (hrs)= 1.233
02295> RUNOFF VOLUME (mm)= 30.128

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```

02296> TOTAL RAINFALL (mm)= 71.665
02297> RUNOFF COEFFICIENT = .420
02298>
02299> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
02300>
-----
02302> 200:0015-----
02303> *#-----
02304> *# UNCONTROLLED AREA UNC-3
02305> *#-----
02306>
02307> | DESIGN STANDHYD | Area (ha)= .55
02308> | 08:UNC-3 DT= 1.00 | Total Imp(%)= 24.20 Dir. Conn.(%)= 13.30
02309>
02310>
02311> IMPERVIOUS PERVIOUS (i)
02312> Surface Area (ha)= .13 .42
02313> Dep. Storage (mm)= 1.57 4.67
02314> Average Slope (%)= 1.00 1.00
02315> Length (m)= 60.55 40.00
02316> Mannings n = .013 .250
02317>
02318> Max.eff.Inten.(mm/hr)= 178.56 170.71
02319> Storage Coeff. (min)= 1.00 9.00
02320> Unit Hyd. Tpeak (min)= 1.00 9.00
02321> Unit Hyd. peak (cms)= .83 .13
02322>
02323> PEAK FLOW (cms)= .04 .12 *TOTALS*
02324> TIME TO PEAK (hrs)= 1.00 1.08 1.083
02325> RUNOFF VOLUME (mm)= 70.09 33.11 38.030
02326> TOTAL RAINFALL (mm)= 71.66 71.66 71.665
02327> RUNOFF COEFFICIENT = .98 .46 .531
02328>
02329> (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
02330> Fo (mm/hr)= 76.20 K (1/hr)= 4.14
02331> Fc (mm/hr)= 13.20 Cum.Inf. (mm)= .700
02332> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
02333> THAN THE STORAGE COEFFICIENT.
02334> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
02335>
-----
02337> 200:0016-----
02338> *#-----
02339> *# UNCONTROLLED AREA UNC-4
02340> *#-----
02341>
02342> | DESIGN NASHYD | Area (ha)= 3.65 Curve Number (CN)=76.50
02343> | 07:UNC-4 DT= 1.00 | Ia (mm)= 4.670 # of Linear Res. (N)= 2.00
02344> | U.H. Tp(hrs)= .450
02345>
02346> Unit Hyd Qpeak (cms)= .211
02347>
02348> PEAK FLOW (cms)= .175 (i)
02349> TIME TO PEAK (hrs)= 1.617
02350> RUNOFF VOLUME (mm)= 30.949
02351> TOTAL RAINFALL (mm)= 71.665
02352> RUNOFF COEFFICIENT = .432
02353>
02354> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
02355>
-----
02357> 200:0017-----
02358>
02359> | ADD HYD (UNC ) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
02360> | (ha) (cms) (hrs) (mm) (cms)
02361> | ID1 10:UNC-1 .96 .099 1.18 32.67 .000
02362> | +ID2 09:UNC-2 1.87 .157 1.23 30.13 .000
02363> | +ID3 08:UNC-3 .55 .129 1.08 38.03 .000
02364> | +ID4 07:UNC-4 3.65 .175 1.62 30.95 .000
02365> |
02366> | SUM 04:UNC 7.03 .465 1.17 31.52 .000
02367>
02368> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
02369>
-----
02371> 200:0018-----
02372>
02373> 200:0002-----
02374>
02375> 200:0002-----
02376>
02377> 200:0002-----
02378>
02379> 200:0002-----
02380>
02381> 200:0002-----
02382>
02383> 200:0002-----
02384> FINISH
02385>
02386>
02387> WARNINGS / ERRORS / NOTES
02388>
02389> 001:0007 COMPUTE VOLUME
02390> *** WARNING: No storage required, RelRate > Inflow Qp.
02391> 001:0012 COMPUTE VOLUME
02392> *** WARNING: No storage required, RelRate > Inflow Qp.
02393> 002:0007 COMPUTE VOLUME
02394> *** WARNING: No storage required, RelRate > Inflow Qp.
02395> 002:0012 COMPUTE VOLUME
02396> *** WARNING: No storage required, RelRate > Inflow Qp.
02397> 005:0007 COMPUTE VOLUME
02398> *** WARNING: No storage required, RelRate > Inflow Qp.
02399> *** WARNING: No storage required, RelRate > Inflow Qp.
02400> 102:0012 COMPUTE VOLUME
02401> *** WARNING: No storage required, RelRate > Inflow Qp.
02402> 105:0007 COMPUTE VOLUME
02403> *** WARNING: No storage required, RelRate > Inflow Qp.
02404> Simulation ended on 2017-09-15 at 09:45:32
02405>
02406>

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DERRY SIDE ROAD SUBDIVISION – BECKWITH, ON CONCEPTUAL STORMWATER MANAGEMENT REPORT

Appendix C Preliminary CDS Sizing
September 25, 2017

Appendix C PRELIMINARY CDS SIZING

DESIGN PARAMETERS

CDS Model No. =	CDS3020	
Design Treatment Flow =	2.0	cfs
Peak Design Flow =	3.18	cfs
Peak Design Return Interval =	2	year
Rim Elevation @ US Structure	432.41	ft

DETAILED CALCULATIONS

TREATMENT FLOW

Tailwater Condition at Outfall, EL₀

$$EL_0 = 431.29 \text{ ft (invert plus depth of flow at D/S outlet)}$$

Exit Loss from DownStream Pipe, h₁

$$h_1 = k * [V^2 / (2*g)]$$

where,

$$k = 1.00$$

$$V = Q / A_F$$

$$= 3.82 \text{ fps}$$

$$h_1 = 0.23 \text{ ft}$$

$$EGL_1 = EL_0 + h_1$$

$$= 431.51 \text{ ft}$$

Head Loss Through Downstream Pipe, h₂

Friction Losses, h₂

$$h_2 = S_{EGL} * L$$

where,

$$L = 52.4934 \text{ ft}$$

$$S_{EGL} = [(Q * n) / (1.49 * A_F * R^{2/3})]^2$$

where,

Pipe Characteristics

$$\text{Dia.} = 12 \text{ in}$$

$$S_{PIPE} = 0.0035 \text{ ft/ft}$$

$$n = 0.01$$

Flow Characteristics

$$d_F = 0.63 \text{ ft}$$

$$A_F = 0.52 \text{ sf}$$

$$P_W = 1.84 \text{ ft}$$

$$R = 0.28 \text{ ft}$$

Head Loss Through Downstream Pipe, h_2 (cont.'d)

9/14/2017

$$S_{EGL} = \underline{0.00351} \text{ ft / ft}$$

$$h_2 = \underline{0.1840} \text{ ft}$$

$$\begin{aligned} EGL_2' &= EGL_1 + h_2 \\ &= \underline{431.70} \text{ ft} \end{aligned}$$

Check Entrance Condition for Critical Depth Control

$$EL_{CDS \text{ Inv.}} = \underline{430.84} \text{ ft}$$

$$d_c = \underline{0.59} \text{ ft}$$

$$\begin{aligned} EGL_C &= EL_{CDS \text{ Inv.}} + d_c + V_{dc}^2 / (2 * g) \\ &= \underline{431.70} \text{ ft} \end{aligned}$$

Identify Controlling EGL

Friction based EGL controls.

$$EGL_2 = \underline{431.70} \text{ ft}$$

Re-entry Loss into DownStream Pipe, h_3

$$h_3 = k * [V^2 / (2 * g)]$$

where,

$$k = \underline{0.20}$$

$$V = Q / A$$

$$= \underline{3.82} \text{ fps (area based on flow depth)}$$

$$h_3 = \underline{0.05} \text{ ft}$$

$$\begin{aligned} EGL_3' &= EGL_2 + h_3 \\ &= \underline{431.74} \text{ ft} \end{aligned}$$

Oil Baffle Loss, h_4

$$h_4 = k * [V^2 / (2 * g)]$$

where,

$$k = \underline{1.00}$$

$$A_{\text{Baffle}} = \underline{6.49} \text{ sf}$$

$$V = Q / A_{\text{baffle}}$$

$$= \underline{0.31} \text{ fps}$$

$$h_4 = \underline{0.0015} \text{ ft}$$

$$\begin{aligned} EGL_4 &= EGL_3 + h_4 \\ &= \underline{431.74} \text{ ft} \end{aligned}$$

Check Standard Weir Elevation

$$HL_{CDS} = \underline{0.50} \text{ ft}$$

$$\begin{aligned} EL_W' &= EGL_4 + HL_{CDS} \\ &= \underline{432.24} \text{ ft} \end{aligned}$$

$$H_W' = EL_W' - EL_{CDS \text{ INV.}}$$

$$= \underline{1.41} \text{ ft, or } \underline{16.88} \text{ in}$$

$$\text{Std. Weir Height} = \underline{17.0} \text{ in}$$

Status **OK**

$$\text{Use } H_W = \underline{17} \text{ in, or } \underline{1.42} \text{ ft}$$

$$\begin{aligned} EL_W &= EL_{CDS \text{ INV.}} + H_W \\ &= \underline{432.26} \text{ ft} \end{aligned}$$

PEAK CONVEYANCE FLOW

9/14/2017

Tailwater Condition at Outfall, EL_0

$$EL_0 = \underline{431.65} \text{ ft (invert plus depth of flow at D/S outlet)}$$

Exit Loss from DownStream Pipe, h_1

$$h_1 = k * [V^2 / (2*g)]$$

where,

$$k = \underline{1.00}$$

$$V = Q / A_F$$

$$= \underline{4.05} \text{ fps}$$

$$h_1 = \underline{0.25} \text{ ft}$$

$$EGL_1 = EL_0 + h_1$$

$$= \underline{431.91} \text{ ft}$$

Head Loss Through Downstream Pipe, h_2

Friction Losses, h_2

$$h_2 = S_{EGL} * L$$

where,

$$L = \underline{52.4934} \text{ ft}$$

$$S_{EGL} = [(Q * n) / (1.49 * A_F * R^{2/3})]^2$$

where,

Pipe Characteristics

$$\text{Dia.} = \underline{12} \text{ in}$$

$$S_{PIPE} = \underline{0.0035} \text{ ft/ft}$$

$$n = \underline{0.01}$$

Flow Characteristics

$$d_n = \underline{1.00} \text{ ft}$$

$$A_F = \underline{0.79} \text{ sf}$$

$$P_W = \underline{3.14} \text{ ft}$$

$$R = \underline{0.25} \text{ ft}$$

$$S_{EGL} = \underline{0.0047} \text{ ft / ft}$$

$$h_2 = \underline{0.25} \text{ ft}$$

$$EGL_2' = EGL_1 + h_2$$

$$= \underline{432.16} \text{ ft}$$

Check Entrance Condition for Critical Depth Control

$$EL_{CDS \text{ Inv.}} = \underline{430.84} \text{ ft}$$

$$d_c = \underline{0.75} \text{ ft}$$

$$EGL_C = EL_{CDS \text{ Inv.}} + d_c + V_{dc}^2 / (2*g)$$

$$= \underline{431.98} \text{ ft}$$

Identify Controlling EGL

Friction based EGL controls.

$$EGL_2 = \underline{432.16} \text{ ft}$$

Re-entry Loss into DownStream Pipe, h_3

9/14/2017

$$h_3 = k * [V^2 / (2*g)]$$

where,

$$k = \frac{0.20}{}$$

$$V = Q / A_F$$

$$= \frac{4.05}{} \text{ fps (area based on flow depth)}$$

$$h_3 = \frac{0.05}{} \text{ ft}$$

$$\text{EGL}_3 = \text{EGL}_2 + h_3$$

$$= \frac{432.21}{} \text{ ft}$$

Oil Baffle Loss, h_4

$$h_4 = k * [V^2 / (2*g)]$$

where,

$$k = \frac{0.00}{} \text{ (Skirted-baffle model)}$$

$$A_{\text{Baffle}} = \frac{6.49}{} \text{ sf}$$

$$V = Q / A_{\text{Baffle}}$$

$$= \frac{0.49}{} \text{ fps}$$

$$h_4 = \frac{0.00}{} \text{ ft}$$

$$\text{EGL}_4 = \text{EGL}_3 + h_4$$

$$= \frac{432.21}{} \text{ ft}$$

$$\text{HGL}_4 = \text{EGL}_4 - [V_P^2 / (2*g)]$$

$$= \frac{431.95}{} \text{ ft}$$

Head over Diversion Weir, h_5

Elevation of Weir

$$\text{EL}_{\text{Weir}} = \frac{432.26}{} \text{ ft (established above)}$$

Headloss for Free Discharge Condition

$$h_{5a} = [Q / (C * L)]^{2/3}$$

where,

$$C = \frac{3.1}{}$$

$$L = \frac{3.00}{} \text{ ft}$$

$$h_{5a} = \frac{0.49}{} \text{ ft}$$

$$\text{EGL}_{5a} = \text{EL}_{\text{Weir}} + h_{5a}$$

$$= \frac{432.75}{} \text{ ft}$$

Headloss for Submerged Condition

$$d_{\text{Sub}} = \frac{0.00}{} \text{ ft (depth of submergence)}$$

$$h_{5b} = \frac{2.49}{} \text{ ft (separate submerged weir calc.)}$$

$$\text{EGL}_{5b} = \text{EGL}_4 + h_{5b}$$

$$= \frac{434.69}{} \text{ ft}$$

Identify EGL U/S of Weir

The discharge condition is Free, therefore

$$\text{EGL}_5 = \frac{432.75}{} \text{ ft}$$

Expansion Loss from U/S Pipe, h_6

9/14/2017

$$h_6 = k * [V^2 / (2 * g)]$$

where,

$$k = \underline{0.30}$$

$$V = Q / A_F$$

$$= \underline{4.05} \text{ fps}$$

$$h_6 = \underline{0.08} \text{ ft}$$

$$EGL_6 = EGL_5 + h_6$$

$$= \underline{432.82} \text{ ft}$$

Head Loss Through Upstream Pipe, h_7 Friction Losses, h_7

$$h_7 = S_{EGL} * L$$

where,

$$L = \underline{30.8399} \text{ ft}$$

$$S_{EGL} = [(Q * n) / (1.49 * A_F * R^{2/3})]^2$$

where,

Pipe Characteristics

$$\text{Dia.} = \underline{12} \text{ in}$$

$$S_{PIPE} = \underline{0.0035} \text{ ft/ft}$$

$$n = \underline{0.01}$$

Flow Characteristics

$$d_n = \underline{1.00} \text{ ft}$$

$$A_F = \underline{0.79} \text{ sf}$$

$$P_W = \underline{3.14} \text{ ft}$$

$$R = \underline{0.25} \text{ ft}$$

$$S_{EGL} = \underline{0.0047} \text{ ft / ft}$$

$$h_7 = \underline{0.14} \text{ ft}$$

$$EGL_7' = EGL_6 + h_7$$

$$= \underline{432.97} \text{ ft}$$

Check Entrance Condition for Critical Depth Control

$$EL_{U/S \text{ Inv.}} = \underline{430.95} \text{ ft}$$

$$d_c = \underline{0.75} \text{ ft}$$

$$EGL_C = EL_{CDS \text{ Inv.}} + d_c + V_{dc}^2 / (2 * g)$$

$$= \underline{432.09} \text{ ft}$$

Identify Controlling EGL

Friction based EGL controls.

$$EGL_7 = \underline{432.97} \text{ ft}$$

$$HGL_7 = EGL_7 - [V^2 / (2 * g)]$$

$$= \underline{432.71} \text{ ft}$$

$$\text{Freeboard} = \underline{-0.30} \text{ ft (at first upstream structure)}$$



**CDS ESTIMATED NET ANNUAL SOLIDS LOAD REDUCTION
BASED ON THE RATIONAL RAINFALL METHOD
BASED ON A FINE PARTICLE SIZE DISTRIBUTION**



Project Name: Derry Side Road Subdivision	Engineer: Stantec
Location: Beckwith, ON	Contact: Ana Paerez, P. Eng.
OGS #: 1	Report Date: 14-Sep-17

Area 3.61 ha	Rainfall Station # 215	
Weighted C 0.35	Particle Size Distribution FINE	
CDS Model 3020	CDS Treatment Capacity 57 l/s	

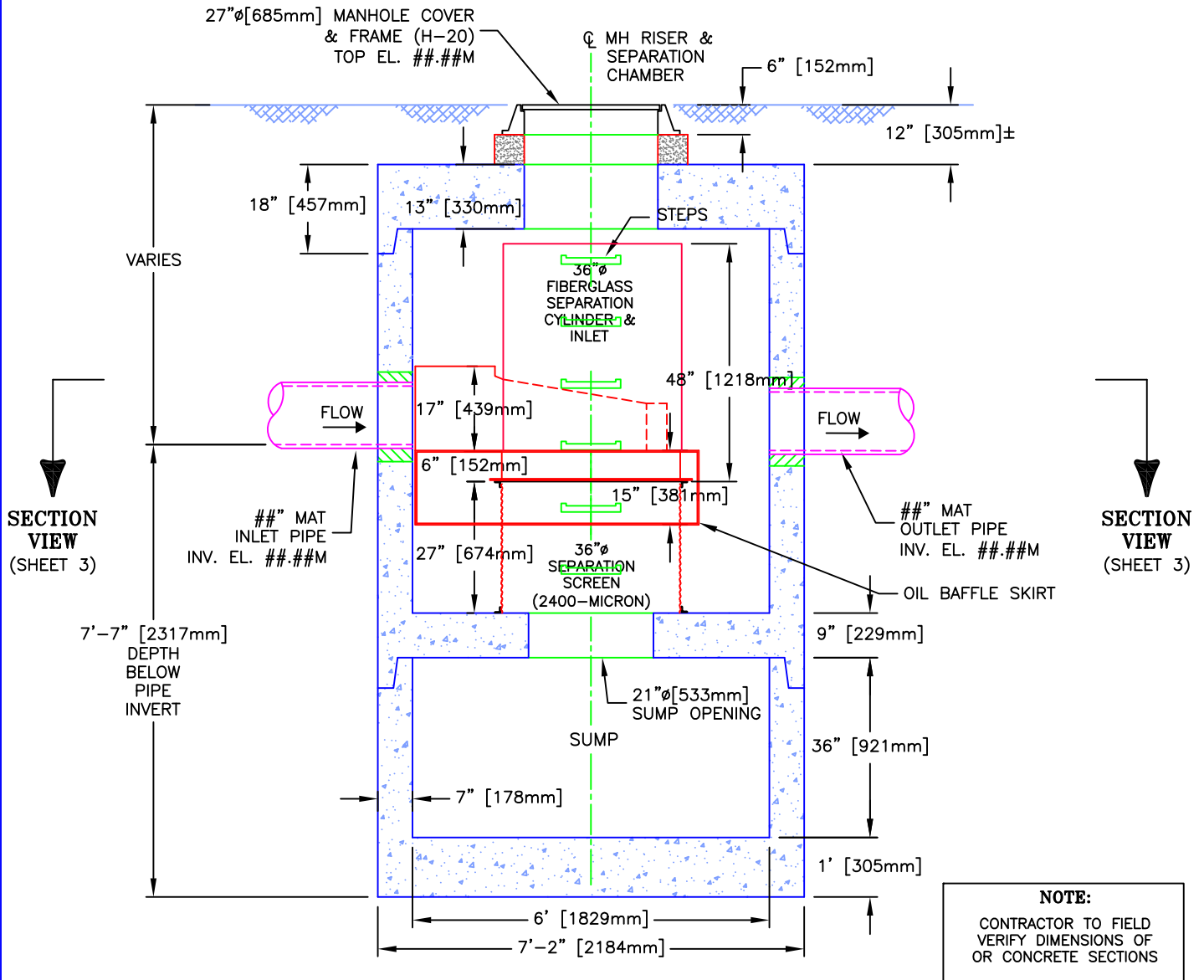
<u>Rainfall Intensity¹</u> (mm/hr)	<u>Percent Rainfall Volume¹</u>	<u>Cumulative Rainfall Volume</u>	<u>Total Flowrate (l/s)</u>	<u>Treated Flowrate (l/s)</u>	<u>Operating Rate (%)</u>	<u>Removal Efficiency (%)</u>	<u>Incremental Removal (%)</u>
0.5	9.2%	9.2%	1.8	1.8	3.1	98.0	9.0
1.0	10.6%	19.8%	3.5	3.5	6.2	97.1	10.3
1.5	9.9%	29.7%	5.3	5.3	9.3	96.2	9.5
2.0	8.4%	38.1%	7.0	7.0	12.4	95.3	8.0
2.5	7.7%	45.8%	8.8	8.8	15.5	94.4	7.3
3.0	5.9%	51.7%	10.5	10.5	18.6	93.5	5.6
3.5	4.4%	56.1%	12.3	12.3	21.7	92.6	4.0
4.0	4.7%	60.7%	14.1	14.1	24.8	91.7	4.3
4.5	3.3%	64.0%	15.8	15.8	27.9	90.9	3.0
5.0	3.0%	67.1%	17.6	17.6	31.0	90.0	2.7
6.0	5.4%	72.4%	21.1	21.1	37.2	88.2	4.8
7.0	4.4%	76.8%	24.6	24.6	43.4	86.4	3.8
8.0	3.5%	80.3%	28.1	28.1	49.6	84.6	3.0
9.0	2.8%	83.2%	31.6	31.6	55.8	82.9	2.3
10.0	2.2%	85.3%	35.1	35.1	62.0	81.1	1.8
15.0	7.0%	92.3%	52.7	52.7	93.0	72.2	5.0
20.0	4.5%	96.9%	70.3	56.6	100.0	56.6	2.6
25.0	1.4%	98.3%	87.8	56.6	100.0	45.3	0.7
30.0	0.7%	99.0%	105.4	56.6	100.0	37.7	0.3
35.0	0.5%	99.5%	122.9	56.6	100.0	32.3	0.2
40.0	0.5%	100.0%	140.5	56.6	100.0	28.3	0.2

	Removal Efficiency Adjustment ² = 6.5%
	Predicted Net Annual Load Removal Efficiency = 81.6%
	Predicted % Annual Rainfall Treated = 97.7%

1 - Based on 42 years of hourly rainfall data from Canadian Station 6105976, Ottawa ON
 2 - Reduction due to use of 60-minute data for a site that has a time of concentration less than 30-minutes.
 3 - CDS Efficiency based on testing conducted at the University of Central Florida
 4 - CDS design flowrate and scaling based on standard manufacturer model & product specifications



ELEVATION VIEW



CDS MODEL PMSU30_20m, 2 CFS TREATMENT CAPACITY STORM WATER TREATMENT UNIT

	PROJECT NAME CITY, STATE	JOB#	CAN-##-###	SCALE 1" = 3'
		DATE	##/##/##	SHEET
		DRAWN	INITIALS	2
		APPROV.		

DESIGN PARAMETERS

CDS Model No. =	CDS3030	
Design Treatment Flow =	3.0	cfs
Peak Design Flow =	4.45	cfs
Peak Design Return Interval =	2	year
Rim Elevation @ US Structure	432.09	ft

DETAILED CALCULATIONS

TREATMENT FLOW

Tailwater Condition at Outfall, EL₀

$$EL_0 = 431.29 \text{ ft (invert plus depth of flow at D/S outlet)}$$

Exit Loss from DownStream Pipe, h₁

$$h_1 = k * [V^2 / (2*g)]$$

where,

$$k = 1.00$$

$$V = Q / A_F$$

$$= 3.82 \text{ fps}$$

$$h_1 = 0.23 \text{ ft}$$

$$EGL_1 = EL_0 + h_1$$

$$= 431.52 \text{ ft}$$

Head Loss Through Downstream Pipe, h₂

Friction Losses, h₂

$$h_2 = S_{EGL} * L$$

where,

$$L = 52.4934 \text{ ft}$$

$$S_{EGL} = [(Q * n) / (1.49 * A_F * R^{2/3})]^2$$

where,

Pipe Characteristics

$$\text{Dia.} = 12 \text{ in}$$

$$S_{PIPE} = 0.0035 \text{ ft/ft}$$

$$n = 0.01$$

Flow Characteristics

$$d_F = 1.00 \text{ ft}$$

$$A_F = 0.79 \text{ sf}$$

$$P_W = 3.14 \text{ ft}$$

$$R = 0.25 \text{ ft}$$

Head Loss Through Downstream Pipe, h_2 (cont.'d)

9/14/2017

$$S_{EGL} = \underline{0.00418} \text{ ft / ft}$$

$$h_2 = \underline{0.2194} \text{ ft}$$

$$\begin{aligned} EGL_2' &= EGL_1 + h_2 \\ &= \underline{431.74} \text{ ft} \end{aligned}$$

Check Entrance Condition for Critical Depth Control

$$EL_{CDS \text{ Inv.}} = \underline{430.48} \text{ ft}$$

$$d_c = \underline{0.73} \text{ ft}$$

$$\begin{aligned} EGL_C &= EL_{CDS \text{ Inv.}} + d_c + V_{dc}^2 / (2 * g) \\ &= \underline{431.58} \text{ ft} \end{aligned}$$

Identify Controlling EGL

Friction based EGL controls.

$$EGL_2 = \underline{431.74} \text{ ft}$$

Re-entry Loss into DownStream Pipe, h_3

$$h_3 = k * [V^2 / (2 * g)]$$

where,

$$k = \underline{0.20}$$

$$V = Q / A$$

$$= \underline{3.82} \text{ fps (area based on flow depth)}$$

$$h_3 = \underline{0.05} \text{ ft}$$

$$\begin{aligned} EGL_3' &= EGL_2 + h_3 \\ &= \underline{431.79} \text{ ft} \end{aligned}$$

Oil Baffle Loss, h_4

$$h_4 = k * [V^2 / (2 * g)]$$

where,

$$k = \underline{1.00}$$

$$A_{\text{Baffle}} = \underline{6.49} \text{ sf}$$

$$V = Q / A_{\text{baffle}}$$

$$= \underline{0.46} \text{ fps}$$

$$h_4 = \underline{0.0033} \text{ ft}$$

$$\begin{aligned} EGL_4 &= EGL_3 + h_4 \\ &= \underline{431.79} \text{ ft} \end{aligned}$$

Check Standard Weir Elevation

$$HL_{CDS} = \underline{0.67} \text{ ft}$$

$$\begin{aligned} EL_W' &= EGL_4 + HL_{CDS} \\ &= \underline{432.46} \text{ ft} \end{aligned}$$

$$H_W' = EL_W' - EL_{CDS \text{ INV.}}$$

$$= \underline{1.98} \text{ ft, or } \underline{23.77} \text{ in}$$

$$\text{Std. Weir Height} = \underline{21.0} \text{ in}$$

Status **Modify Std Height**

$$\text{Use } H_W = \underline{24} \text{ in, or } \underline{1.98} \text{ ft}$$

$$\begin{aligned} EL_W &= EL_{CDS \text{ INV.}} + H_W \\ &= \underline{432.46} \text{ ft} \end{aligned}$$

PEAK CONVEYANCE FLOW

9/14/2017

Tailwater Condition at Outfall, EL_0

$$EL_0 = \underline{431.29} \text{ ft (invert plus depth of flow at D/S outlet)}$$

Exit Loss from DownStream Pipe, h_1

$$h_1 = k * [V^2 / (2 * g)]$$

where,

$$k = \underline{1.00}$$
$$V = Q / A_F$$
$$= \underline{5.67} \text{ fps}$$

$$h_1 = \underline{0.50} \text{ ft}$$

$$EGL_1 = EL_0 + h_1$$
$$= \underline{431.79} \text{ ft}$$

Head Loss Through Downstream Pipe, h_2

Friction Losses, h_2

$$h_2 = S_{EGL} * L$$

where,

$$L = \underline{52.4934} \text{ ft}$$

$$S_{EGL} = [(Q * n) / (1.49 * A_F * R^{2/3})]^2$$

where,

Pipe Characteristics

$$\text{Dia.} = \underline{12} \text{ in}$$
$$S_{PIPE} = \underline{0.0035} \text{ ft/ft}$$
$$n = \underline{0.01}$$

Flow Characteristics

$$d_n = \underline{1.00} \text{ ft}$$
$$A_F = \underline{0.79} \text{ sf}$$
$$P_W = \underline{3.14} \text{ ft}$$
$$R = \underline{0.25} \text{ ft}$$

$$S_{EGL} = \underline{0.0092} \text{ ft / ft}$$

$$h_2 = \underline{0.48} \text{ ft}$$

$$EGL_2' = EGL_1 + h_2$$
$$= \underline{432.28} \text{ ft}$$

Check Entrance Condition for Critical Depth Control

$$EL_{CDS \text{ Inv.}} = \underline{430.48} \text{ ft}$$

$$d_c = \underline{0.89} \text{ ft}$$

$$EGL_C = EL_{CDS \text{ Inv.}} + d_c + V_{dc}^2 / (2 * g)$$
$$= \underline{431.93} \text{ ft}$$

Identify Controlling EGL

Friction based EGL controls.

$$EGL_2 = \underline{432.28} \text{ ft}$$

Re-entry Loss into DownStream Pipe, h_3

9/14/2017

$$h_3 = k * [V^2 / (2*g)]$$

where,

$$k = \frac{0.20}{}$$

$$V = Q / A_F$$

$$= \frac{5.67}{} \text{ fps (area based on flow depth)}$$

$$h_3 = \frac{0.10}{} \text{ ft}$$

$$EGL_3 = EGL_2 + h_3$$

$$= \frac{432.38}{} \text{ ft}$$

Oil Baffle Loss, h_4

$$h_4 = k * [V^2 / (2*g)]$$

where,

$$k = \frac{0.00}{} \text{ (Skirted-baffle model)}$$

$$A_{\text{Baffle}} = \frac{6.49}{} \text{ sf}$$

$$V = Q / A_{\text{Baffle}}$$

$$= \frac{0.69}{} \text{ fps}$$

$$h_4 = \frac{0.00}{} \text{ ft}$$

$$EGL_4 = EGL_3 + h_4$$

$$= \frac{432.38}{} \text{ ft}$$

$$HGL_4 = EGL_4 - [V_P^2 / (2*g)]$$

$$= \frac{431.88}{} \text{ ft}$$

Head over Diversion Weir, h_5

Elevation of Weir

$$EL_{\text{Weir}} = \frac{432.46}{} \text{ ft (established above)}$$

Headloss for Free Discharge Condition

$$h_{5a} = [Q / (C * L)]^{2/3}$$

where,

$$C = \frac{3.1}{}$$

$$L = \frac{3.00}{} \text{ ft}$$

$$h_{5a} = \frac{0.61}{} \text{ ft}$$

$$EGL_{5a} = EL_{\text{Weir}} + h_{5a}$$

$$= \frac{433.07}{} \text{ ft}$$

Headloss for Submerged Condition

$$d_{\text{Sub}} = \frac{0.00}{} \text{ ft (depth of submergence)}$$

$$h_{5b} = \frac{0.61}{} \text{ ft (separate submerged weir calc.)}$$

$$EGL_{5b} = EGL_4 + h_{5b}$$

$$= \frac{432.99}{} \text{ ft}$$

Identify EGL U/S of Weir

The discharge condition is Free, therefore

$$EGL_5 = \frac{433.07}{} \text{ ft}$$

Expansion Loss from U/S Pipe, h_6

9/14/2017

$$h_6 = k * [V^2 / (2 * g)]$$

where,

$$k = \underline{0.30}$$

$$V = Q / A_F \\ = \underline{5.67} \text{ fps}$$

$$h_6 = \underline{0.15} \text{ ft}$$

$$\text{EGL}_6 = \text{EGL}_5 + h_6 \\ = \underline{433.22} \text{ ft}$$

Head Loss Through Upstream Pipe, h_7

Friction Losses, h_7

$$h_7 = S_{\text{EGL}} * L$$

where,

$$L = \underline{30.1837} \text{ ft}$$

$$S_{\text{EGL}} = [(Q * n) / (1.49 * A_F * R^{2/3})]^2$$

where,

Pipe Characteristics

$$\text{Dia.} = \underline{12} \text{ in}$$

$$S_{\text{PIPE}} = \underline{0.0035} \text{ ft/ft}$$

$$n = \underline{0.01}$$

Flow Characteristics

$$d_n = \underline{1.00} \text{ ft}$$

$$A_F = \underline{0.79} \text{ sf}$$

$$P_W = \underline{3.14} \text{ ft}$$

$$R = \underline{0.25} \text{ ft}$$

$$S_{\text{EGL}} = \underline{0.0092} \text{ ft / ft}$$

$$h_7 = \underline{0.28} \text{ ft}$$

$$\text{EGL}_7' = \text{EGL}_6 + h_7 \\ = \underline{433.50} \text{ ft}$$

Check Entrance Condition for Critical Depth Control

$$\text{EL}_{\text{U/S Inv.}} = \underline{430.58} \text{ ft}$$

$$d_c = \underline{0.89} \text{ ft}$$

$$\text{EGL}_C = \text{EL}_{\text{CDS Inv.}} + d_c + V_{dc}^2 / (2 * g) \\ = \underline{432.04} \text{ ft}$$

Identify Controlling EGL

Friction based EGL controls.

$$\text{EGL}_7 = \underline{433.50} \text{ ft}$$

$$\text{HGL}_7 = \text{EGL}_7 - [V^2 / (2 * g)] \\ = \underline{433.00} \text{ ft}$$

$$\text{Freeboard} = \underline{-0.91} \text{ ft (at first upstream structure)}$$



**CDS ESTIMATED NET ANNUAL SOLIDS LOAD REDUCTION
BASED ON THE RATIONAL RAINFALL METHOD
BASED ON A FINE PARTICLE SIZE DISTRIBUTION**



Project Name: Derry Side Road Subdivision	Engineer: Stantec
Location: Beckwith, ON	Contact: Ana Paerez, P. Eng.
OGS #: 2	Report Date: 14-Sep-17

Area 5.47 ha	Rainfall Station # 215	
Weighted C 0.33	Particle Size Distribution FINE	
CDS Model 3030	CDS Treatment Capacity 85 l/s	

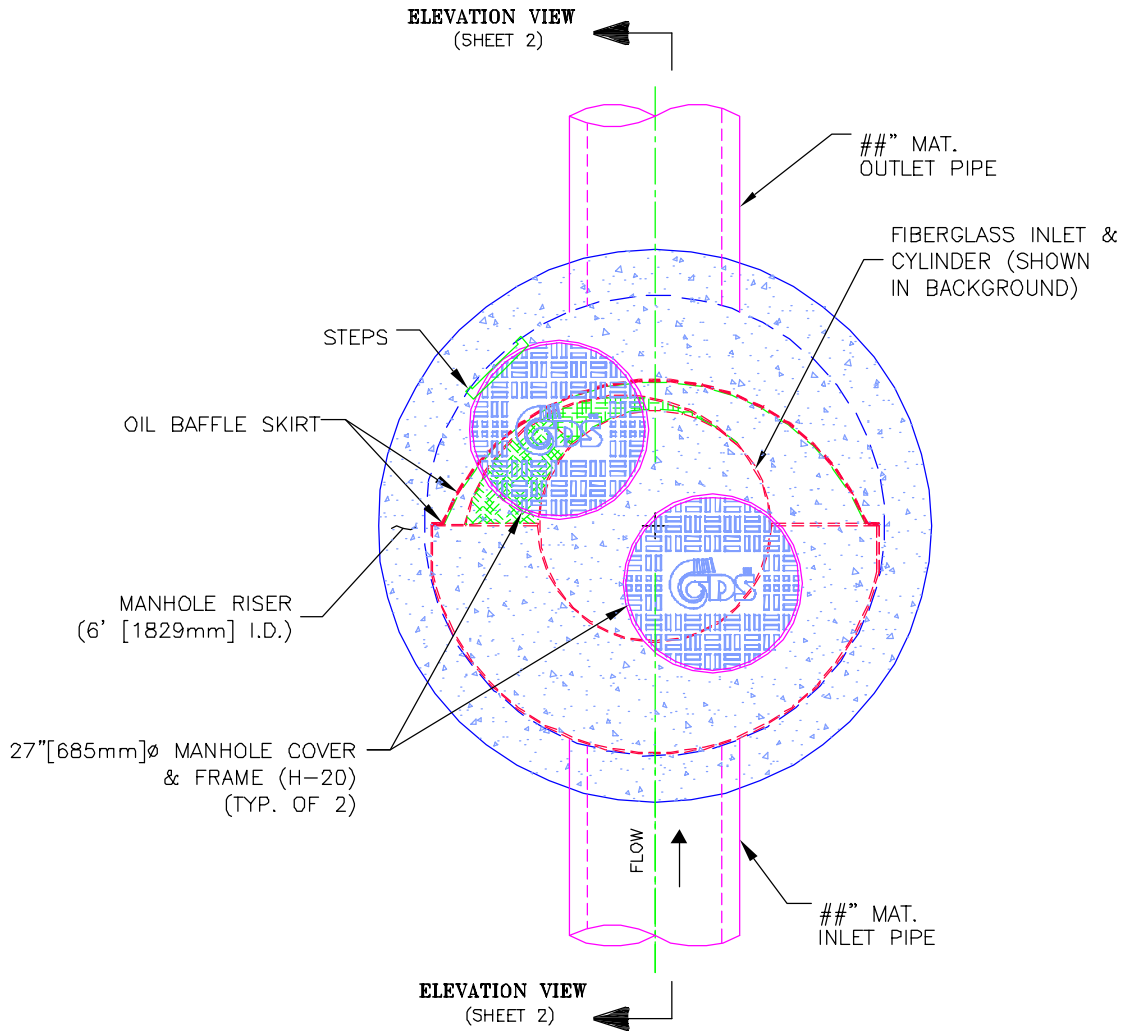
<u>Rainfall Intensity¹</u> (mm/hr)	<u>Percent Rainfall Volume¹</u>	<u>Cumulative Rainfall Volume</u>	<u>Total Flowrate (l/s)</u>	<u>Treated Flowrate (l/s)</u>	<u>Operating Rate (%)</u>	<u>Removal Efficiency (%)</u>	<u>Incremental Removal (%)</u>
0.5	9.2%	9.2%	2.5	2.5	3.0	98.0	9.0
1.0	10.6%	19.8%	5.0	5.0	5.9	97.2	10.3
1.5	9.9%	29.7%	7.5	7.5	8.9	96.3	9.5
2.0	8.4%	38.1%	10.0	10.0	11.8	95.5	8.0
2.5	7.7%	45.8%	12.5	12.5	14.8	94.6	7.3
3.0	5.9%	51.7%	15.1	15.1	17.7	93.8	5.6
3.5	4.4%	56.1%	17.6	17.6	20.7	92.9	4.0
4.0	4.7%	60.7%	20.1	20.1	23.6	92.1	4.3
4.5	3.3%	64.0%	22.6	22.6	26.6	91.2	3.0
5.0	3.0%	67.1%	25.1	25.1	29.5	90.4	2.7
6.0	5.4%	72.4%	30.1	30.1	35.4	88.7	4.8
7.0	4.4%	76.8%	35.1	35.1	41.3	87.0	3.8
8.0	3.5%	80.3%	40.1	40.1	47.3	85.3	3.0
9.0	2.8%	83.2%	45.2	45.2	53.2	83.6	2.4
10.0	2.2%	85.3%	50.2	50.2	59.1	81.9	1.8
15.0	7.0%	92.3%	75.3	75.3	88.6	73.5	5.1
20.0	4.5%	96.9%	100.4	85.0	100.0	59.4	2.7
25.0	1.4%	98.3%	125.5	85.0	100.0	47.5	0.7
30.0	0.7%	99.0%	150.5	85.0	100.0	39.6	0.3
35.0	0.5%	99.5%	175.6	85.0	100.0	34.0	0.2
40.0	0.5%	100.0%	200.7	85.0	100.0	29.7	0.2

	Removal Efficiency Adjustment ² = 6.5%
	Predicted Net Annual Load Removal Efficiency = 82.1%
	Predicted % Annual Rainfall Treated = 98.0%

1 - Based on 42 years of hourly rainfall data from Canadian Station 6105976, Ottawa ON
 2 - Reduction due to use of 60-minute data for a site that has a time of concentration less than 30-minutes.
 3 - CDS Efficiency based on testing conducted at the University of Central Florida
 4 - CDS design flowrate and scaling based on standard manufacturer model & product specifications



PLAN VIEW

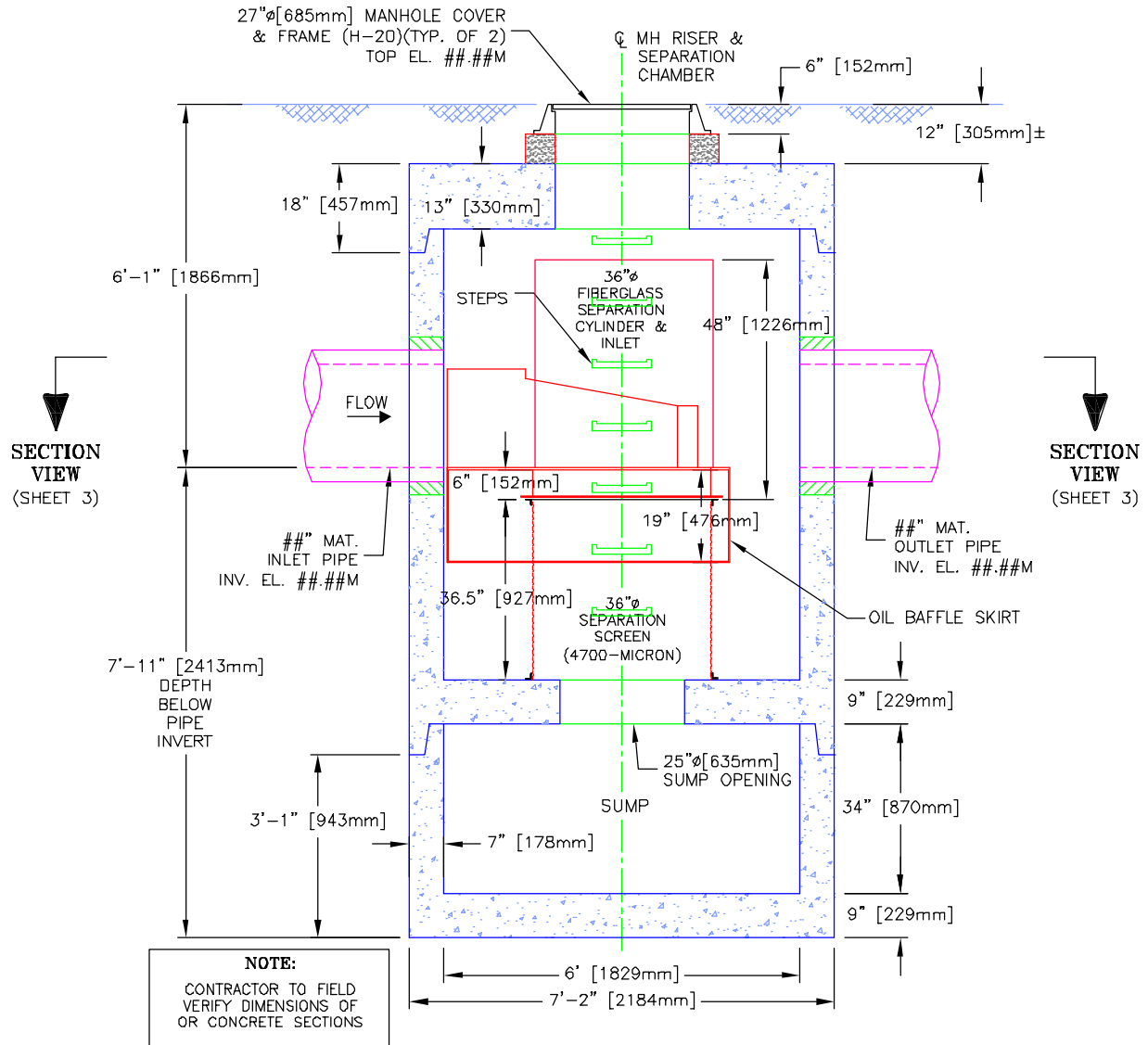


CDS MODEL PMSU30_30m, 3.0 CFS TREATMENT CAPACITY STORM WATER TREATMENT UNIT

	PROJECT NAME CITY, STATE	JOB#	CAN-##-###	SCALE 1" = 2.5'
		DATE	##/##/##	SHEET
		DRAWN	INITIALS	1
		APPROV.		



ELEVATION VIEW



CDS MODEL PMSU30_30m, 3.0 CFS TREATMENT CAPACITY STORM WATER TREATMENT UNIT



PROJECT NAME
CITY, STATE

JOB# CAN-##-###

DATE ##/##/##

DRAWN INITIALS

APPROV.

SCALE
1" = 3'

SHEET

2

DERRY SIDE ROAD SUBDIVISION – BECKWITH, ON CONCEPTUAL STORMWATER MANAGEMENT REPORT

Appendix D Conceptual Drawings
September 25, 2017

Appendix D CONCEPTUAL DRAWINGS