

CAIVAN PERTH DEVELOPMENT - HYDROLOGIC AND HYDRAULIC CONDITIONS REPORT

FEBRUARY 2023



Prepared For:

Caivan Communities
3713 Borrisokane Road
Nepean, ON
<Postal Code>
<Phone Number>

Prepared By:

J.F. Sabourin and Associates Inc.
52 Springbrook Drive,
Ottawa, ON
K2S 1B9
T 613-836-3884 F 613-836-0332

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In Perth, Ontario

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A handwritten signature in black ink that reads 'J. Burnett'.

Jonathon Burnett, B.Eng, P.Eng
(J.F. Sabourin and Associates Inc.)

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1 Introduction

This Report has been prepared to provide a comprehensive understanding of the current hydrologic and hydraulic conditions of the future residential development site located at 141 Peter Street, Perth, Ontario, referred here on as the “Perth GC development”. The report is intended to serve as a baseline for future studies and design work related to water resources management, floodplain management, and other hydrologic and hydraulic analyses.

Figure 1 below outlines the development site, major watercourses and the Grants Creek wetland. As shown in this figure the development is located between the Tay River and Grants Creek, with the Grants Creek wetland located to the south of the site, additional details regarding the development and drainage areas have been outlined in Section 2 below. The report also covers a range of hydrologic and hydraulic characteristics, which includes an overview of surface water monitoring completed by JFSA in 2022, an updated existing floodplain delineation, a conceptual existing conditions water budget based on continuous hydrologic modelling and preliminary SWM pond sizing for the future development.

Each of the key items addressed in the report has been laid out in individual sections to ensure that the report provides a comprehensive and easy-to-understand overview of each of the components of the hydrologic and hydraulic conditions in the study area.

Figure 1. Site Overview



2 Existing Drainage Area

The following section provides an overview of the various drainage areas surrounding and within the development study area and outlines the land use compositions of each of the major watersheds.

2.1 Development Site

As outlined in **Figure 1** above the site is bound by the Tay River to the north and east of the site and by Grants Creek to the south. Under existing conditions, the Perth development site has a total drainage area of approximately **44.86 ha**, with **22.85 ha** currently draining north to the Tay River and the remaining **22.01 ha** draining south to the nearby wetland and Grants Creek. Currently, the development site is approximately split 50-50 between Grants Creek and the Tay River. The site under existing conditions consists primarily of a golf course with well-maintained lawns, surrounded by irregular forest patches. Refer to **Figure A1** in **Appendix A**, for a visual overview of the study area's pre-development drainage divide.

Under proposed conditions, the Perth development has a total drainage area of approximately **44.86 ha**, with **28.54 ha** draining north to the Tay River with the remaining **16.32 ha** draining south to the nearby wetland and Grants Creek. This is a drainage area adjustment between the two watersheds of **5.69 ha**. Note that efforts have been made to maintain the existing drainage areas within the development site as much as possible with consideration for grading and servicing limitations. Refer to **Figure A2** in **Appendix A**, for a visual overview of the study area's post-development drainage divide.

2.2 Grants Creek

The total existing drainage area of Grants Creek (upstream and surrounding lands - minus the development site) is approximately **9351.78 ha**. A land use summary in **Table 2.1** below shows that land cover within the drainage area is primarily natural features (**60.8%**), agricultural lands (**23.4%**), and open water (**9.3%**). The remainder of the land cover within the watershed is bedrock (**4.8%**) and community/infrastructure (**1.7%**).

Table 2.1 – Grant's Creek - Land Use Summary

Land Cover	Area (ha)	Total Area (ha)	Percentage of Total
Natural (Forest/Meadows/Swamps)	5689.8	9351.78	60.8%
Agricultural	2189.1	9351.78	23.4%
Water	868.3	9351.78	9.3%
Bedrock	447.2	9351.78	4.8%
Community/Infrastructure	157.3	9351.78	1.7%

Under post-developed conditions, the Perth GC Development would decrease the total area of the Grants Creek watershed by around **5.69 ha**, a change of **0.06%**. **Figure A3** provides an overview of the various Grants Creek drainage areas and land use.

Table 2.2 - Grants Creek Wetland Drainage Area Change

Development Conditions	Upstream and Surrounding Area (ha)	Perth GC Development (ha)	Total Area (ha)	Difference	
				(ha)	(%)
Pre-Dev	9351.78	22.01	9373.8	-	-
Post-Dev	9351.78	16.32	9368.1	-5.69	0.06%

2.3 Tay River

The total drainage area of the Tay River watersheds (upstream and surrounding lands – minus the development site) is around **58,382.7 ha**. A land use summary in **Table 2.3** below shows that land cover within the drainage area is primarily natural features (**64.7%**), agricultural lands (**14.3%**), and open water (**13.9%**). The remainder is bedrock (**6.2%**), and community/infrastructure (**0.9%**).

Table 2.3 – Tay River - Land Use Summary

Land Cover	Area (ha)	Total Area (ha)	Percentage of Total
Natural (Forest/Meadows/Swamps)	37799.6	58382.7	64.70%
Agriculture	8325.8	58382.7	14.30%
Water	8131.2	58382.7	13.90%
Bedrock/Sand/Gravel	3594.9	58382.7	6.20%
Community/Infrastructure	531.2	58382.7	0.90%

As shown in **Table 2.4** below, the post-developed Perth GC site would result in an increase of **5.69 ha** to the Tay River Watershed, representing a change in the total drainage area of **0.009%**. **Figure A4** outlines the total drainage area and land use types within the watershed.

Table 2.4 - Tay River Wetland Drainage Area Change

Conditions	Upstream and Surrounding Area (ha)	Perth GC Development (ha)	Total Area (ha)	Difference	
				(ha)	(%)
Pre-Dev	58382.7	22.85	58405.5	-	-
Post-Dev	58382.7	28.54	58411.2	5.69	0.009%

2.4 Summary

This section provided an overview of the various drainage areas around and within the development study area. As discussed above, under existing conditions the Perth development has a total drainage area of approximately **44.86 ha**, with **22.86 ha** currently draining north, while the remaining **22.01 ha** draining south to the nearby wetland and Grants Creek. The development is approximately split 50-50 draining to Grants Creek and the Tay River. The primary land cover of the Grants Creek and Tay River watersheds are natural features, agriculture, and open water.

Under proposed conditions, the Perth GC development has a total drainage area of approximately **44.86 ha**, with **28.54 ha** draining north to the Tay River and **16.32 ha** draining south to the nearby wetland and Grants Creek. The total existing drainage area upstream of and surrounding Grants Creek is **9351.8 ha**. The proposed development would result in an overall decrease of **5.69 ha**, or **0.06%** to the total Grants Creek watershed. The Tay River drainage area would receive an increase of **5.69 ha**, an increase of **0.009%** to the Tay River watershed. Given the size of these watersheds, and the location of the drainage area change (at the confluence of the two watersheds) it is unlikely that this change under post-development conditions will have a quantifiable impact on the hydraulic and hydrologic conditions of the surrounding watercourses.

3 Surface Water Monitoring (2022)

As a part of the Perth GC development, J.F. Sabourin & Associates (JFSA) has been commissioned by Caivan Communities to complete surface water monitoring throughout the subject area. These works are intended to develop a strong understanding of how the watercourses react to various environmental conditions, and how flows and water levels are related at key locations within the surrounding lands. This work included surface water monitoring and precipitation monitoring in the study area from June 2022 to November 2022. The following section briefly outlines the data obtained and conclusions drawn from this 2022 monitoring window.

3.1 Overview

The 2022 monitoring program consisted of 2 level loggers, 1 barometric logger, and 1 rain gauge implemented on and around the site. A level logger was installed on Grants Creek at Glen Tay Road, on the upstream side of the road crossing, to monitor the flow contributions from the upstream drainage area to the Grants Creek wetland. A secondary level logger was installed within the Grants Creek Wetland near the confluence with the Tay River to monitor water levels within the wetland itself. Both the Barometric logger and rain gauge were located within the existing Perth Golf Course site. Refer to **Figure B1** for the monitoring locations from 2022.

3.2 Rainfall

A tipping bucket rain gauge was installed on-site on **June 10, 2022**, until **November 2, 2022**, providing **152 days** of rainfall data. The gauge was placed in a flat, open area on a platform to avoid any interference from nearby vegetation and trees and to withstand large rainstorms and wind without shifting. The gauge was calibrated before installation, and the lip of the funnel was installed level with the surrounding ground. The rain gauge was inspected monthly to ensure that it was level and functioning properly, and the data recorded during that month was downloaded.

Throughout the monitoring period of **June 10, 2022**, until **November 2, 2022**, there was a total of **325.3 mm** of rainfall. Based on the rainfall data acquired during this window 'significant' rainfall events were then identified. For this study, a 'Significant Rainfall Event' was defined as a single event if the total rainfall volume was greater than 5 mm and was followed by at least 12 hours without any additional rainfall. A total of **18** significant rainfall events took place in 2022. The largest event recorded over this duration occurred on July 18, from 09:40 AM to 21:20 PM (duration of 11:40) and had a total rainfall volume of **38.3 mm**. **Table 3.1** provides a full summary of these significant events.

Table 3.1: Significant Rainfall Events, 2022
(Events with more than 5 mm and separated by at least 12 hours of no rain)

Event	Start Date/Time	Finish Date/Time	Duration (Hr : Min)	Total Rainfall (mm)
1	2022-06-21 10:00	2022-06-21 14:40	4:40	6.1
2	2022-06-29 12:10	2022-06-29 17:50	5:40	6.2
3	2022-07-12 13:50	2022-07-12 14:35	0:45	13.1
4	2022-07-18 09:40	2022-07-18 21:20	11:40	38.3
5	2022-07-22 17:10	2022-07-22 17:40	0:30	13.9
6	2022-07-24 21:15	2022-07-25 00:35	3:20	8.4
7	2022-08-07 20:55	2022-08-08 02:10	5:15	17.9
8	2022-08-21 12:20	2022-08-21 17:15	4:55	8.9
9	2022-08-22 14:55	2022-08-22 16:35	1:40	7.4
10	2022-08-22 23:10	2022-08-23 00:30	1:20	21.6
11	2022-08-29 17:25	2022-08-29 18:35	1:10	20.9
12	2022-08-30 13:20	2022-08-30 18:45	5:25	7.1
13	2022-09-03 20:45	2022-09-03 23:00	2:15	10.1
14	2022-09-13 12:00	2022-09-14 06:05	18:05	18.3
15	2022-09-18 11:00	2022-09-19 01:20	14:20	16.8
16	2022-09-19 06:35	2022-09-20 07:50	1:15	24
17	2022-10-13 08:00	2022-10-13 21:15	13:15	8.6
18	2022-10-17 05:20	2022-10-17 19:00	13:40	10.8

The Rainfall-Duration Max Intensity summary for the 2022 collected rainfall has been compared to the IDF curves for Perth (**Table 6.1**) and assessed for various rainfall intervals, with the summary outlined below in **Table 3.2** for this study period. Based on this analysis it was seen that the rainfall intensities observed in 2022 equate to either less than a 2-Year or 5-Year event, depending on the duration observed.

Table 3.2: Rainfall Duration/Max Intensity Summary, 2022

	Duration	Maximum Measured Rainfall Intensity (mm/hr)	Return Periods Based on Ottawa Airport IDF (Years)
2022	5 Minute	93.60	<2-Year
	10 Minute	76.20	<5-Year
	15 Minute	62.00	<5-Year
	30 Minute	31.80	<2-Year
	60 Minute	21.10	<5-Year
	2 Hour	10.80	<2-Year
	6 Hour	4.65	<2-Year
	12 Hour	3.19	<2-Year
	24 Hour	1.60	<2-Year

3.3 Glen Tay Road Crossing

A level logger was placed at the upstream side of Glen Tay Road on Grants Creek. The minimum, maximum and average for both water temperature and depth, as well as the number of days with zero depth readings, are provided in **Table 3.3**. Graphs showing continuous water depth vs. rainfall events are available in **Appendix B**.

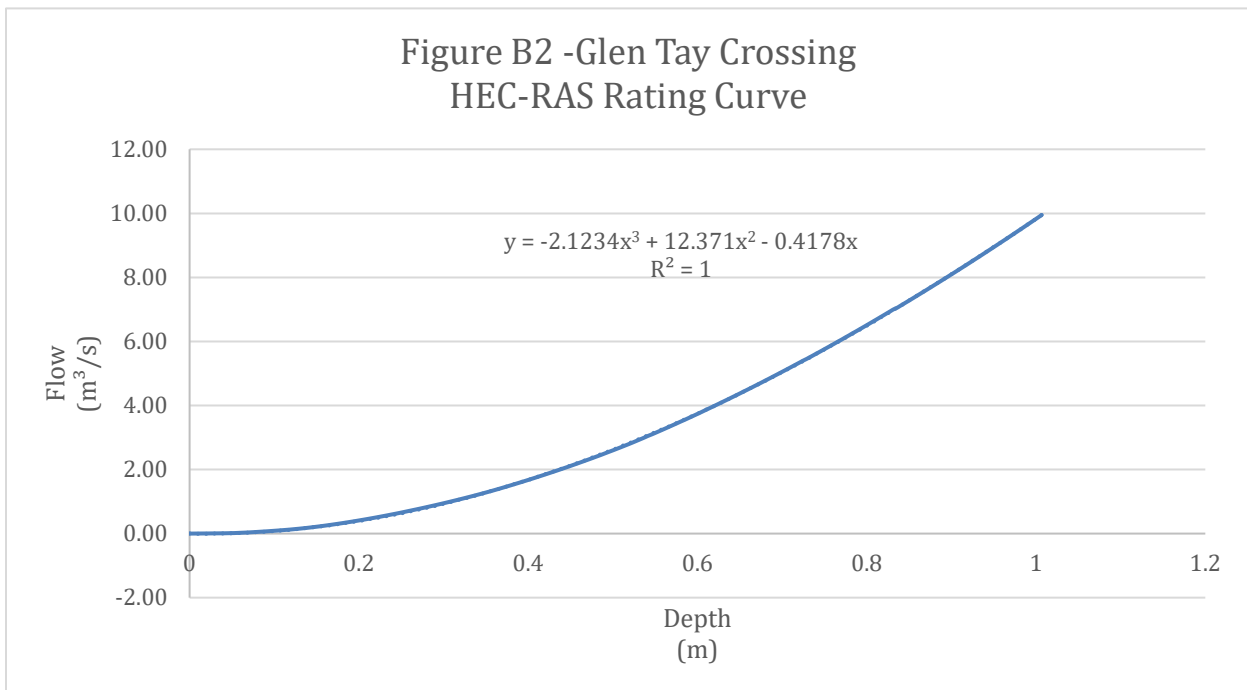
Table 3.3: Glen Tay Road Level Logger Monitoring Summary, 2022

Site	Monitoring Duration (days)		Water Temperature (°C)	Water Depth (m)	Duration of measured zero depth
Glen Tay Road	152	Min	5.3	0.07	0 days / 0%
		Max	30.9	0.38	
		Avg	18.6	0.18	

Based on the above results the average water depth at this location was **18 cm**, and only fluctuated by **31 cm** over the full monitoring period. While the average water temperature was **18.6 °C** varied by **25.6 °C** over the monitoring period. Note that there was a constant based flow at this location and the channel never went dry during the monitoring period.

3.4 Glen Tay Road Rating Curve / Flow Derivation

A detailed survey of the bridge crossing under Glen Tay Road was completed by JFSA field staff, and the crossing details were incorporated into a simple HEC-RAS model to derive a rating curve (Depth vs Flow) relationship at this location (refer to **Figure B2**), to allow for the continuous water level depths measured at this location to be converted to flows. This analysis assumes that the crossing operates under inlet control the entire time and that downstream/tailwater conditions have no impact on the flows through this crossing.



Based on the rating curve derived by HEC-RAS the total flow through this crossing was **49,759,017 m³**. There was a total rainfall volume of **325.3 mm** recorded by the gauge for this duration and the total drainage area to this location is approximately **7,986.2 ha**. Based on the above the upstream area has a runoff coefficient of **1.92**, which is not possible. As such the assumption that this crossing operates under inlet control may not always be valid and future monitoring will require a level logger both upstream and downstream of this crossing to accurately capture the impacts that the tailwater has on flows through this crossing and to the wetland.

3.5 Grants Creek Wetland

A level logger was placed at the downstream extent of the Grants Creek wetland near the confluence with the Tay River. The minimum, maximum and average for both water temperature and depth, as well as the number of days with zero depth readings, are provided in **Table 3.4**. Graphs showing continuous water depth vs. rainfall events are available in **Appendix B**.

Table 3.4: Grants Creek Wetland Level Logger Monitoring Summary, 2022

Site	Monitoring Duration (days)		Water Temperature (°C)	Water Depth (m)	Duration of measured zero depth
Grants Creek Wetland	152	Min	7.0	0.320	0 days / 0%
		Max	26.8	0.558	
		Avg	18.8	0.411	

Based on the above results the average water depth at this location was **41 cm**, and only fluctuated by **24 cm** over the full monitoring period. While the average water temperature was **18.8 °C** and varied by **19.8 °C** over the monitoring period. Note that there was a constant based flow at this location and the channel never went dry during the monitoring period.

3.6 Tay River (WSC Gauge)

Water Survey Canada (WSC) has an active gauge on the Tay River approximately 500 m downstream of the Perth GC development site which reports both water levels and flows at this location. This location includes contributions from both the Tay River and Grants Creek. The flow and level data recorded at the gauge have been overlaid with the rainfall data collected by JFSA from the subject site to give an overview of the response of the Tay River and to approximate a runoff coefficient. Full figures for this location have been provided in **Appendix B**.

Based on the JFSA rain gauge a total rainfall volume of **325.3 mm** fell over the window from June 10th to November 2nd, 2022. Water Survey Canada indicates that the gauge at this location has a total drainage area of approximately **66,100 ha** with a total flow volume of **54,152,004 m³** over this duration. Based on the above the Tay River at this location has a runoff coefficient of approximately **0.25**, which is in line with the land use for this area.

3.7 Summary

Rainfall and surface water monitoring was completed on the site from June 2022 to November 2022. The rainfall monitoring recorded **18** significant events (with volumes greater than 5mm) but all rainfall events recorded this year had return periods less than the 5-year event. Water level monitoring at the Glen Tay Road crossing indicated that tailwater impacts at this location may affect the flows through the crossing and to the wetland, as such additional loggers are advised for future monitoring to capture these impacts. The level logger in the Glen Tay wetland showed that the wetland water levels fluctuated by only **24 cm** over the full monitoring period. Combining the rainfall data with the flows recorded at the water survey Canada gauge, it was found that the Tay River at this location (which includes both the Tay River and Grants Creek) has a runoff coefficient of approximately **0.25**. As no significant rainfall events were observed in this year of monitoring it is advised that the surface water monitoring program is to be continued in the following years.

4 Floodplain Mapping Update

Accurate floodplain mapping is required for the future Perth GC development. Upon review of the floodplain mapping based on the 2013 model of the Tay River provided by the Rideau Valley Conservation Authority (RVCA), J.F. Sabourin & Associates (JFSA) determined that additional topographic data would improve/refine the floodplain boundaries affecting the subject property. This included acquiring higher resolution site-specific LiDAR of the area and completing field checks to determine culvert locations and elevations. This resulted in a site-specific refinement of the floodplain extent on the subject lands. Note that no modifications have been made to the existing hydraulic model produced by RVCA in 2013, simply the topography that the flood elevations have been mapped on has been updated using the latest available LiDAR and onsite topographic survey of existing culverts through the existing golf course.

4.1 Updated Analysis

Site-specific imagery was collected by First Base Solutions Inc. retained by David Schaeffer Engineering Ltd (DSEL), on November 7th, 2021 at a ground sample distance of 6 cm and controlled with Airborne Kinematic GPS and Surveyed Ground Control points. The resulting mapping was compiled with a DTM capable of producing 0.25m contours and map accuracies of +/- 12cm at a 95% confidence level on well-defined, easily visible objects within the imagery. Note that this LiDAR has been used in other analyses outlined in this report such as section 2.1-Development Site. This site-specific data is at a much higher resolution than the 1m contour data used in the RVCA model. **Figure C1** outlines the regulatory floodplain boundary based on the work completed by RVCA as a part of the “Tay River Flood Risk Mapping Report, Glen Tay Road to Lower Rideau Lake, 2013”, and is the current official floodplain extent for this location. JFSA used the newer LiDAR to run the original HECRAS model with updated terrain to delineate a refined floodplain extent shown in **Figure C2**. It is important to note that no model parameters have been changed from the RVCA model of record for the Tay River. The floodplain extents produced by this model have simply been remapped using the latest available topographic data.

4.2 Field Verification

To further the accuracy of the results obtained through the updated topographic data, staff from J.D Barnes Limited (JDB) surveyed culvert locations on the golf course. Several key locations were identified as potentially having a direct impact on the floodplain extent outcome, as they would allow the Tay River floodplain to connect to Grant’s Creek through the subject property. JDB field staff surveyed the culvert invert and obvert elevations to determine whether floodwaters would be permitted to pass through. Results from the survey can be seen in **Figure C3**. All culverts surveyed were determined to be below their adjacent floodplain elevation, which means that they would allow floodwaters to spill onto the proposed development site between the Tay River and Grant’s Creek.

4.3 Summary

Based on the compiled data and completed field checks, JFSA is confident in the accuracy of the floodplain extent generated using the updated topographic data. The refined boundaries produced by JFSA are georeferenced and have been provided to JDB and Caivan (Perth GC) Ltd. in support of the development of the proposed draft plan of subdivision and used in the balance cut fill analysis completed by DSEL. Note that no modifications have been made to the existing hydraulic model produced by RVCA in 2013, simply the topography that the flood elevations have been mapped on has been updated.

5 Existing Water Budget Modelling

A continuous SWMHYMO hydrologic model has been developed to assess the site's pre-development water budget. The model makes use of the pre-development water budget analysis completed by GEMTEC for this site. Model parameters have been adaptively adjusted as a part of this analysis to ensure the continuous simulation results are in line with the static MOE-style water budget completed by GEMTEC.

5.1 Continuous Simulation Modelling

The continuous SWMHYMO model was run using 36 years of hourly rainfall data from the Ottawa International Airport from 1967 to 2003 (excluding missing 2001 rainfall data), and the average annual evaporation, infiltration and runoff volumes from the subject site were computed and compared. Note that this rain gauge is generally only operational for the months of April-November. Outside of this window precipitation is more likely to be in the form of snowfall and the soils are also more likely to be frozen, making it difficult to simulate such conditions with a hydrologic model using conventional parameters, as such, this period has not been considered in the analysis. Note that GEMTEC's water budget analysis considered the full year, while the JFSA analysis only considered April to November. To resolve this disconnect the total percentage of rainfall that evaporates infiltrates and runs off each year has been matched as an alternative to matching annual volumes, which is not possible due to the difference in analysis windows.

5.2 Model Parameters

As a part of this analysis the Initial Abstraction (IA) value and Curve Number (CN) values have been iteratively adjusted to calibrate the model to produce similar results to the GEMTEC water budget. It is justifiable to adjust the IA value as it is known that the typical initial abstraction/wetting loss that occurs throughout the year fluctuates with the seasons and amount of vegetation present. Additionally, although CN can be derived empirically by simply looking at the land use and soil type alone, for natural lands again the volume of runoff that infiltrates varies throughout the year depending on the soil conditions (High runoff in the winter-freshet when the soils are either frozen or saturated and very little runoff in the summer when the soils are dry) and the degree of vegetation present throughout the year.

Based on this analysis the typical average annual Initial Abstraction value for the site was found to be 8.75 mm. Although this is relatively high compared to typical IA values assumed for grassed lands (5 mm), it is within the range outlined in the Design & Construction of Urban Stormwater Management Systems, ASCE, (1992) for vegetated areas which range from 2.5 mm to 12.7mm depending on the extent and type of vegetation present. Based on this analysis the typical average CN value for the site is 90 and 92 for the Grants Creek and Tay River drainage areas respectively. Again, these values are higher than what is typically assumed for design storms due to two factors; the water budget analysis considers winter /spring freshet months when the soils are frozen and little infiltration will occur, where CN values of 95-99 are typically assumed for these conditions. Additionally, a large portion of the site is currently bedrock at the surface or with very shallow overburden, as such these areas are treated as impervious (CN 99).

It is important to note that the model parameters adopted above are an annual average representation of the site and will fluctuate throughout the year with various seasonal changes. As such the typical Textbook IA and CN values have been adopted for the preliminary SWM ponding sizing completed in Section 6 below, as the design storms assumed for that analysis area based on summer rainfall events.

5.3 Model Results

The complete SWMHYMO modelling input and summary files have been provided in **Appendix D. Table D.1 and D.2** provide a full summary of the SWMHYMO modelling, based on the 39 years of data, and outline the maximum, minimum and average volumes and percentages of precipitation that evaporate infiltrate and runs off for the Grants Creek and Tay River portions of the development site respectively. **Table 5.1** below is an excerpt from this summary.

Table 5.3: Pre-Development Water Budget based on Continuous Simulations

Location	Precipitation (mm)	Total Evaporation (mm)	Total Infiltration (mm)	Total Runoff (mm)
Grants Creek	589.1	361.2 62%	85.2 15%	142.8 24%
Tay River	589.1	361.2 62%	93.9 16%	134.0 22%

Based on the continuous simulations using 39 years of historical rainfall data it was determined that for the total development site, approximately **22-24%** of the annual rainfall will result in runoff, **62%** will evaporate and **15-16%** will infiltrate.

5.4 Summary

Continuous hydrologic modelling has been completed which has made use of the water budget modelling completed by GEMTEC. Based on this analysis it was determined that under pre-development conditions for the total development site, approximately **22-24%** of the annual rainfall will result in runoff, **62%** will evaporate and **15-16%** will infiltrate.

6 Preliminary SWM Facility Sizing

The following section details the preliminary stormwater management (SWM) facility sizing for the development site based on a post-development concept plan. The various SWM facilities throughout the site will provide water quality treatment, peak flow attenuation, and flood control for the project site and have been sized to ensure that total peak flows to both Grants Creek and the Tay River match Pre-Development conditions. This analysis has been completed using SWMHYMO hydrologic modelling software, as it is well suited to simulating large undeveloped lands as well as lumped conceptual future development lands. Note that this analysis has simply been completed to provide an order of magnitude of the required storage volume of the various possible SWM facilities throughout the site, and does not give any directive on exactly where or how this volume should be provided, which will be addressed during detailed design. The primary intention of this study is to ensure that sufficient land is set aside under post-development conditions to ensure that there is adequate room for SWM facilities to meet the objectives specified above.

6.1 Design Storms

Design storms for the development were derived using historical rainfall data outlined in the MTO IDF Curve lookup tool for the exact site locations. Full details of this tool and IDF data for this location can be found using the link below.

http://www.eng.uwaterloo.ca/~dprincz/mto_site/results_out.shtml?coords=44.892975,-76.275126

Table 6.1 below outlines the rainfall intensity provided in the MTO tool. These intensities were then fit to the formula below to derive A, B and C values which were then used to derive synthetic designs storms. For this analysis, the 3-hour Chicago and 24-Hour SCS design storms were used for both pre and post-development.

$$\text{Rainfall Intensity} \left(\frac{\text{mm}}{\text{hr}} \right) = \frac{A}{(t_c + B)^C}$$

Table 6.1: Rainfall Intensity – Perth – MTO IDF Tool

Return Period (Yr)	5 mins	10 mins	15 mins	30 mins	60 mins	2 hrs	6 hrs	12 hrs	24 hrs	A	B	C
2	115.9	71.4	53.8	33.1	20.4	12.6	5.8	3.6	2.2	362.018	0.102	0.702
5	153.4	94.5	71.2	43.8	27.0	16.6	7.7	4.8	2.9	478.921	0.106	0.701
10	178.9	110.2	83.0	51.1	31.5	19.4	9.0	5.5	3.4	559.506	0.102	0.702
25	210.2	129.5	97.5	60.1	37	22.8	10.6	6.5	4.0	655.462	0.104	0.701
50	233.4	143.8	108.3	66.7	41.1	25.3	11.7	7.2	4.5	723.892	0.087	0.700
100	256.7	158.1	119.1	73.4	45.2	27.8	12.9	8.0	4.9	796.709	0.078	0.700

6.2 Drainage Areas

Figure E1 provides an overview of the development area under pre-development conditions. For this analysis under pre-development conditions, the site has simply been broken into two subcatchments, one that represented the development area contributions to the Tay River and one that represented the development area contribution to Grants Creek. As outlined above in

section 2.1 the site under existing conditions is essentially a 50-50 split to Grants Creek and the Tay River.

6.3 Land Use

Under pre-development conditions, the site primarily consists of a mix of manicured grass (golf course) surrounded by forest. Land use data has been taken from Southern Ontario Land Resource Information System (SOLRIS) v3.0 Land Use Data, publicly available through Land Information Ontario (LIO). **Figure E2** in **Appendix E** provides a visual overview of the respective land use data for each of the subcatchments within the study area.

6.4 Soil/Infiltration Data

Soil data within the study area has been taken from Soil Survey Complex Data publicly available from Land Information Ontario (LIO). **Figure E3** in **Appendix E** provides a visual overview of the respective soil type data for each of the subcatchments within the study area. From this data the site primarily consists of Monteagle and Monteagle Sandy Loam soils, which are considered a Type B SCS soil group. The site also consists of Muck and North Gower soils, which are considered a Type D SCS soil group.

6.5 Curve Number (CN)

Curve Numbers (CN) were calculated, based on underlying Land Use Type and Soil Classification at each location within the subcatchments based on values outlined in Tables A2 and A3 in the SWMHYMO Manual. Each Curve Number was then weighted based on the total area within a given subcatchment to determine the weighted CN for that subcatchment. Full CN derivation Tables have been provided in **Table E1** in **Appendix E**.

6.6 Time to Peak

Flow paths have been discretized based on the topographic data using GIS tools and the longest major flow path within each subcatchment identified; refer to **Figure E4** in **Appendix E** for the flow paths discretized for each subcatchment. The upstream and downstream topographic elevations and flow lengths were identified for each subcatchment and used in the calculations. For these natural subcatchments, the Federal Aviation Administration (FFA) method was determined to be the most appropriate method to calculate the Time to Peak. Full details of these calculations have been provided in **Table E2** in **Appendix E**, along with other time-to-peak values using alternative tp calculation methods.

6.7 Initial Abstraction

For undeveloped lands, an initial abstraction value of 5 mm has been assumed which is typical for undeveloped lands commonly used throughout Ontario (parameters are in line with typical rates per City of Ottawa Storm Sewer Design Guidelines). Full SWMHYMO modelling input and summary files for pre-development conditions have been provided in **Appendix E**

6.8 Pre-Development Results

As outlined above the model has been run using both the 3-hour Chicago and 24-hour SCS design storms, for the 2-, 5-, 10-, 25-, 50- and 100-Year events as well as the 25mm event. **Table 6.2** below outlines the peak flows from the development site to both Grants Creek and the Tay River under pre-development conditions. Note that although the drainage area to Grants Creek is

slightly smaller than that to the Tay River, the Grants Creek drainage area is producing slightly larger peak flows for most events. This is due to the fact that the Grants Creek drainage areas are slightly steeper, which results in higher peak flows for an equivalent area.

Table 6.2 – Pre-Development Peak Flow Summary

Event	Grants Creek (22.01 ha) Peak Outflow (m ³ /s)	Tay River (22.86 ha) Peak Outflow (m ³ /s)
25MMC3H	0.125	0.126
2YRCHI3HR	0.149	0.150
5YRCHI3HR	0.288	0.285
10YRCHI3HR	0.399	0.393
25YRCHI3HR	0.559	0.546
50YRCHI3HR	0.688	0.669
100YRCHI3HR	0.830	0.804
2YRSCS24HR	0.463	0.444
5YRSCS24HR	0.790	0.750
10YRSCS24HR	1.044	0.986
25YRSCS24HR	1.382	1.298
50YRSCS24HR	1.653	1.545
100YRSCS24HR	1.932	1.800

6.9 Post-Development Drainage Area and Imperviousness

To assist in the post-development SWM facility sizing a conceptual site servicing plan has been developed by DSEL. Based on this plan the site will have 3 SWM ponds and 2 uncontrolled areas that will provide water quality and quantity control through LIDs and OGS units. **Figure E5** in **Appendix E** provides an overview of the conceptual development plan. Based on this plan approximately **16.32 ha** will drain to Grants Creek and the remaining **28.54 ha** to the Tay River. Note that efforts have been made to maintain the existing drainage areas within the development as much as possible with consideration for grading and servicing limitations.

Based on this conceptual plan there will be two SWM ponds (Ponds 1 & 3) that will discharge to the Tay River and a small segment (**1.35 ha**) that will have an OGS and LIDs. There will be one SWM Pond (Pond 2) that will discharge to Grants Creek and a small segment (**1.75 ha**) of development that will have an OGS and LIDs. To simplify this analysis while also being conservative it was assumed that the whole development would have a runoff coefficient of 0.7 (66% imperviousness) and it was assumed that 90% of the impervious area will be directly connected to the storm sewer infrastructure, which is a conservative assumption.

To ensure sufficient storage volume is provided for the lands treated by the OGS units, these drainage areas have been lumped with the areas treated by the SWM pond. This allows flexibility at the detailed design stage to allow for adjustment of drainage areas (controlled and uncontrolled) while ensuring sufficient storage volume is provided to the site.

6.10 Soil Infiltration

To represent the proposed developed land infiltration rates, Horton's infiltration has been used. For these lands, the following Horton's Infiltration parameters have been applied: $F_o=76.2$ mm/hr, $F_c=13.2$ mm/hr, $DCAY=4.14$ /hr, $F=0$ mm. These Horton infiltration rates are typical for urban grassed areas and are commonly used throughout Ontario (infiltration parameters are in line with typical rates per City of Ottawa Storm Sewer Design Guidelines)

6.11 Quality Control Volumes

Quality control active storage volumes for each of the facilities have been calculated as per MOE guidelines, based on the required 40 m³/ha. There is a total of **28.54 ha** of land that will drain to the Tay River and as such will require **1,142 m³** of quality control storage. There is a total of **16.32 ha** of land that will drain to Grants Creek and as such will require **653 m³** of quality control storage. Note that the SWM pond preliminary sizing has considered this quality control volume to drain over 48 hours, and this active quality control volume has been included in the preliminary facility sizing.

6.12 Quantity Control Volumes

As mentioned above the SWM Facilities will be designed to meet pre-development peak flows at the two respective watercourses/receivers. **Tables 6.3A** and **6.3B** below outline the pre-and post-development flows and the associated required SWM Facility storage volumes to ensure that the proposed development meets these pre-development rates. Note that the total peak flow to Grants Creek and the Tay River are either equal to or less than that specified under pre-development conditions for all events. Full SWMHYMO modelling input and summary files for post-development conditions have been provided in **Appendix E**.

From **Table 6.3A** below it is seen that the development area draining south to Grants Creek will need a total of approximately **6,343 m³** of active storage to attenuate post-development flows to pre-development conditions up to and including the 100-year event. From **Table 6.3B** below it is seen that the development area draining north to the Tay River will need a total of approximately **13,662 m³** of active storage to attenuate post-development flows to pre-development conditions up to and including the 100-year event. Note that the required unitary storage volumes (m³/ha) are higher for the area draining to the Tay River due to the increase in total drainage area when compared to pre-development conditions.

Table 6.3A: Grants Creek - Preliminary SWM Pond Sizing

Event	Pre Development 22.01 Peak Outflow (m ³ /s)	Post Development							
		SWM Pond 2 + OGS2 16.32 ha		OGS2 1.75 ha		SWM Pond 2 14.57 ha			
		Peak Outflow (m ³ /s)	Required Volume (m ³)	Peak Outflow (m ³ /s)	Required Volume (m ³)	Peak Outflow (m ³ /s)	Required Volume (m ³)		
Quality Control*	-	0.002	653	0.0002	70	0.002	583		
25MMC3H	0.125	0.125	1,723	0.013	185	0.112	1,538		
2YRCHI3HR	0.149	0.149	1,974	0.016	212	0.133	1,762		
5YRCHI3HR	0.288	0.288	2,684	0.031	288	0.257	2,396		
10YRCHI3HR	0.399	0.399	3,151	0.043	339	0.356	2,812		
25YRCHI3HR	0.559	0.559	3,773	0.060	406	0.499	3,367		
50YRCHI3HR	0.688	0.688	4,223	0.074	454	0.614	3,769		
100YRCHI3HR	0.830	0.830	4,678	0.089	503	0.741	4,175		
2YRSCS24HR	0.463	0.408	3,184	0.044	342	0.364	2,842		
5YRSCS24HR	0.790	0.672	4,167	0.072	448	0.600	3,719		
10YRSCS24HR	1.044	0.918	4,795	0.099	515	0.819	4,280		
25YRSCS24HR	1.382	1.382	5,409	0.149	581	1.233	4,828		
50YRSCS24HR	1.653	1.652	5,874	0.178	631	1.474	5,243		
100YRSCS24HR	1.932	1.930	6,343	0.207	682	1.723	5,661		

Quality control volume (40 m³/ha) released over 48 hours

Table 6.3B: Tay River - Preliminary SWM Facility Sizing

Event	Pre Development 22.86 Peak Outflow (m ³ /s)	Post Development								
		SWM Pond 1 11.26 ha		SWM 3 + OGS 17.28 ha		OGS1 1.353 ha		SWM Pond 3 15.93 ha		Tay Total 28.54
		Peak Outflow (m ³ /s)	Required Volume (m ³)	Peak Outflow (m ³ /s)	Required Volume (m ³)	Peak Outflow (m ³ /s)	Required Volume (m ³)	Peak Outflow (m ³ /s)	Required Volume (m ³)	Peak Outflow (m ³ /s)
Quality Control*	-	0.001	450	0.002	691	0.000	54	0.002	637	-
25MMC3H	0.126	0.050	1,318	0.076	2,025	0.006	159	0.070	1,866	0.126
2YRCHI3HR	0.150	0.059	1,540	0.091	2,363	0.007	185	0.084	2,178	0.150
5YRCHI3HR	0.285	0.112	2,089	0.173	3,204	0.014	251	0.159	2,953	0.285
10YRCHI3HR	0.393	0.155	2,452	0.238	3,759	0.019	294	0.219	3,465	0.393
25YRCHI3HR	0.546	0.215	2,943	0.331	4,510	0.026	353	0.305	4,157	0.546
50YRCHI3HR	0.669	0.264	3,325	0.405	5,097	0.032	399	0.373	4,698	0.669
100YRCHI3HR	0.804	0.317	3,695	0.487	5,664	0.038	443	0.449	5,221	0.804
2YRSCS24HR	0.444	0.175	2,502	0.269	3,831	0.021	300	0.248	3,531	0.444
5YRSCS24HR	0.750	0.296	3,342	0.454	5,116	0.036	400	0.419	4,716	0.749
10YRSCS24HR	0.986	0.389	3,871	0.597	5,931	0.047	464	0.550	5,467	0.986
25YRSCS24HR	1.298	0.512	4,481	0.786	6,869	0.062	538	0.724	6,331	1.298
50YRSCS24HR	1.545	0.609	4,940	0.936	7,560	0.073	592	0.862	6,968	1.545
100YRSCS24HR	1.800	0.710	5,397	1.090	8,265	0.085	647	1.005	7,618	1.800

Quality control volume (40 m³/ha) released over 48 hours

6.13 Summary

A preliminary SWM Facility sizing has been completed for the proposed development site. The SWM Facility release rates have been determined based on the pre-development conditions modelling outlined above. Based on this analysis it was found that the development area draining north to the Tay River will need a total of approximately **13,662 m³** of active storage to attenuate post-development flows to pre-development conditions up to and including the 100-year event. The development area draining south to Grants Creek will need a total of approximately **6,343 m³** of active storage to attenuate post-development flows to pre-development conditions up to and including the 100-year event. Note that the primary intention of this analysis is to guarantee that sufficient land is set aside under post-development conditions to ensure that there is adequate room for SWM facilities to meet the objectives specified above.

7 CONCLUSION

This report has provided an overview of the various existing hydraulic and hydrologic conditions of the site. A drainage area analysis has been completed for the Tay River and Grants Creek. Based on post-development plans there will be a drainage area boundary revision of approximately **5.69 ha** from existing conditions. This results in an increase of **+0.009%** to the Tay River watershed and a decrease of **-0.06%** to the total Grants Creek watershed. Given the size of these watersheds, and the location of the drainage area change (at the confluence of the two watersheds) it is unlikely that this change under post-development conditions will have a quantifiable impact on the hydraulic and hydrologic of the surrounding watercourses.

Rainfall and surface water monitoring was completed on the site from June 2022 to November 2022. The rainfall monitoring recorded **18** significant events (with volumes greater than 5mm) and all rainfall events recorded had return periods less than the 5-year event. Water level monitoring at the Glen Tay Road crossing indicated that tailwater impacts at this location may affect the flows through the crossing and to the wetland, as such additional loggers are advised for future monitoring to capture these impacts. The level logger in the Glen Tay wetland showed that the wetland water levels fluctuated by only **24 cm** over the full monitoring period. Combining the rainfall data with the flows recorded at the water survey Canada gauge, it was found that the Tay River at this location (which includes both the Tay River and Grants Creek) has a runoff coefficient of approximately **0.25**.

The RVCA floodplain mapping boundaries surrounding the subject area have been updated based on the latest available data to ensure accurate delineation supporting the balance cut fill analysis completed by DSEL. No modifications have been made to the existing hydraulic model produced by RVCA in 2013, simply the topography that the flood elevations have been mapped on has been updated.

Continuous hydrologic modelling has been completed which has made use of the water budget modelling completed by GEMTEC. IA and CN values were iteratively adjusted to align with GEMTEC's pre-development annual water budget. Based on this analysis it was determined that under pre-development conditions for the total development site, approximately **22-24%** of the annual rainfall will result in runoff, **62%** will evaporate and **15-16%** will infiltrate.

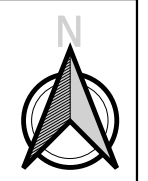
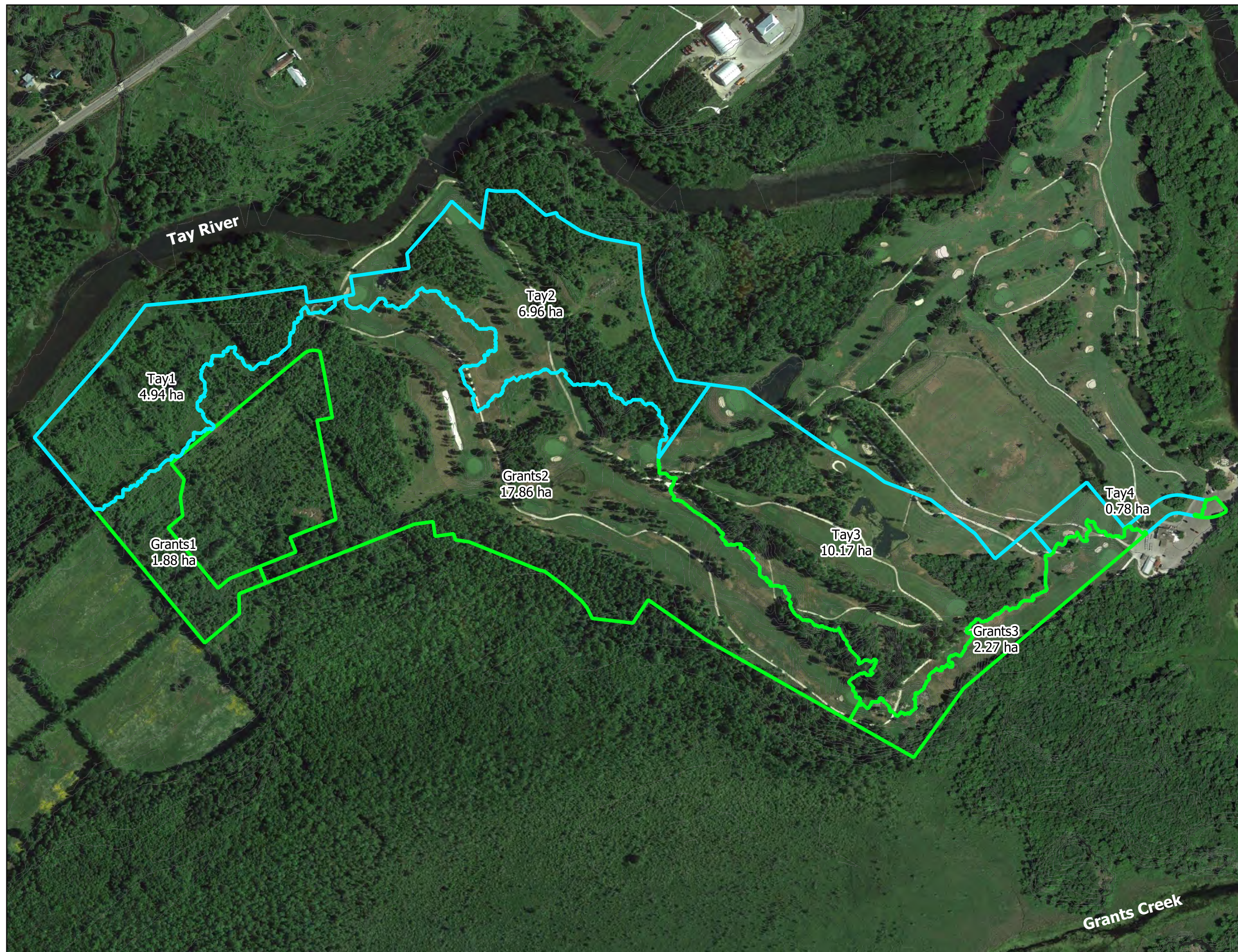
A preliminary SWM Facility sizing has been completed for the proposed development site. The SWM Facility release rates have been determined based on the pre-development conditions. Based on this analysis it was found that the development area draining north to the Tay River will need a total of approximately **13,662 m³** of active storage to attenuate post-development flows to pre-development conditions up to and including the 100-year event. The development area draining south to Grants Creek will need a total of approximately **6,343 m³** of active storage to attenuate post-development flows to pre-development conditions up to and including the 100-year event. Note that this analysis is simply a conceptual analysis, with the primary intention to ensure that sufficient land is set aside under post-development conditions to ensure that there is adequate room for SWM facilities to meet the objectives specified above.

8 JFSA STATEMENT OF LIMITATIONS

J.F. Sabourin and Associates Inc. (JFSA) has prepared this report and performed the services described in this report, in a manner consistent with the level of care and skill normally exercised by members of the engineering and science professions currently practicing under similar conditions in the jurisdiction in which the services are provided, subject to the time limits and financial and physical constraints applicable to the services. No other warranty, expressed or implied, is made. This report has been prepared for the exclusive use of the client representative, for the specific site, objective, and purpose described to JFSA by the client. The factual data, interpretations and recommendations pertain to a specific project as described in this report and do not apply to any other project or site location. Any change in site conditions, purpose and/or development plans may alter the validity of the report. The report, which specifically includes all tables, figures and appendices, is based on data and information assembled by JFSA and is based on the conditions at the site and study area at the time of the work and on the information provided by others. JFSA has relied in good faith on all information provided and does not accept responsibility for any deficiencies, misstatements, or inaccuracies contained in the report as a result of omissions, misinterpretation, or fraudulent acts of the persons contacted or errors or omissions in the reviewed documentation and data. Any use that a third party makes of this report, or any reliance on, or decisions to be made based on it, are the responsibilities of such third parties. JFSA accepts no responsibility for damages, if any, suffered by any third party as a result of decisions made or actions based on this report.

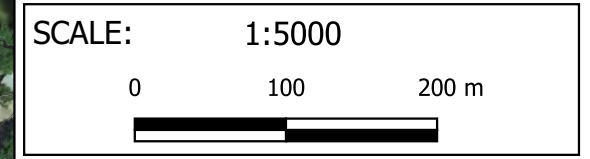
Appendix A

Existing Drainage



Legend

- Drainage Area
[Name]
[Area]
- Drains to Tay River
 - Drains to Grants Creek
- Contours (m)
— 0.5



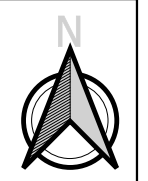
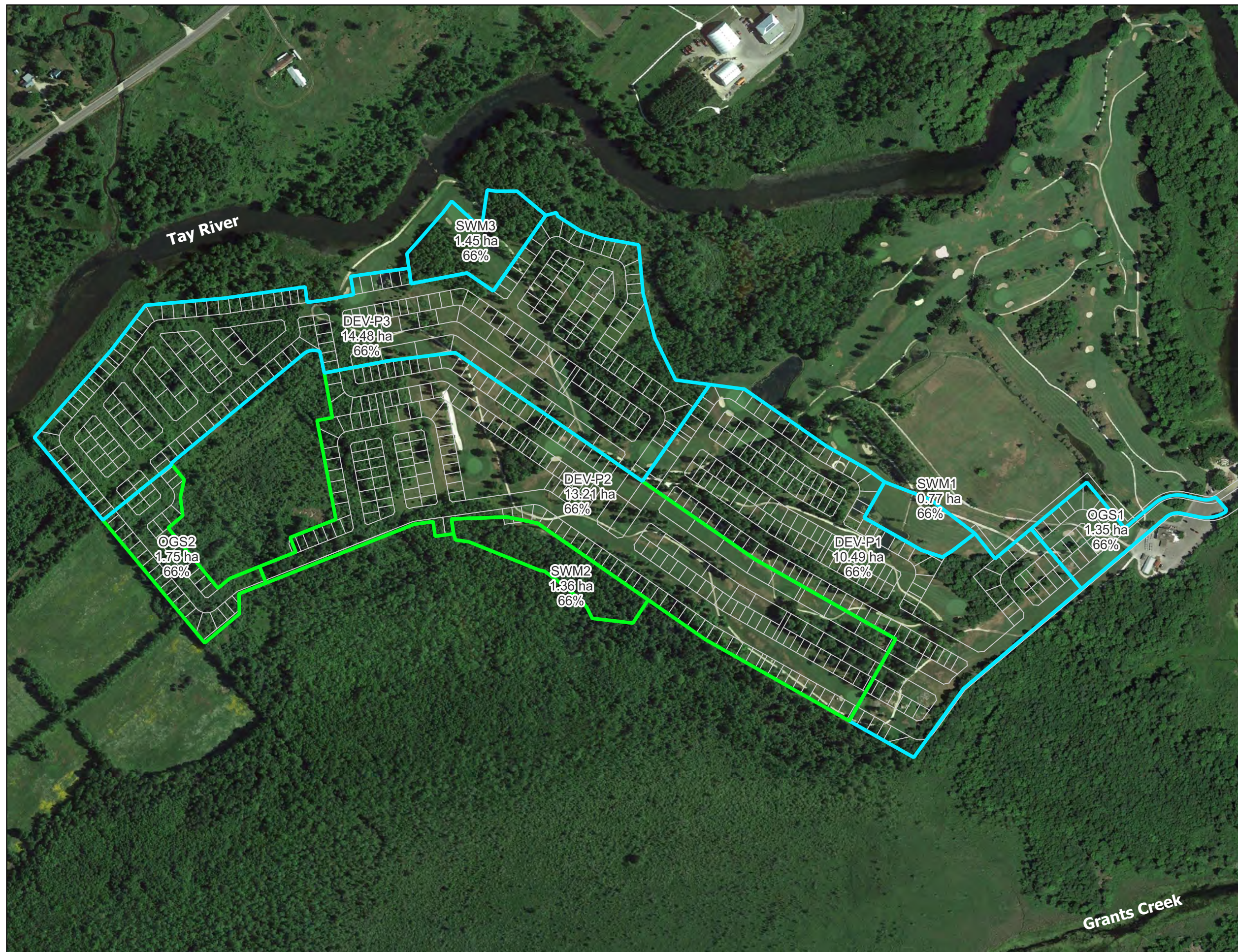
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(613) 836-3884
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Perth Golf Course

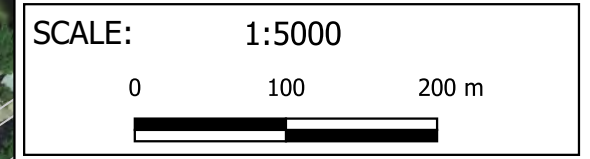
Figure A1: Existing Drainage Conditions

PROJECT	2118-21
DRAWN	BT
DATE	February 2023



Legend

- Drainage Area
 [Name]
 [Area]
 [% Imp]
- Drains to Tay River
 - Drains to Grants Creek
 - Proposed Development Plan



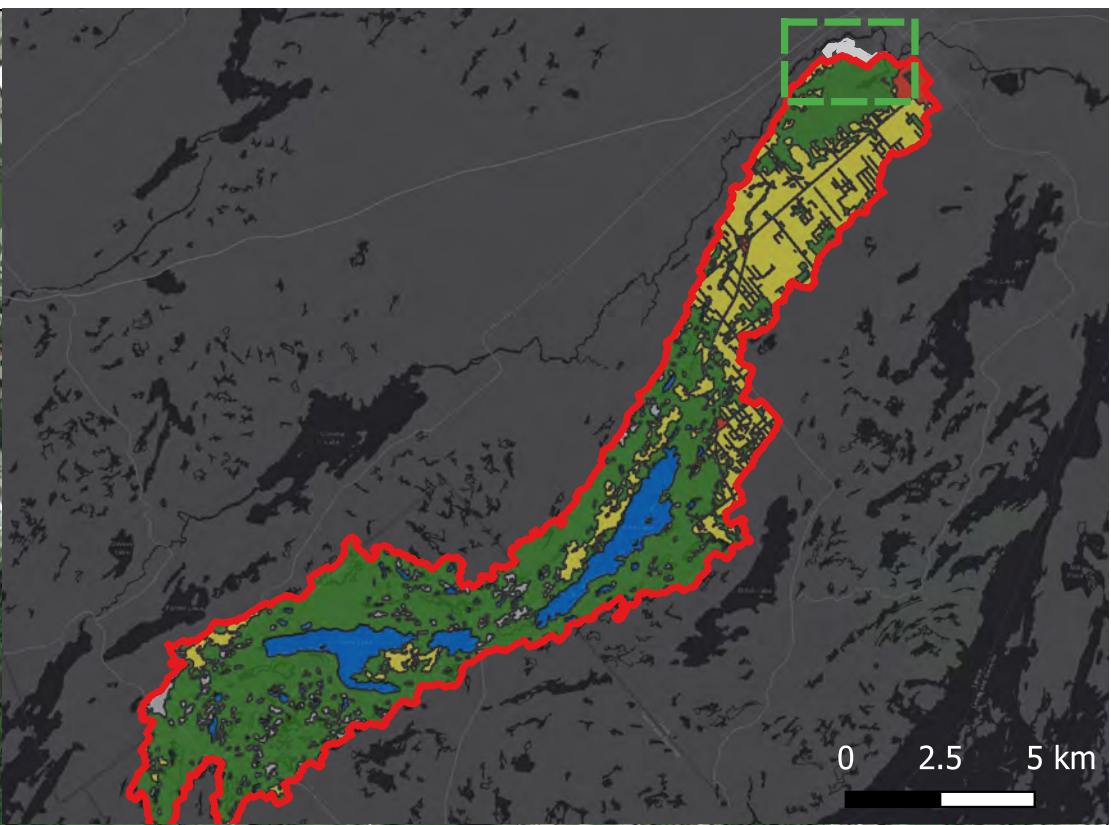
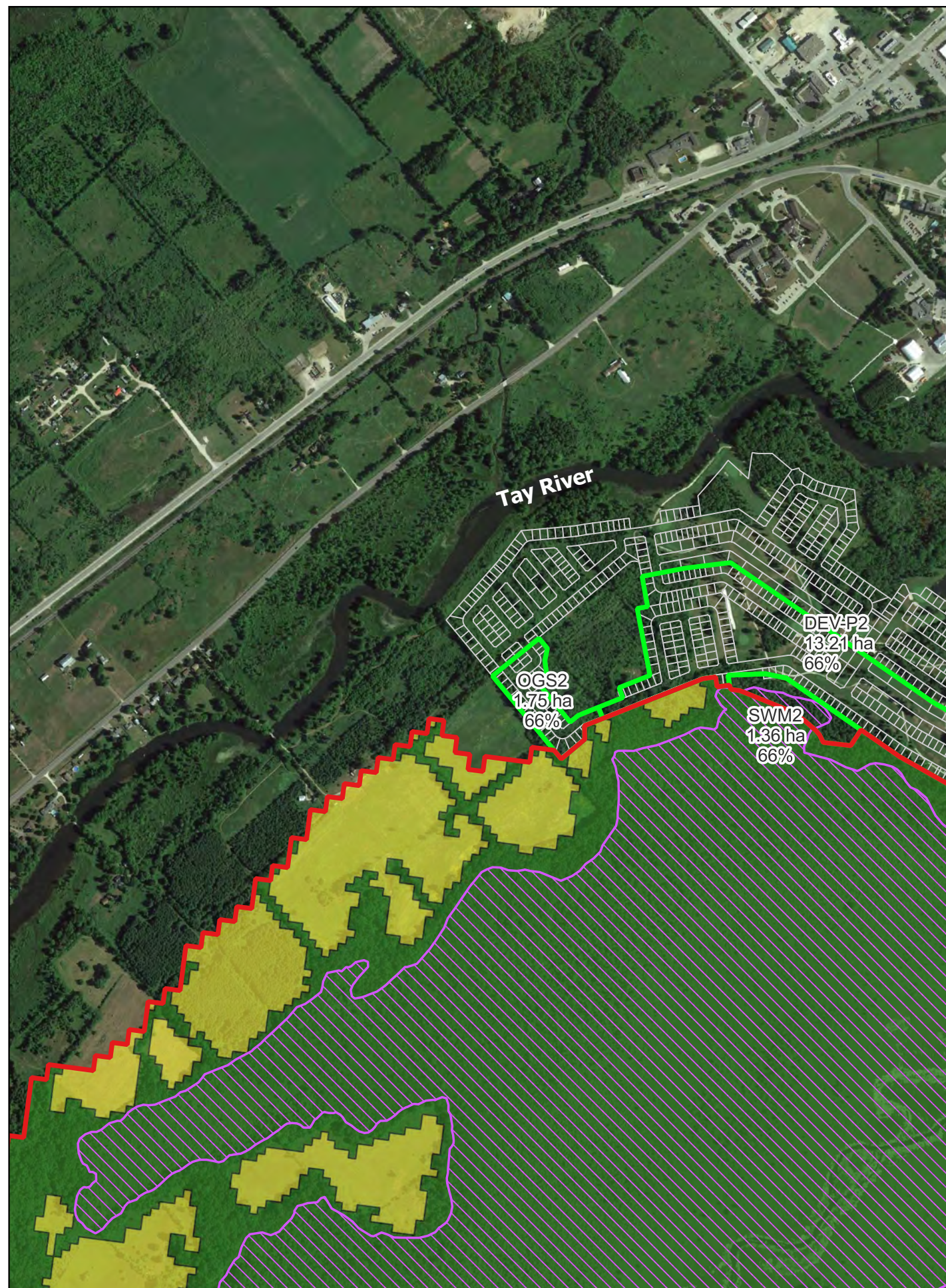
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Figure A2: Post-Development Drainage Area

PROJECT	2118-21
DRAWN	BT
DATE	February 2023



N

Legend

- Grants Creek Watershed (9,351.78 ha)
- RVCA Significant Wetland
- Study Area
- Post-Development Drainage Area
- Grants Creek
- Proposed Development Plan
- Land Cover
- Agriculture
- Bedrock
- Community/Infrastructure
- Natural
- Water

SCALE: 1:10000

0 200 400 m

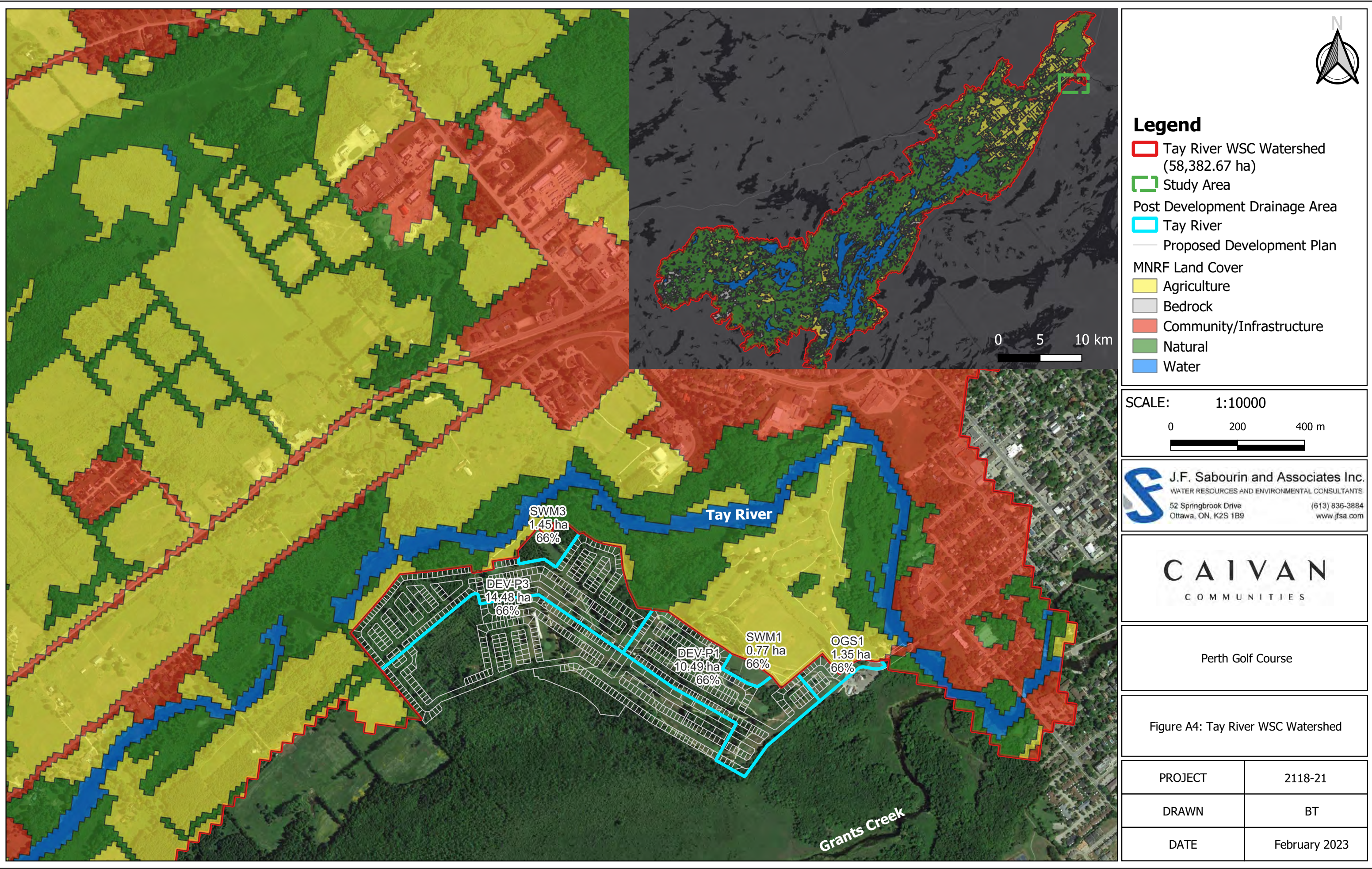
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Figure A3: Grants Creek Watershed

PROJECT	2118-21
DRAWN	BT
DATE	February 2023



Legend

- Tay River WSC Watershed (58,382.67 ha)
- Study Area
- Post Development Drainage Area
- Tay River
- Proposed Development Plan
- MNRF Land Cover
- Agriculture
- Bedrock
- Community/Infrastructure
- Natural
- Water

SCALE: 1:10000

0 200 400 m

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Figure A4: Tay River WSC Watershed

PROJECT	2118-21
DRAWN	BT
DATE	February 2023

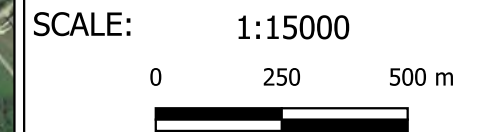
Appendix B

Surface Water Monitoring



Legend

- Rain Gauge Site
- WSC Site
- Grant's Creek Logger Site
- Glen Tay Road Logger Site
- Watercourses



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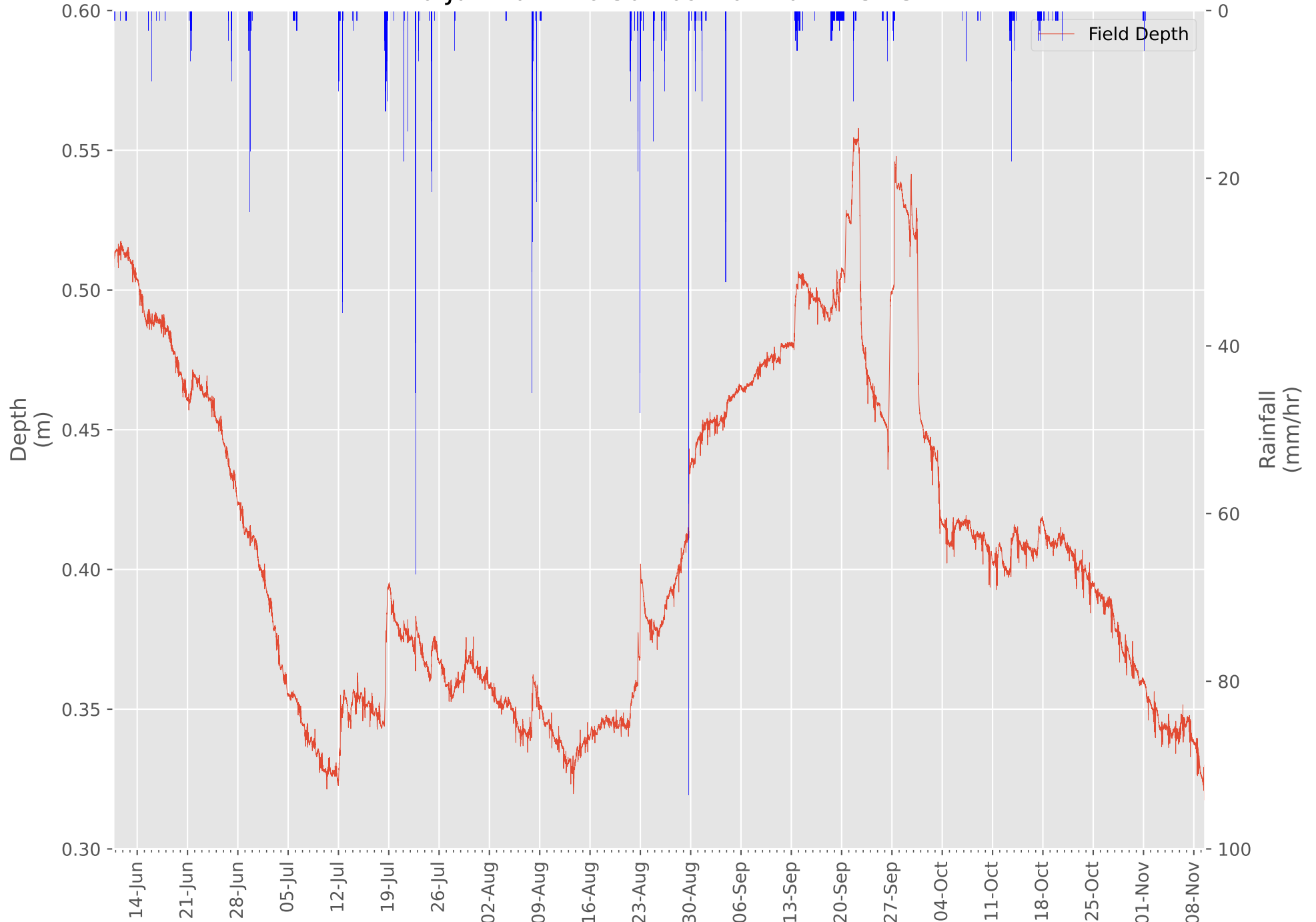
Perth Golf Course

Figure B1:
 2022 Monitoring Locations

PROJECT	2118(01)-21
DRAWN	MP
DATE	FEB 2023

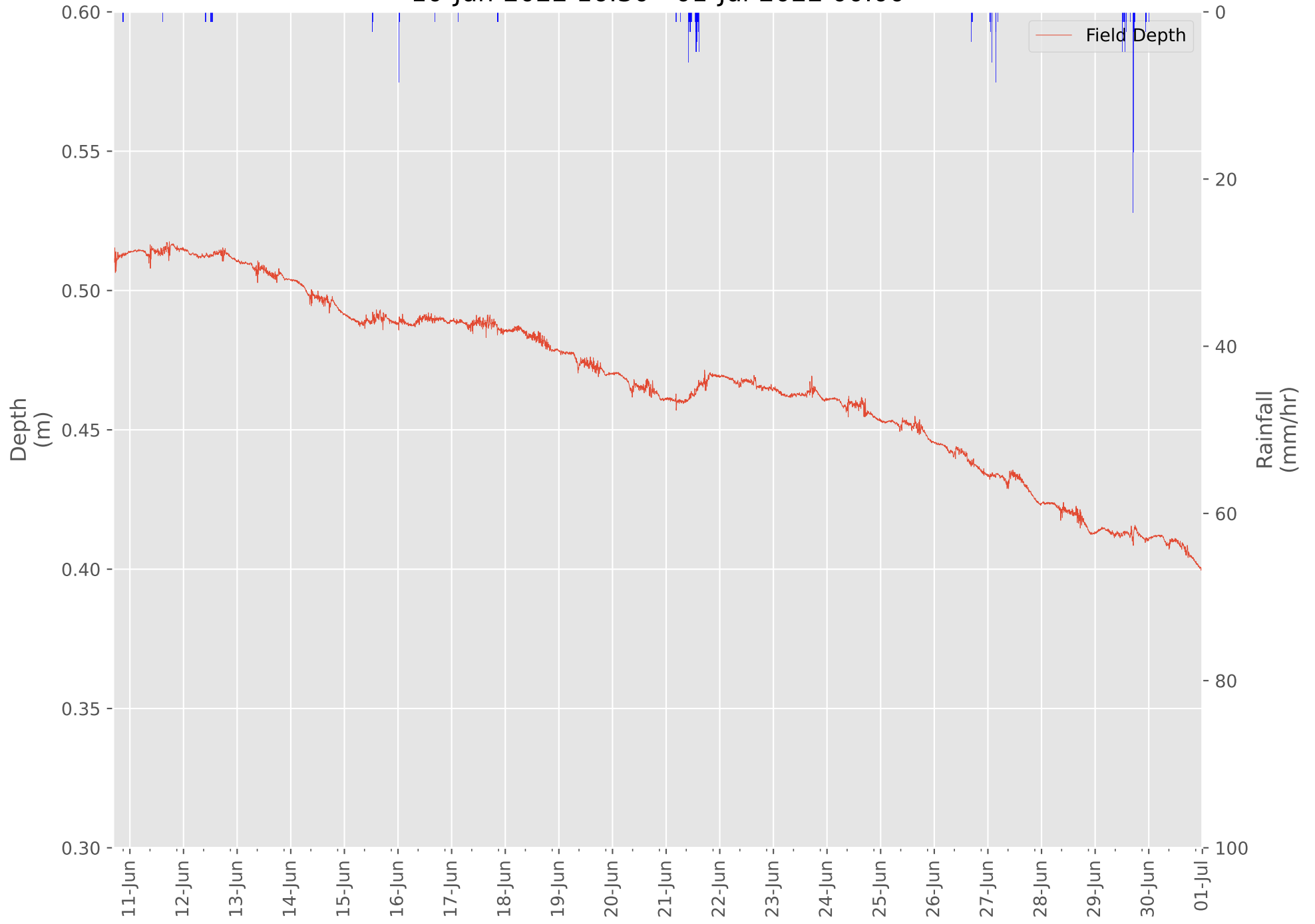
Glen Tay Crossing

10-Jun-2022 16:30 - 09-Nov-2022 13:45



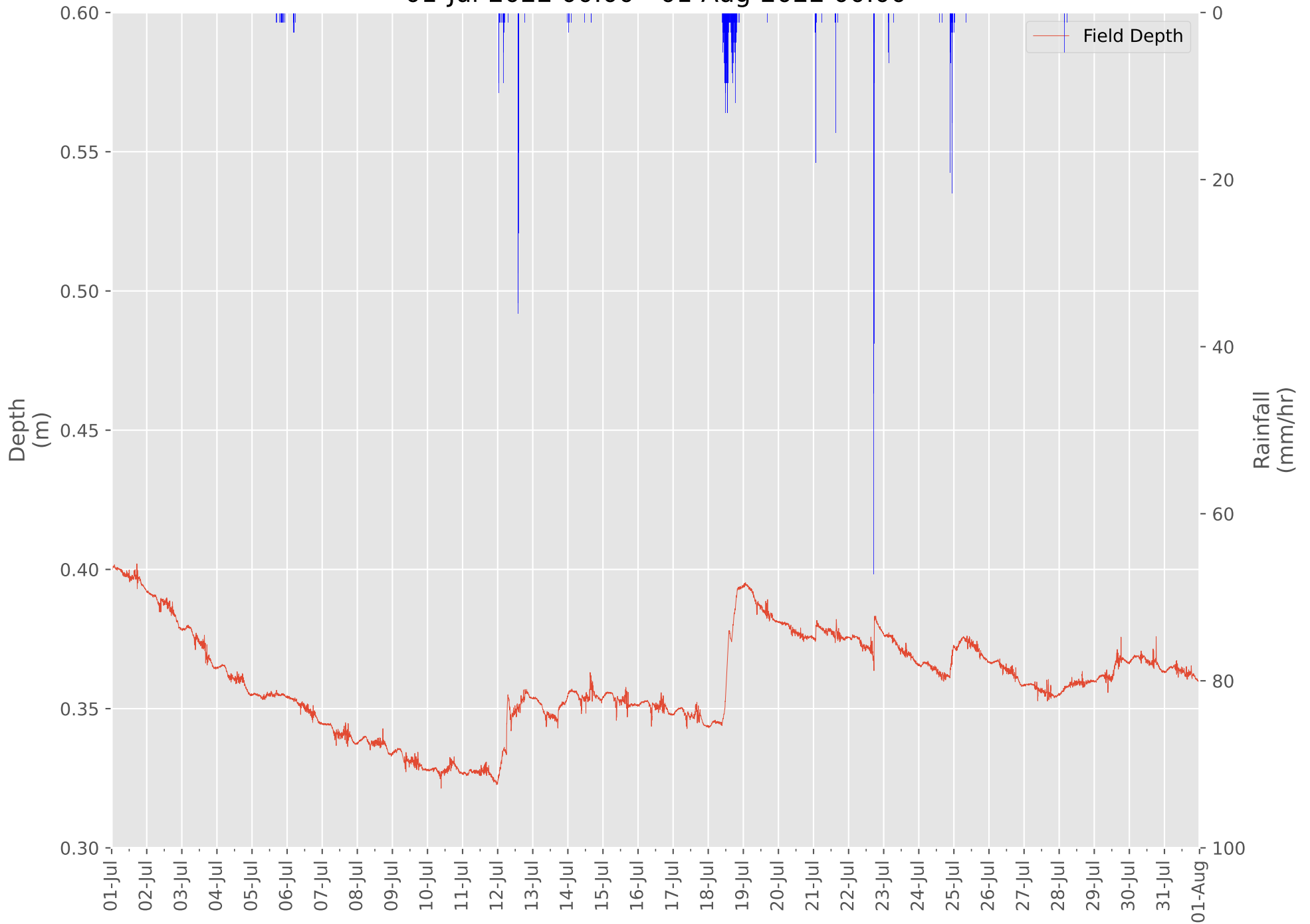
Glen Tay Crossing

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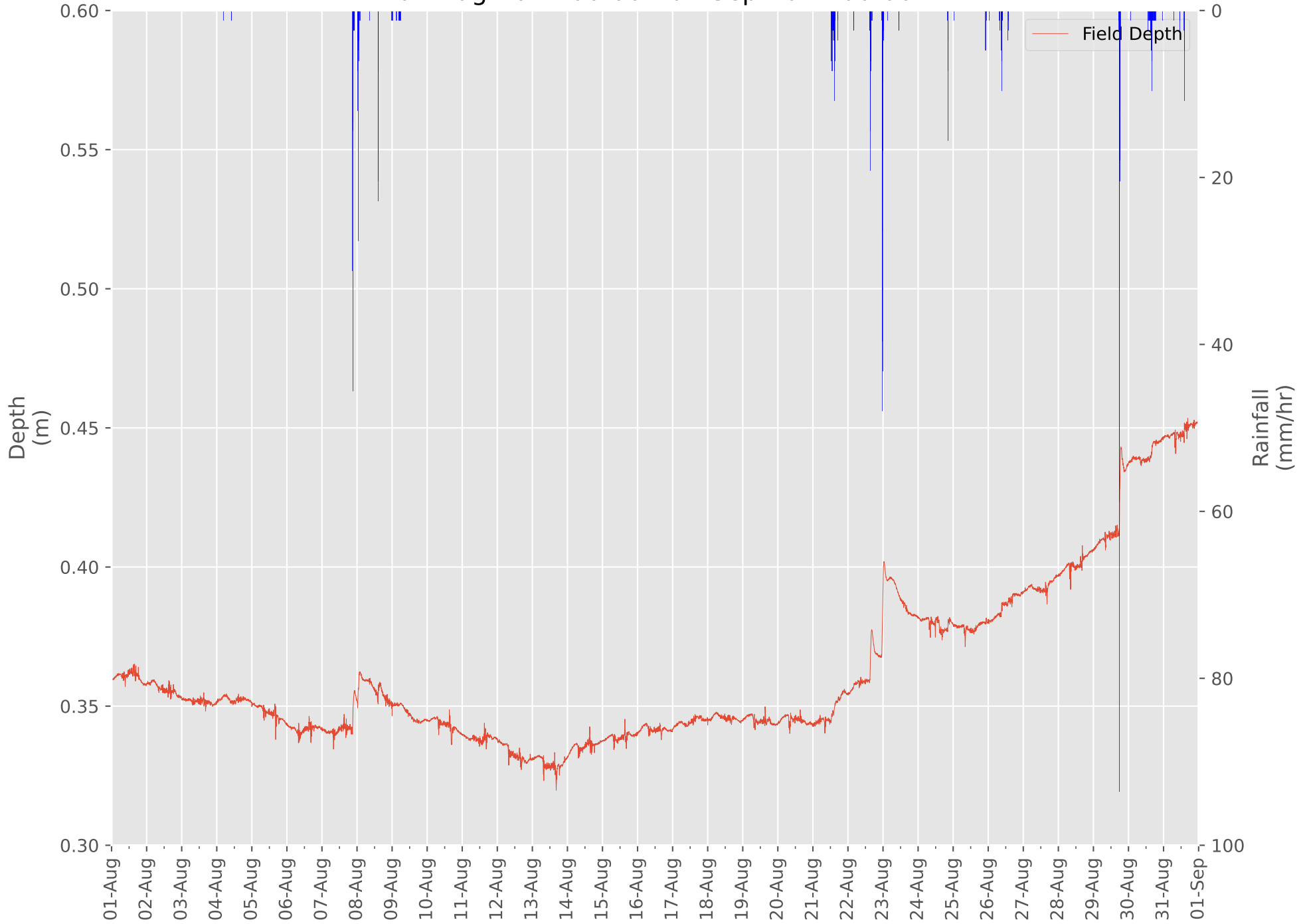
Glen Tay Crossing

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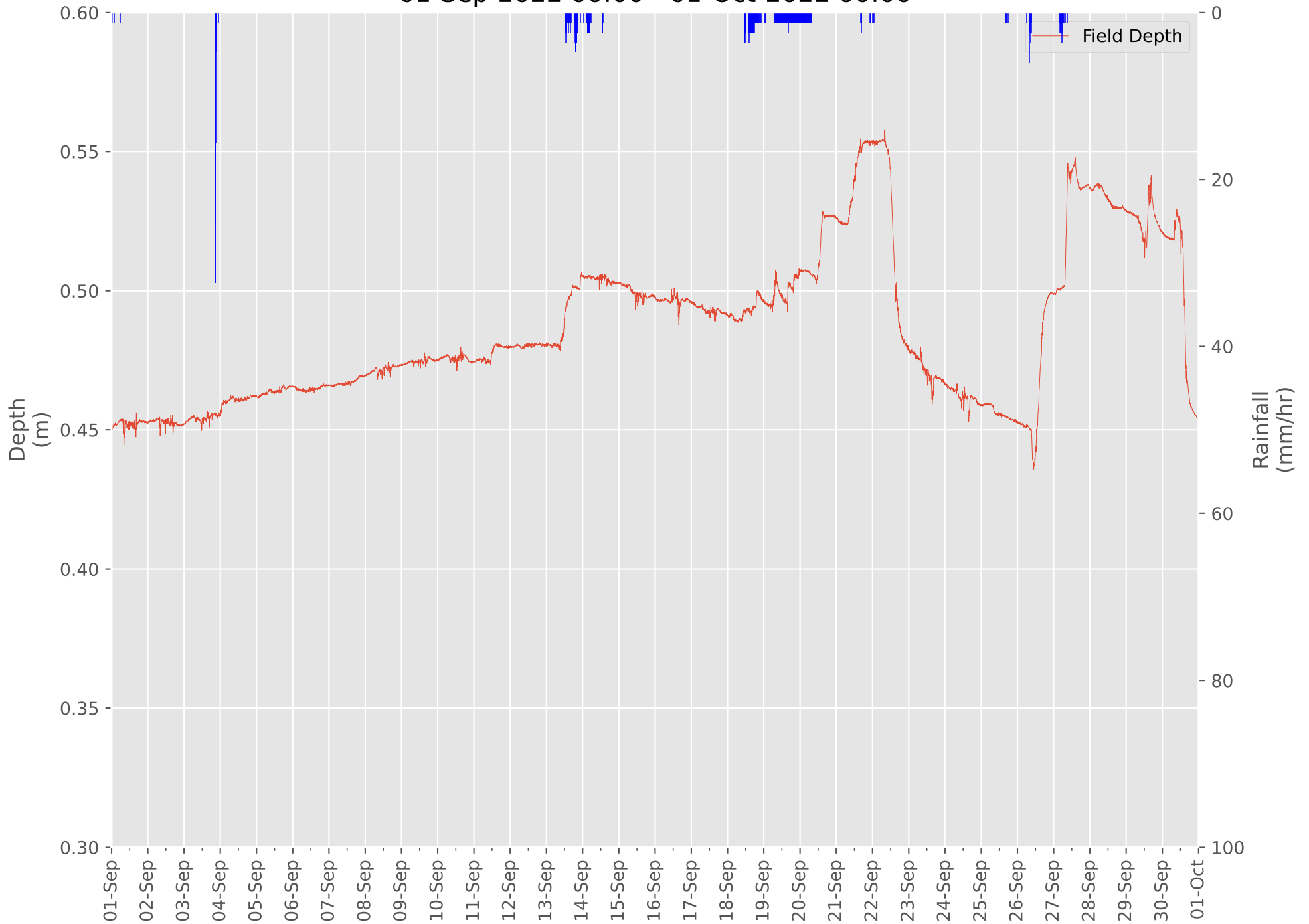
Glen Tay Crossing

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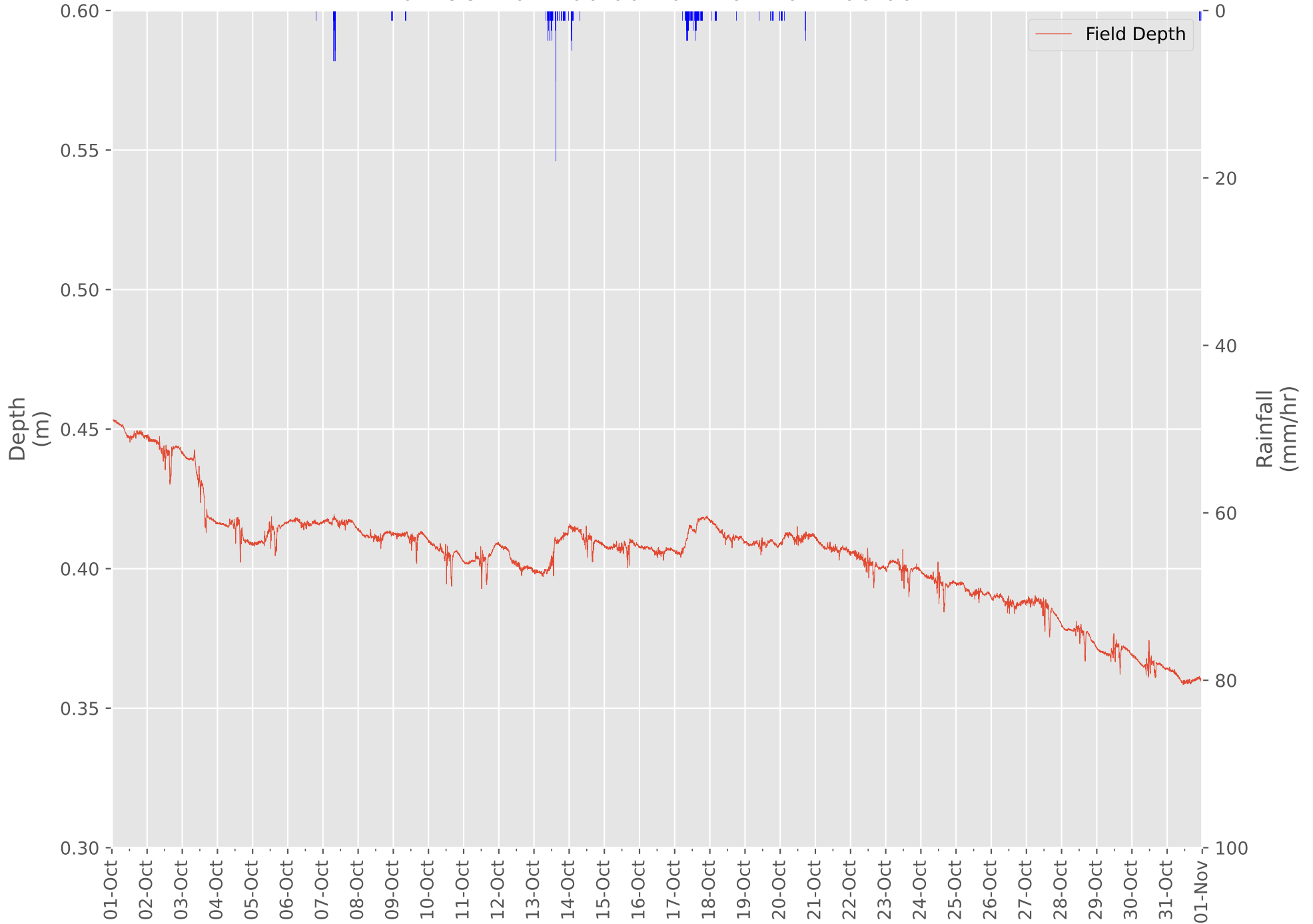
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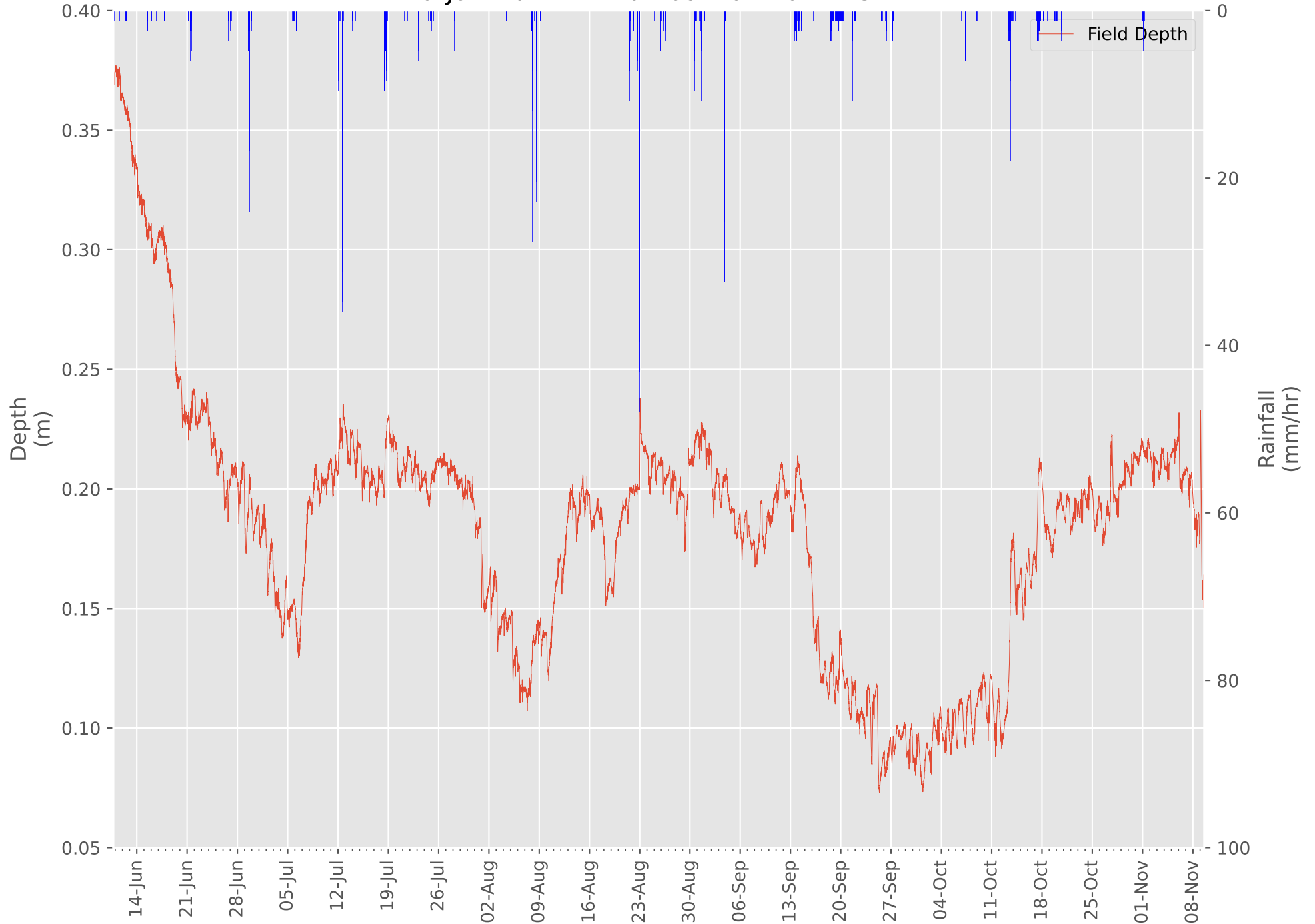
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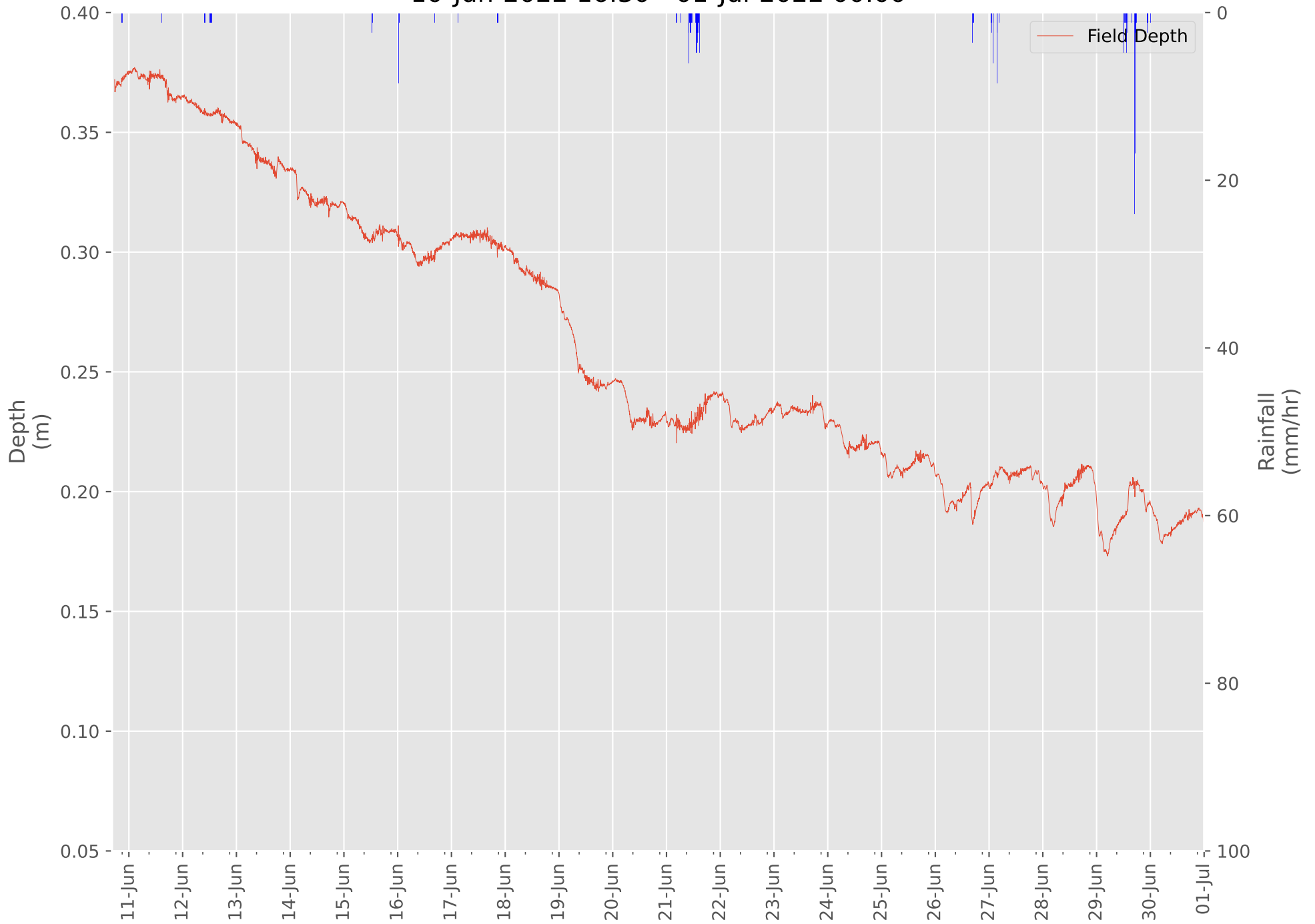
Grants Creek Wetland

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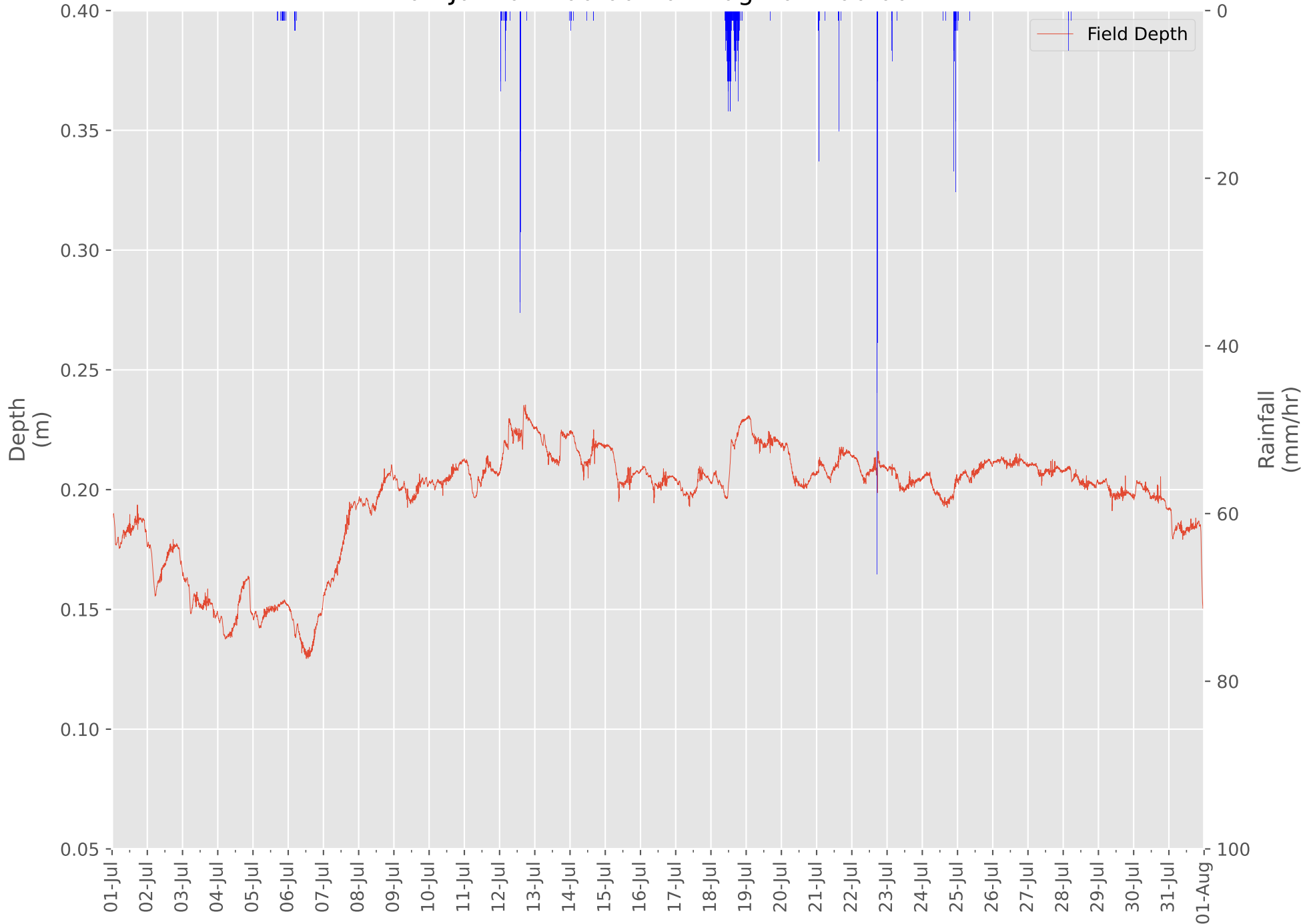
Grants Creek Wetland

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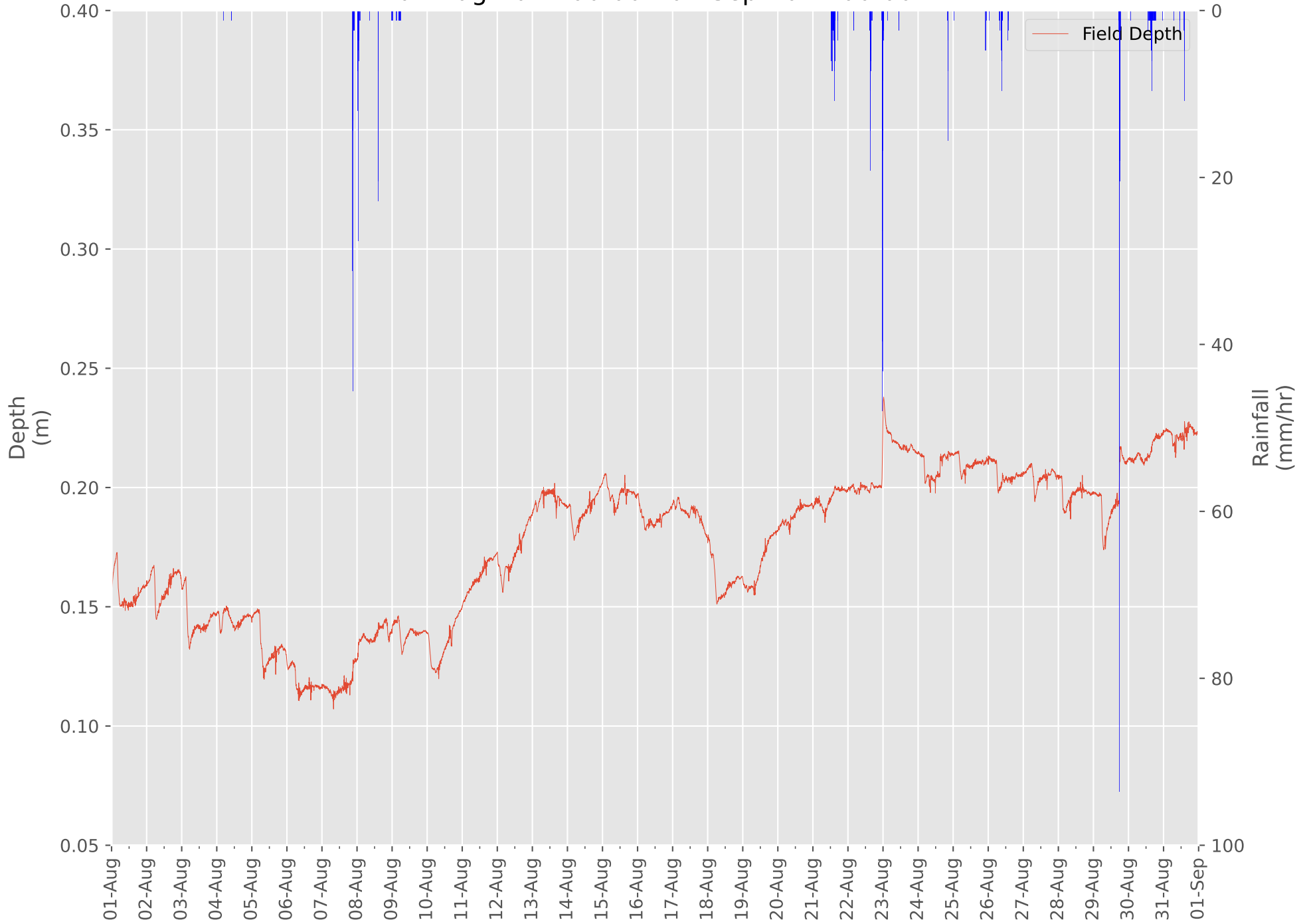
Grants Creek Wetland

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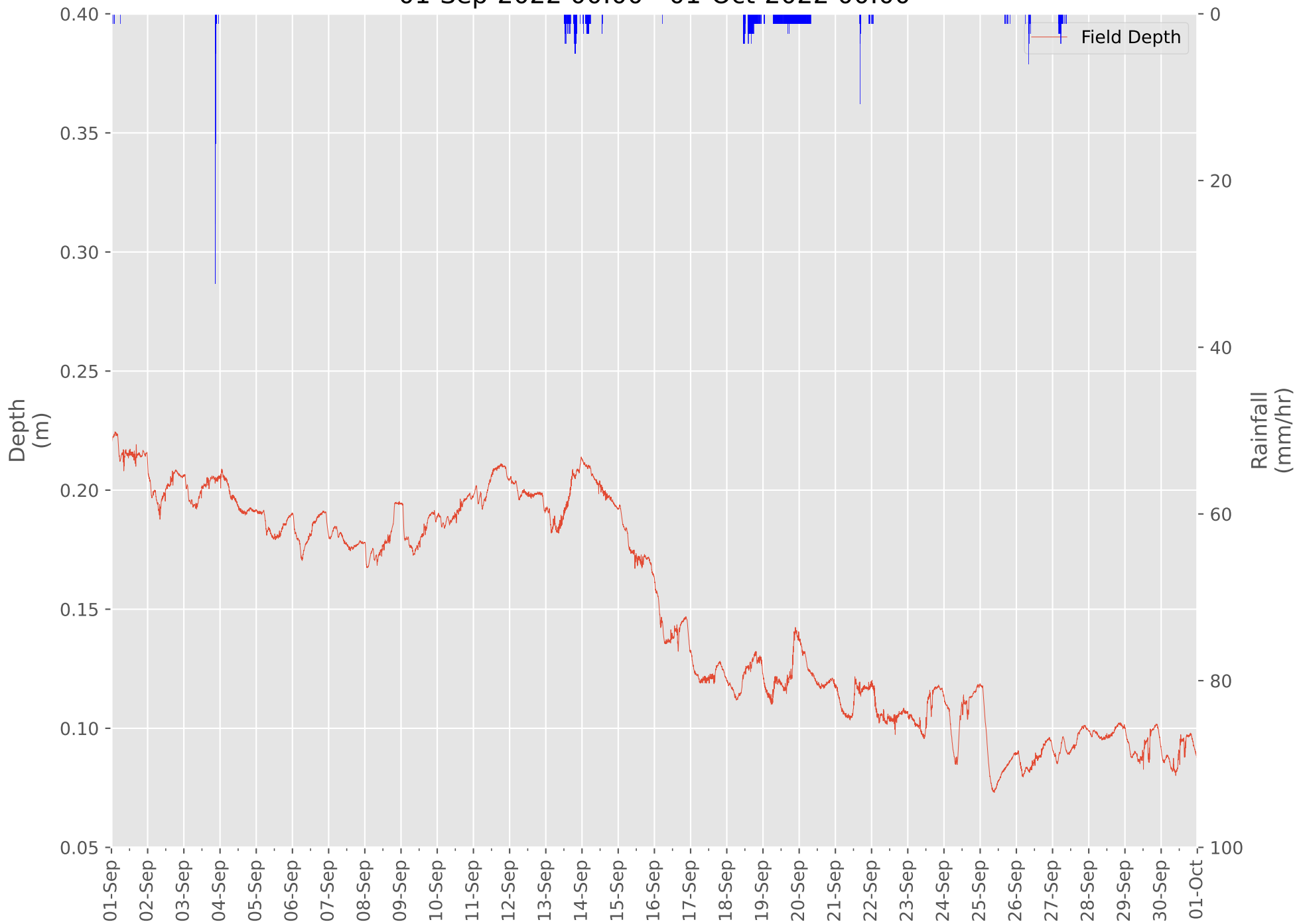
Grants Creek Wetland

01-Aug-2022 00:00 - 01-Sep-2022 00:00



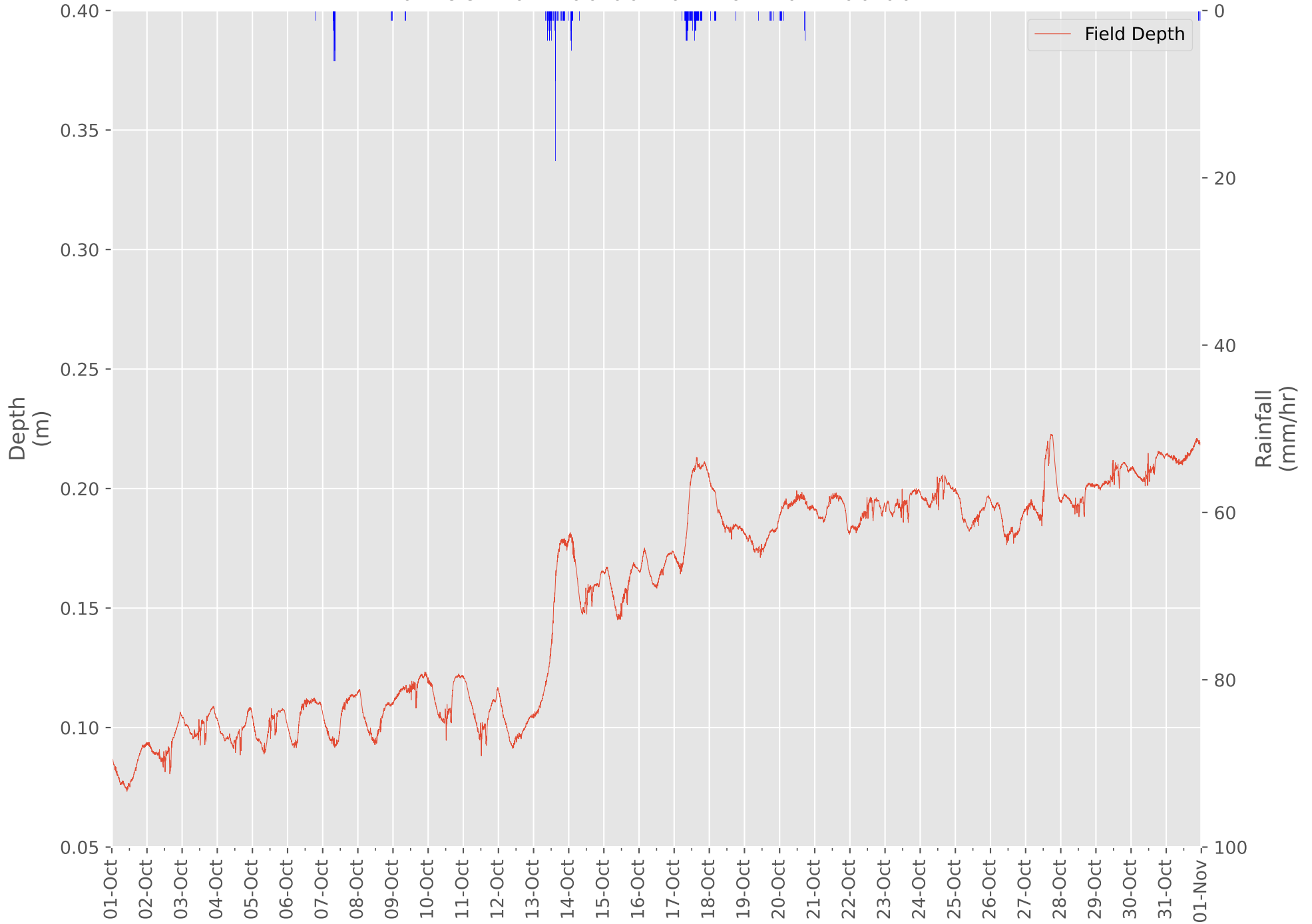
Grants Creek Wetland

01-Sep-2022 00:00 - 01-Oct-2022 00:00



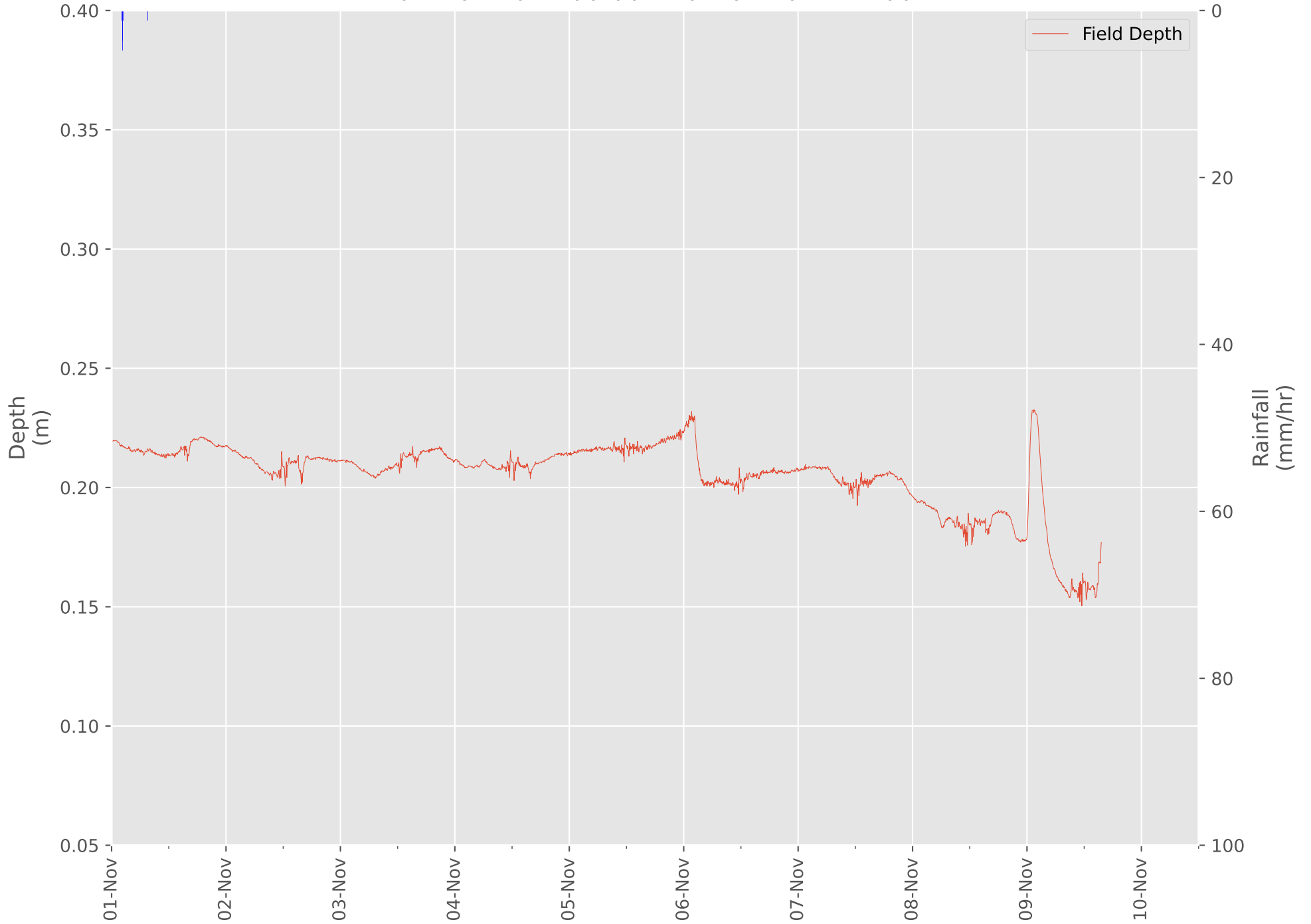
Grants Creek Wetland

01-Oct-2022 00:00 - 01-Nov-2022 00:00



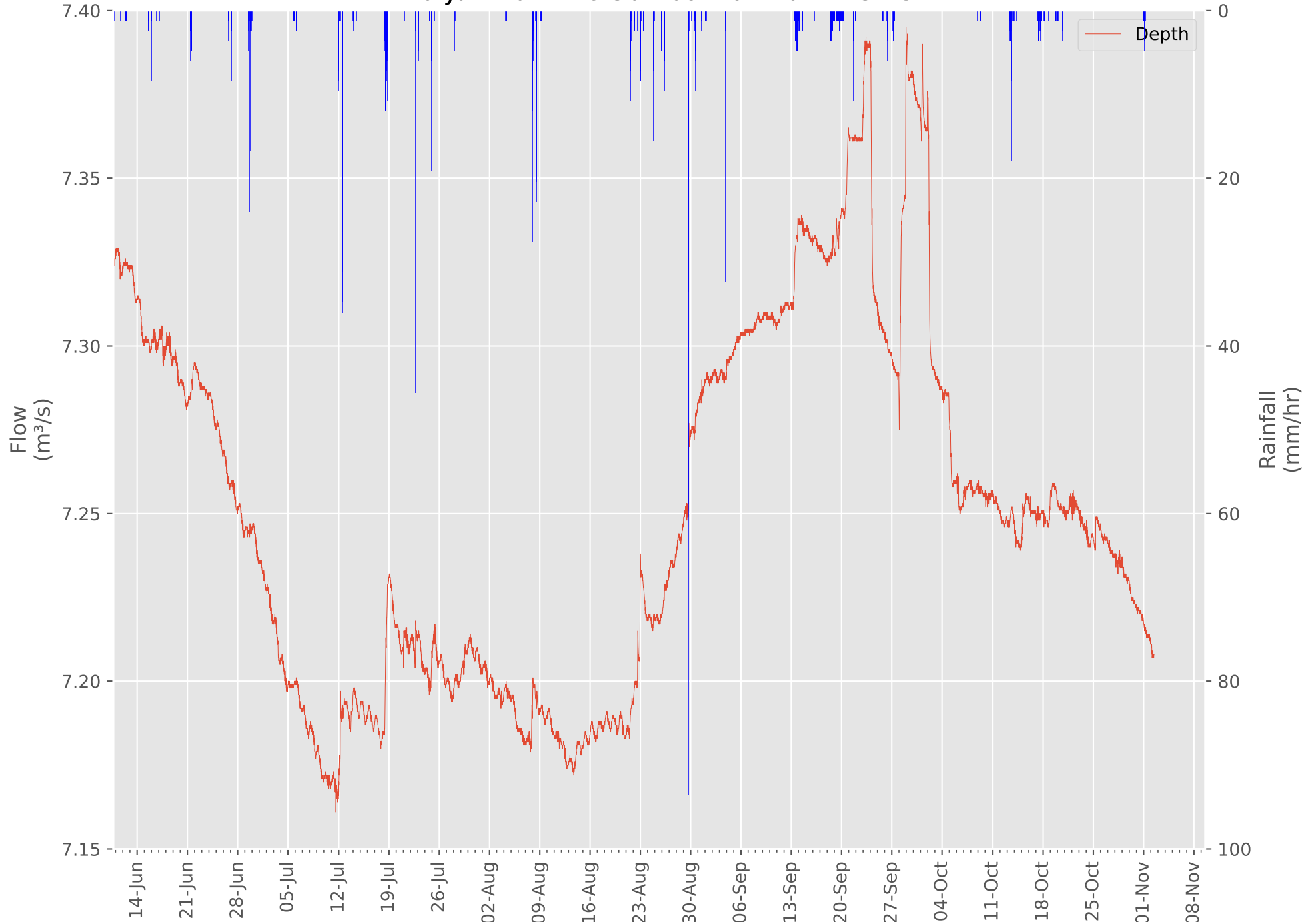
Grants Creek Wetland

01-Nov-2022 00:00 - 10-Nov-2022 12:00



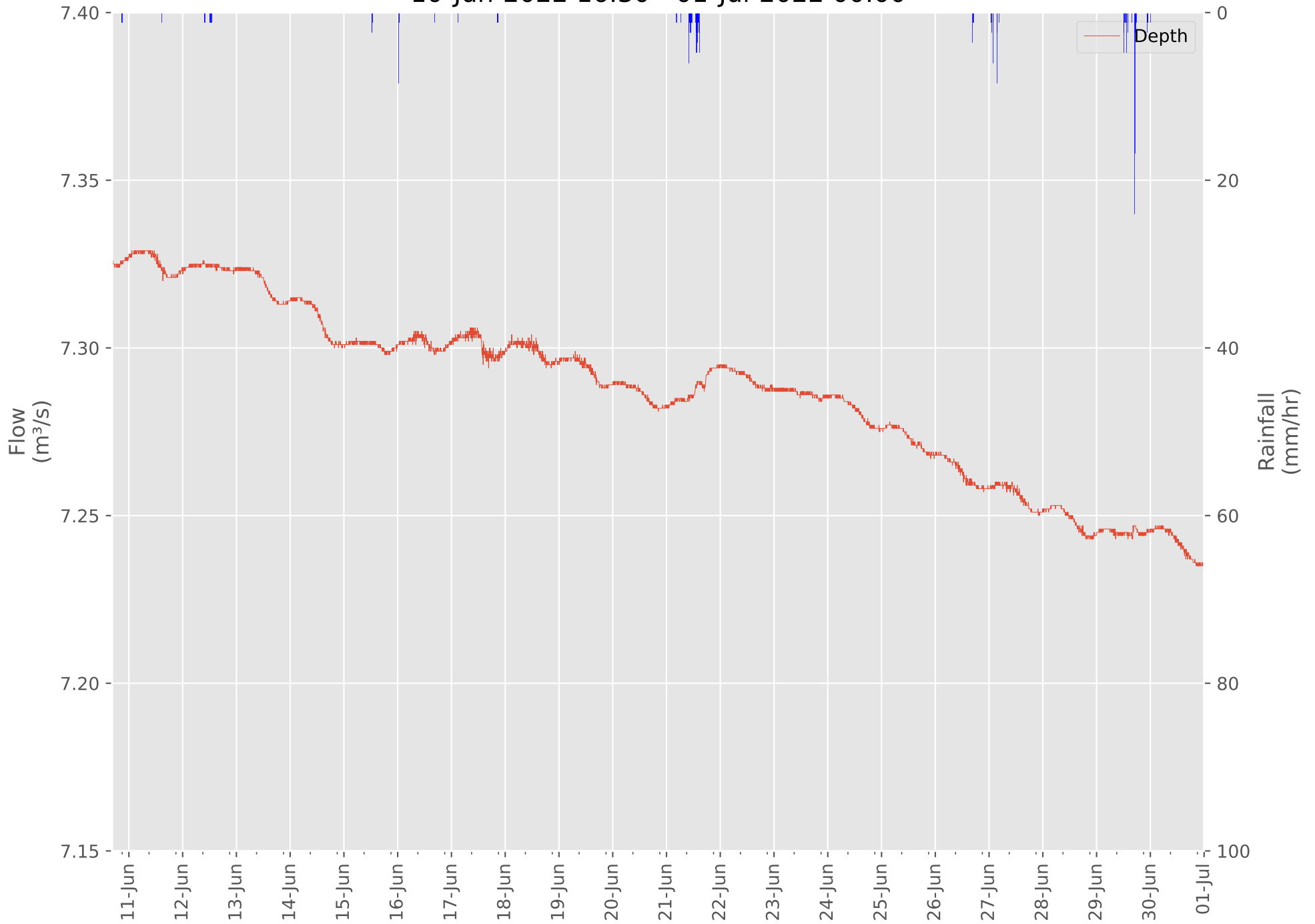
Tay River WSC Gauge Level

10-Jun-2022 16:30 - 09-Nov-2022 13:45

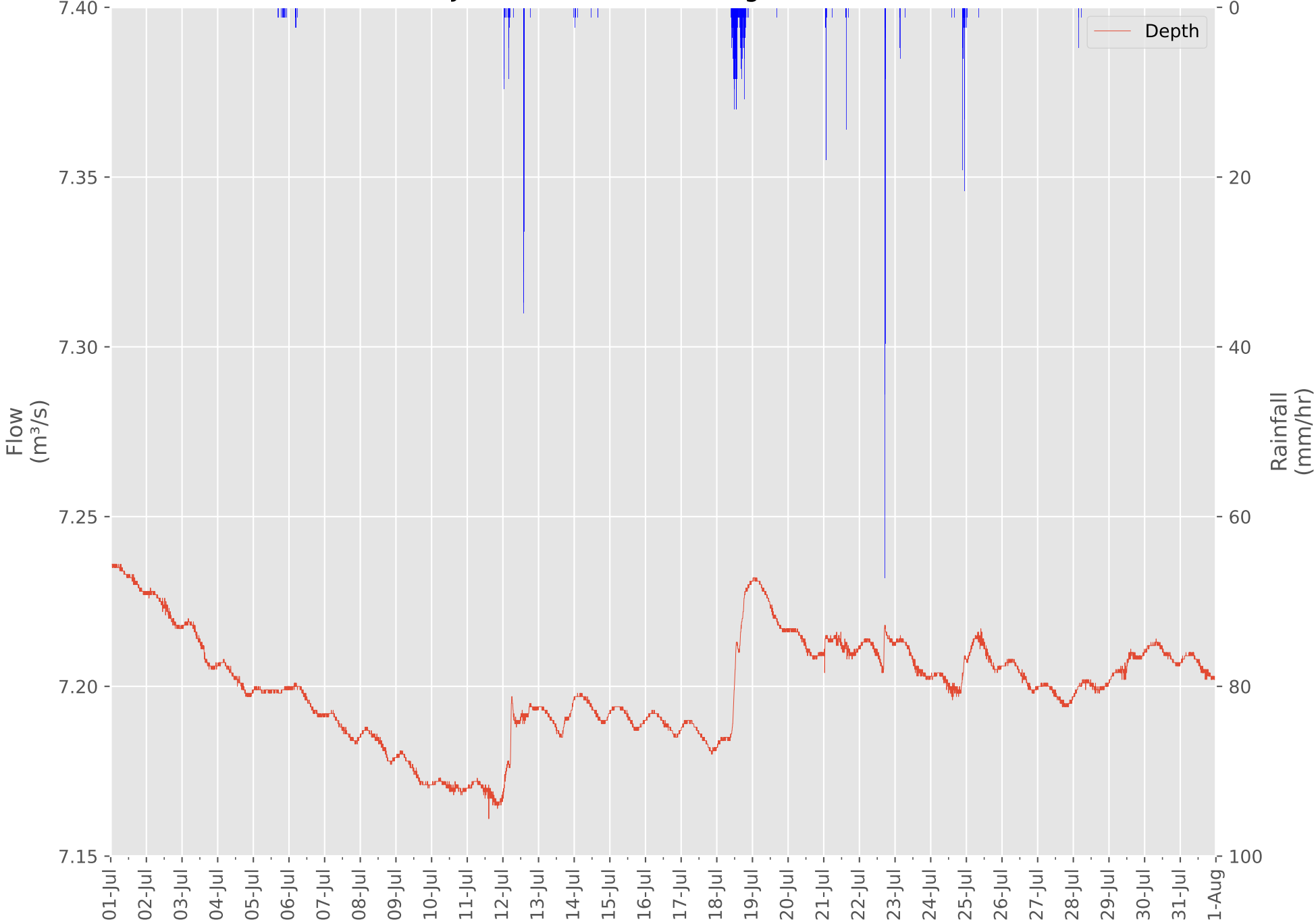


Tay River WSC Gauge Level

10-Jun-2022 16:30 - 01-Jul-2022 00:00

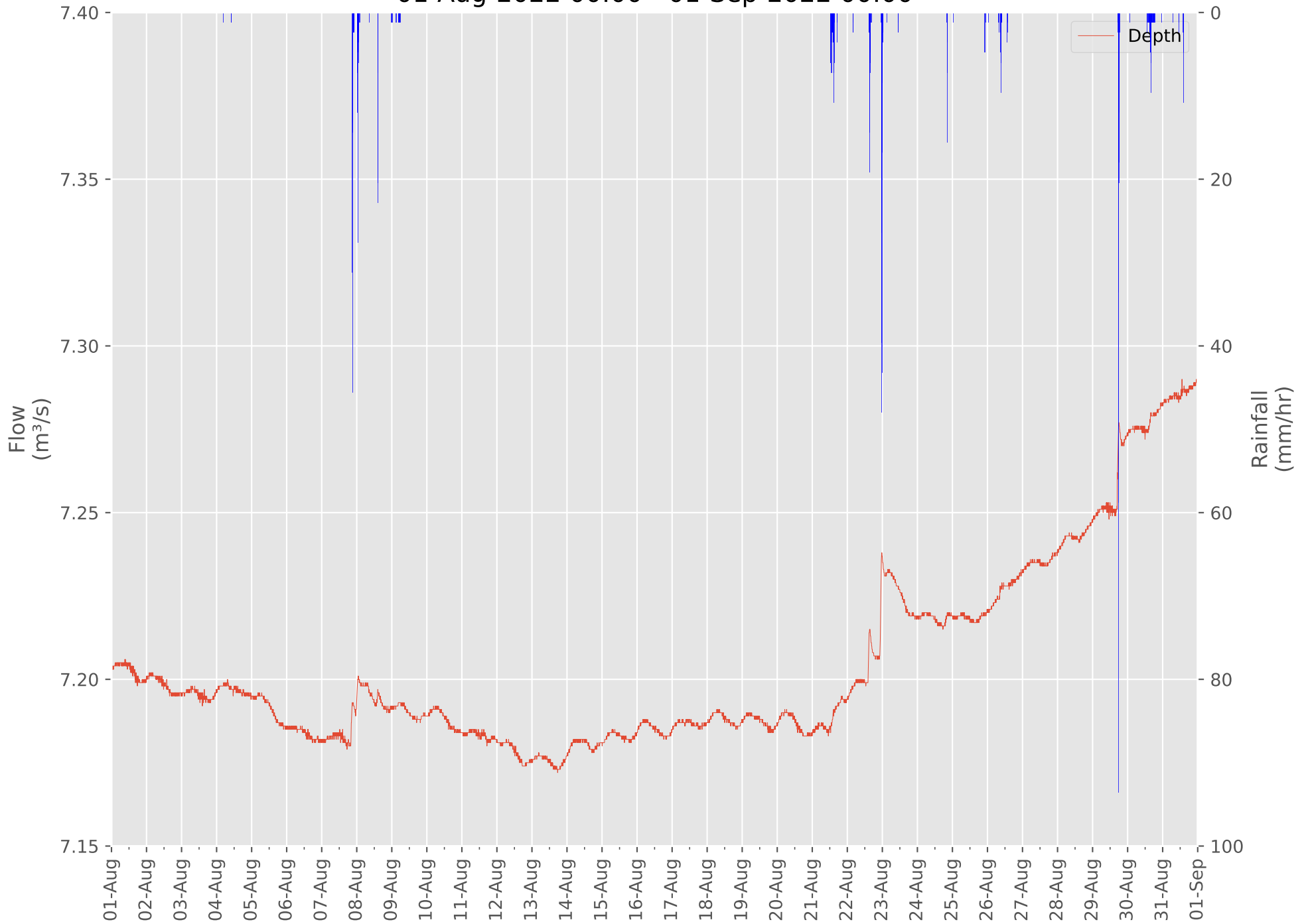


Tay River WSC Gauge Level 01-Jul-2022 00:00 - 01-Aug-2022 00:00



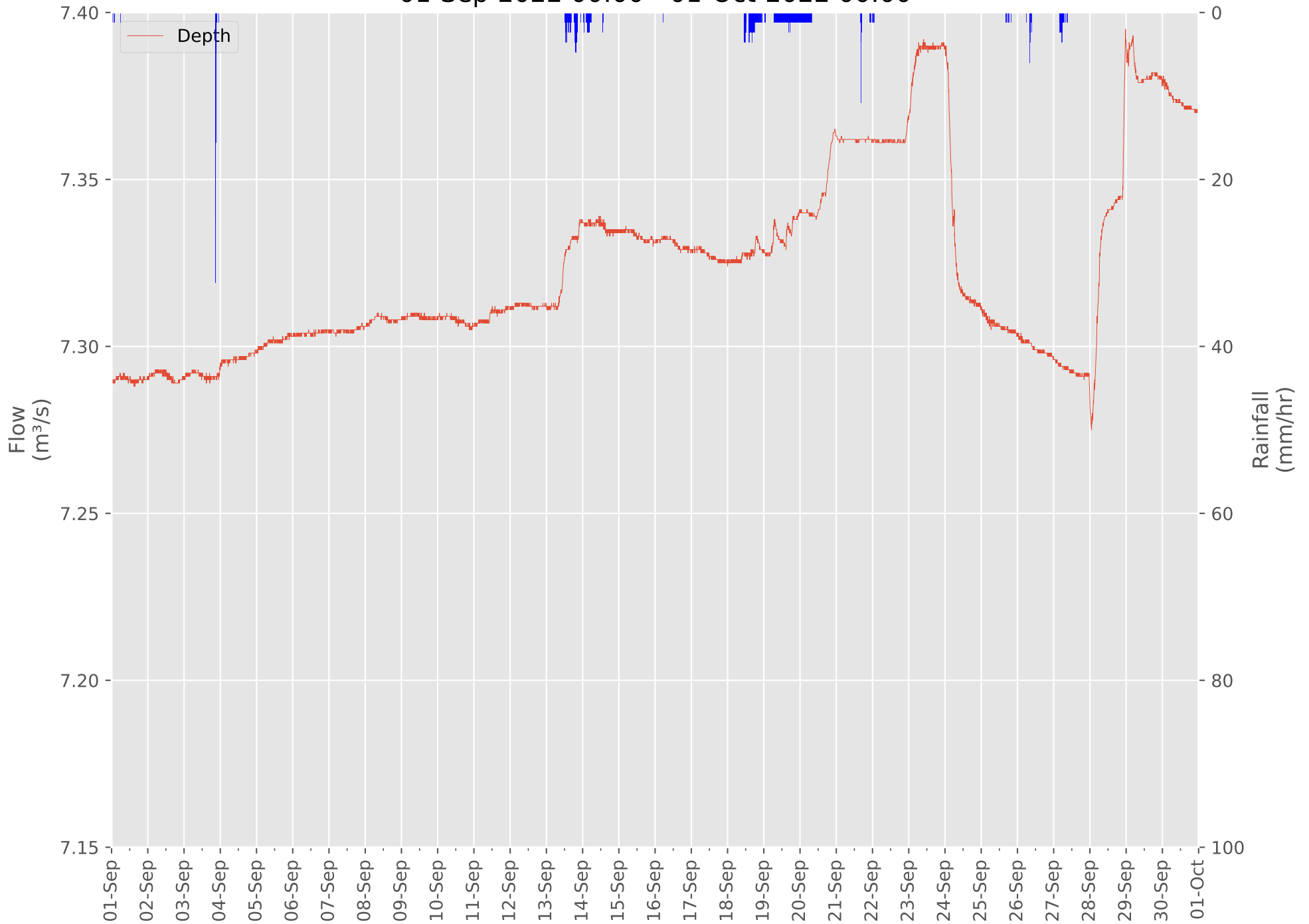
Tay River WSC Gauge Level

01-Aug-2022 00:00 - 01-Sep-2022 00:00



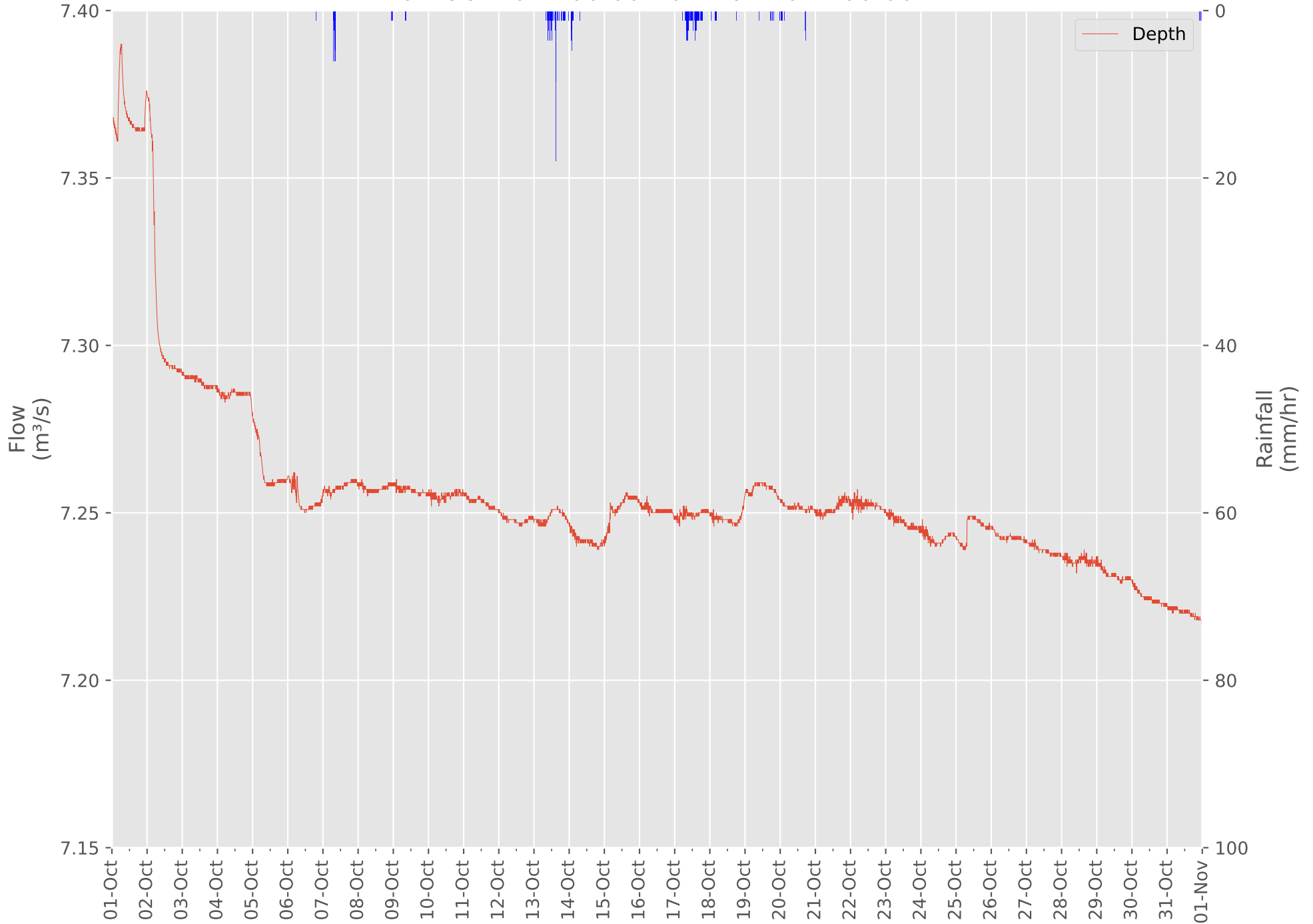
Tay River WSC Gauge Level

01-Sep-2022 00:00 - 01-Oct-2022 00:00



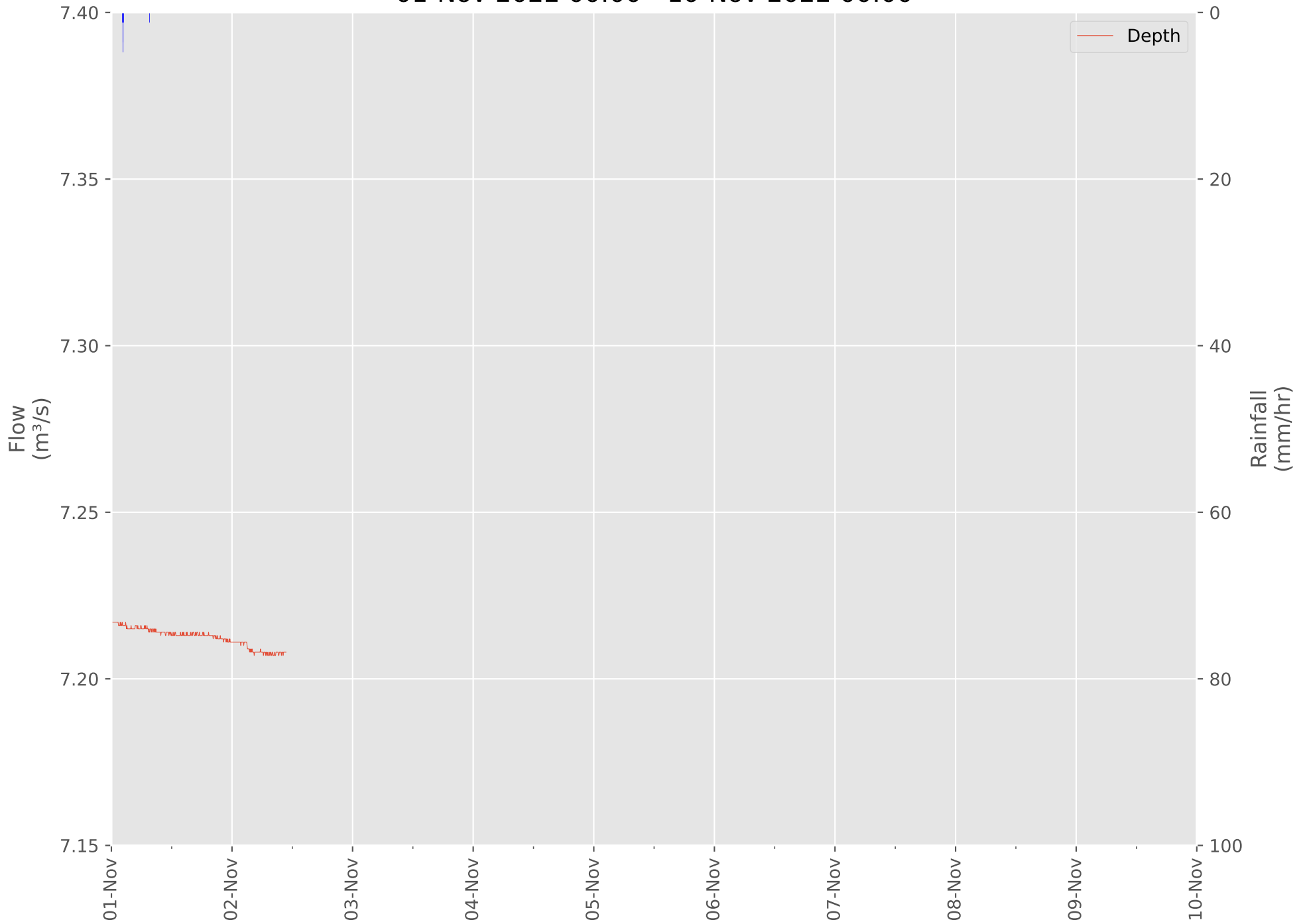
Tay River WSC Gauge Level

01-Oct-2022 00:00 - 01-Nov-2022 00:00



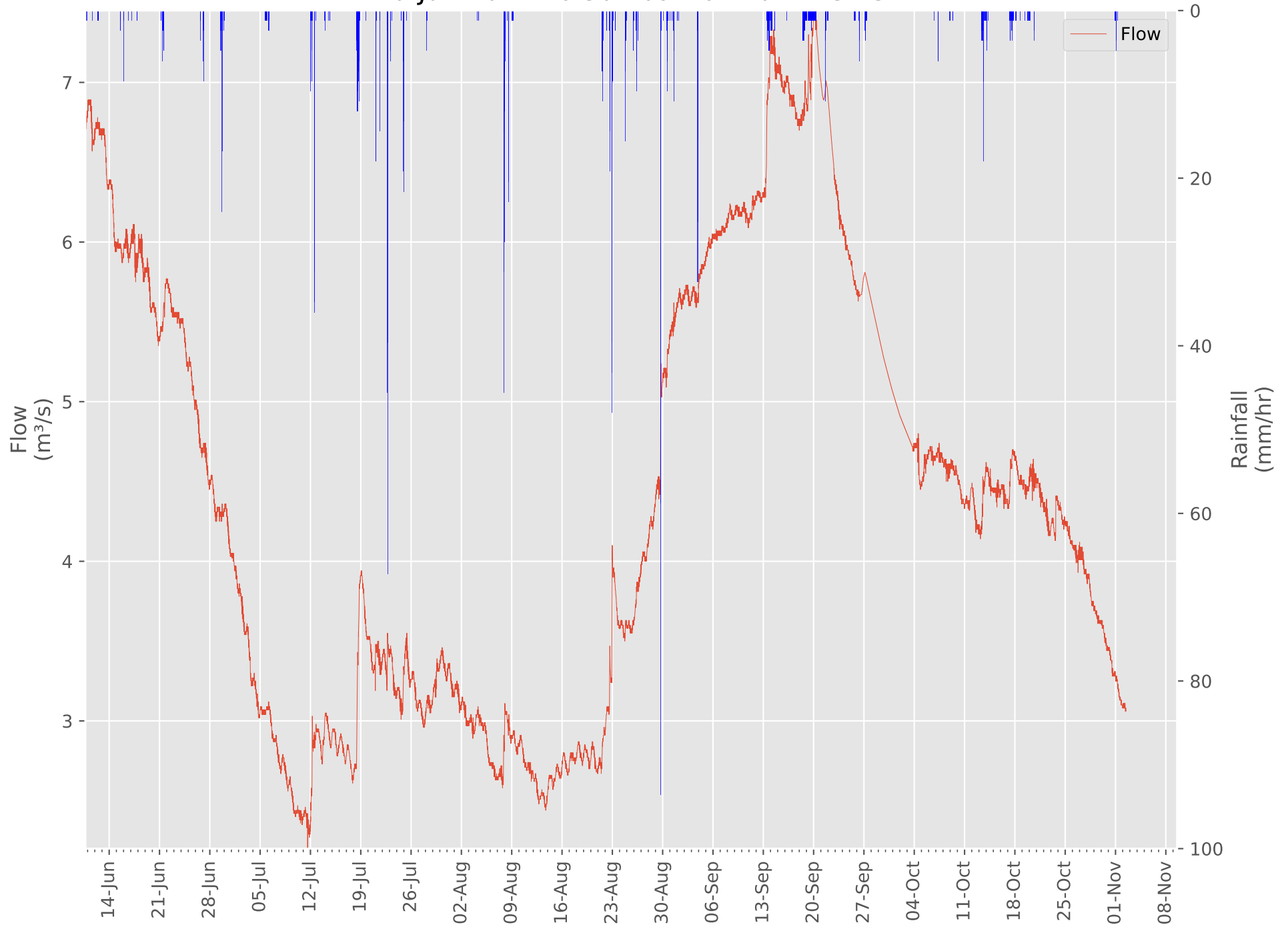
Tay River WSC Gauge Level

01-Nov-2022 00:00 - 10-Nov-2022 00:00



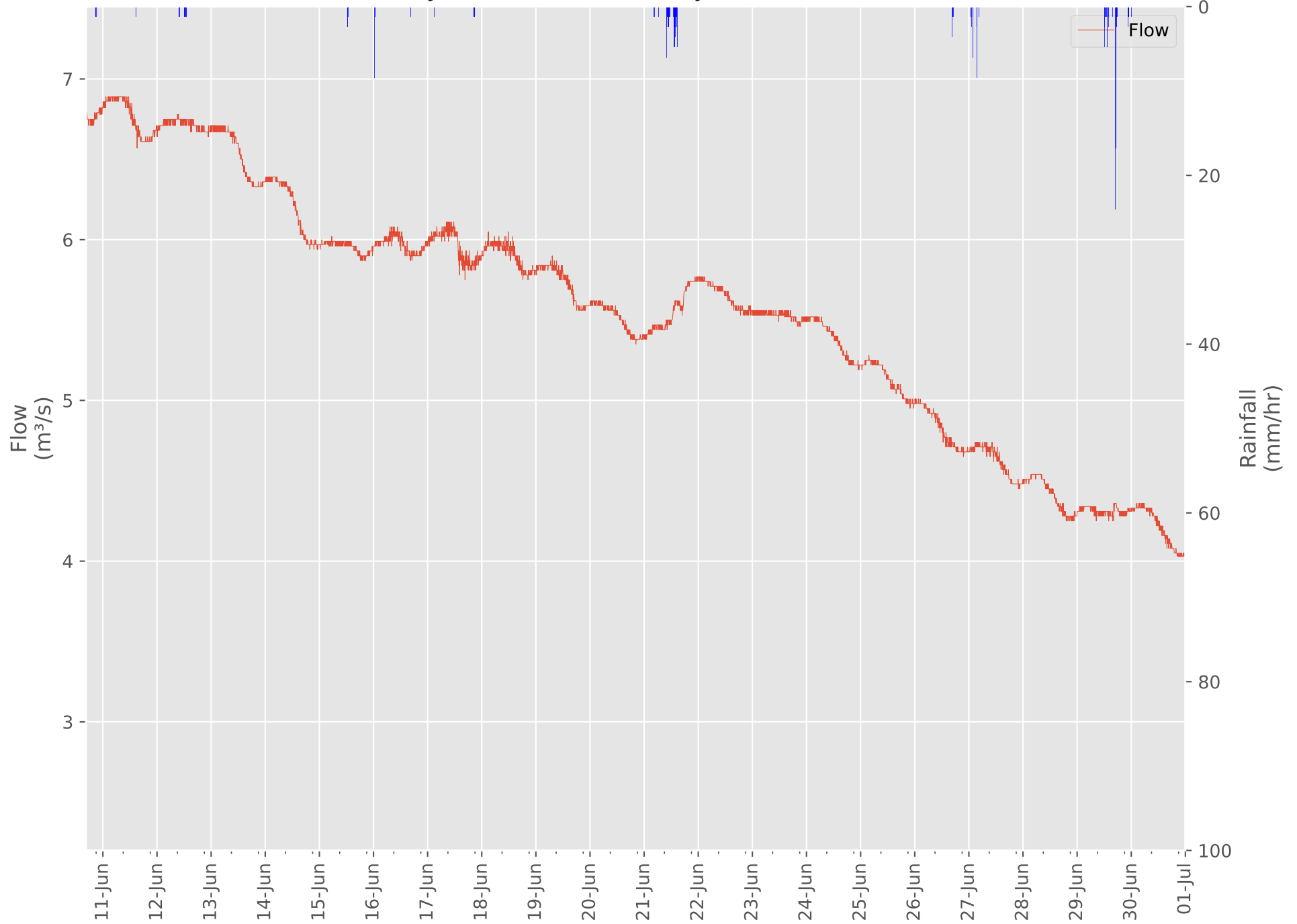
Tay River WSC Gauge Flow

10-Jun-2022 16:30 - 09-Nov-2022 13:45



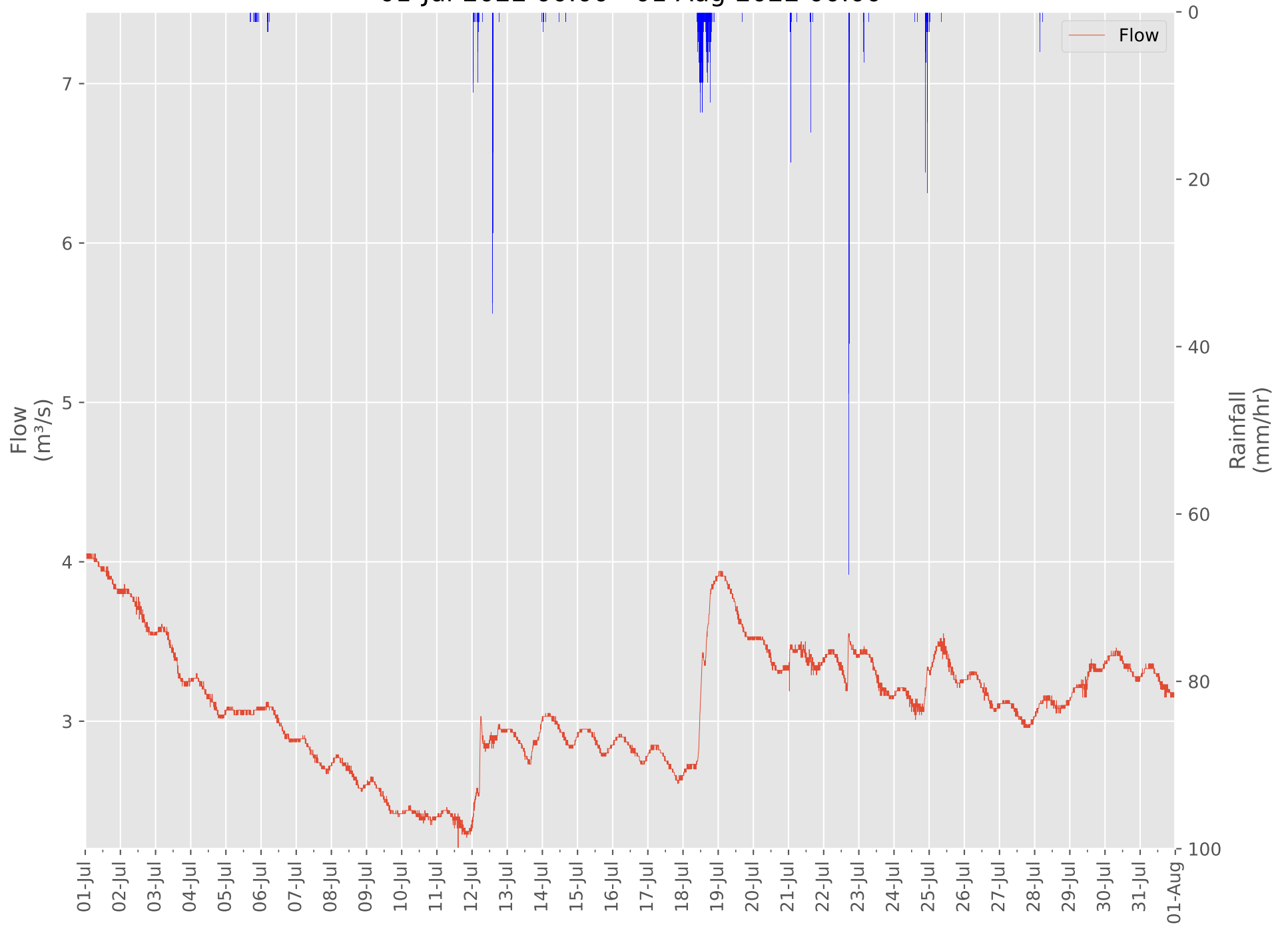
Tay River WSC Gauge Flow

10-Jun-2022 16:30 - 01-Jul-2022 00:00



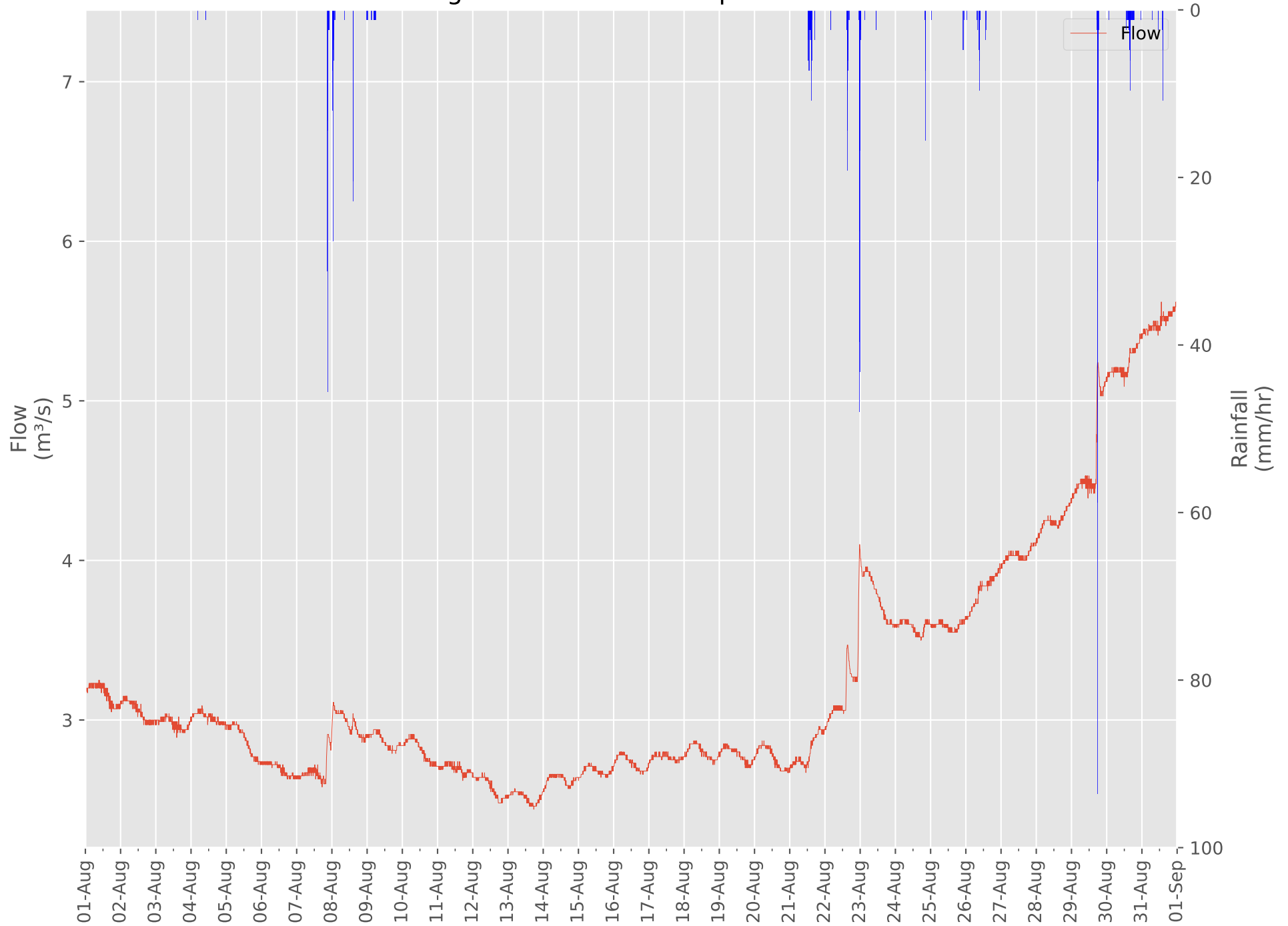
Tay River WSC Gauge Flow

01-Jul-2022 00:00 - 01-Aug-2022 00:00



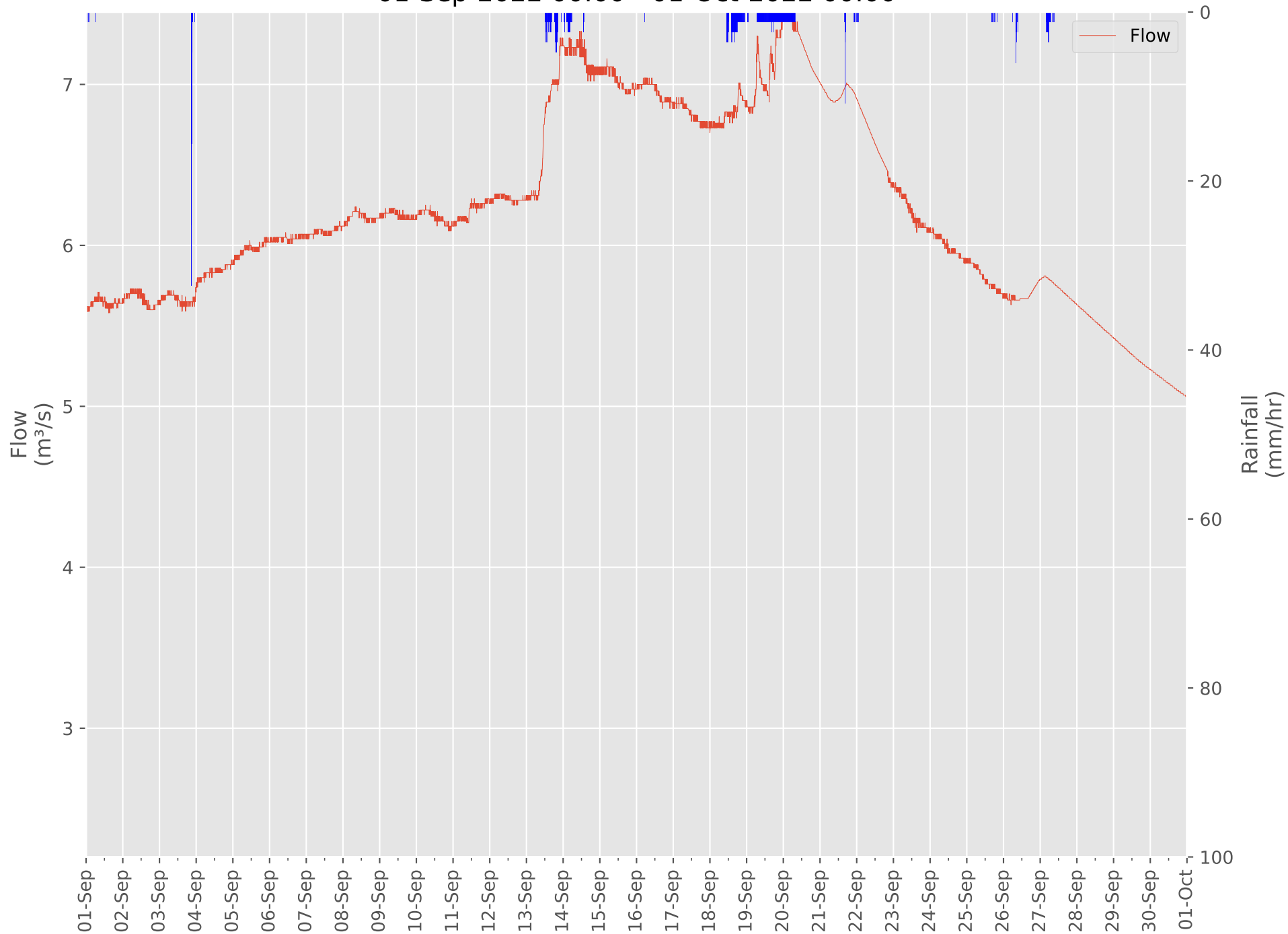
Tay River WSC Gauge Flow

01-Aug-2022 00:00 - 01-Sep-2022 00:00



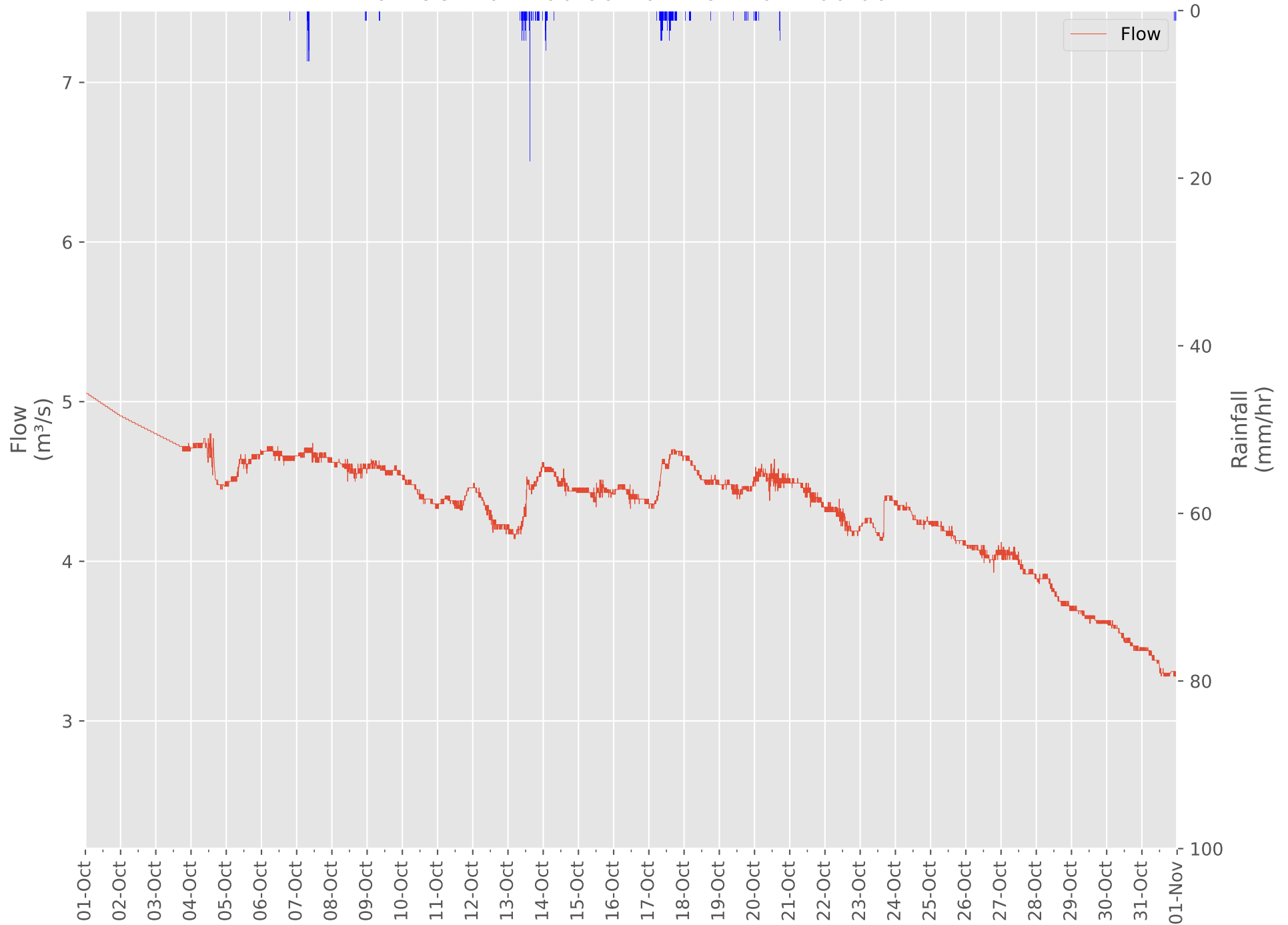
Tay River WSC Gauge Flow

01-Sep-2022 00:00 - 01-Oct-2022 00:00



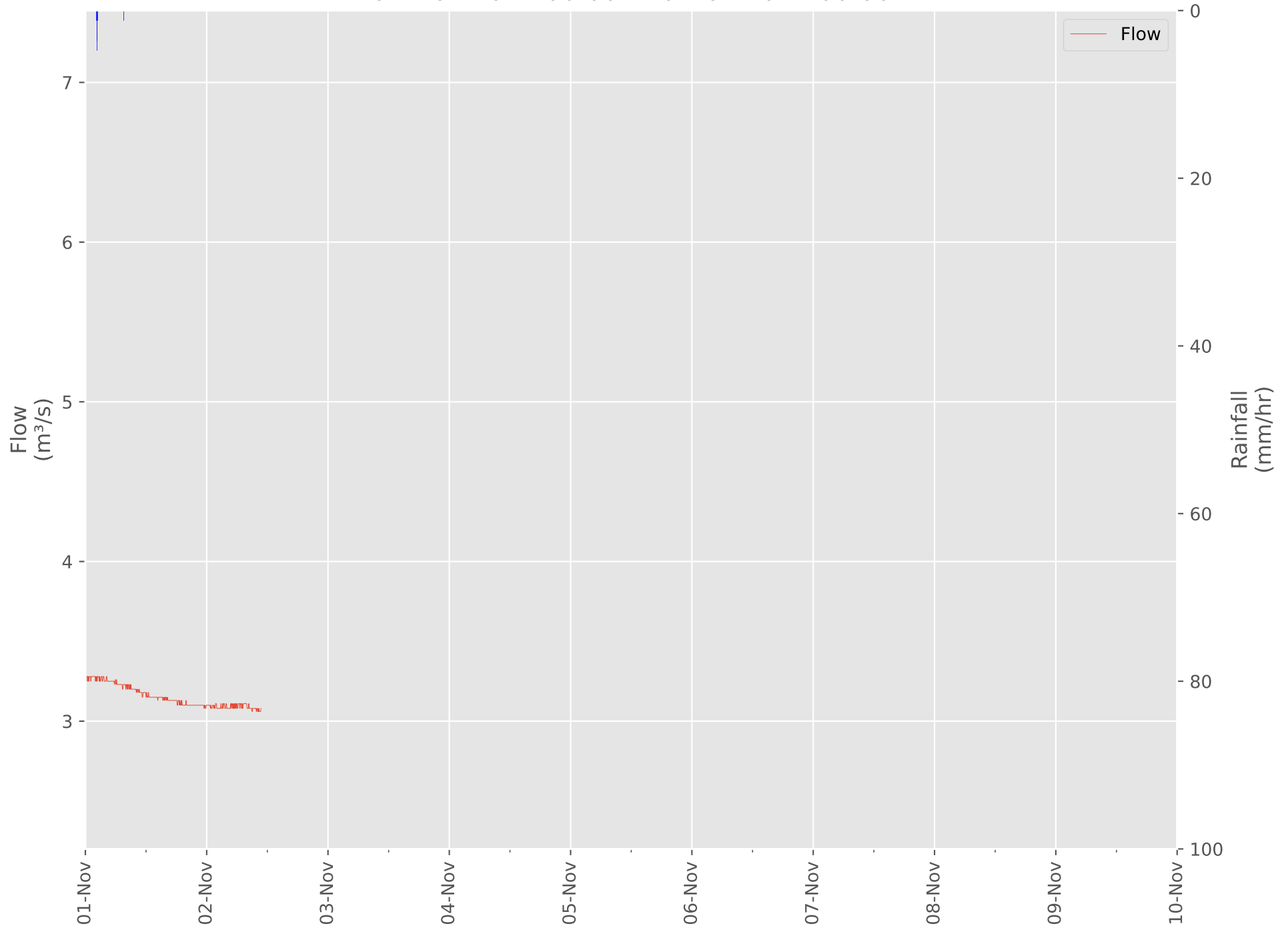
Tay River WSC Gauge Flow

01-Oct-2022 00:00 - 01-Nov-2022 00:00



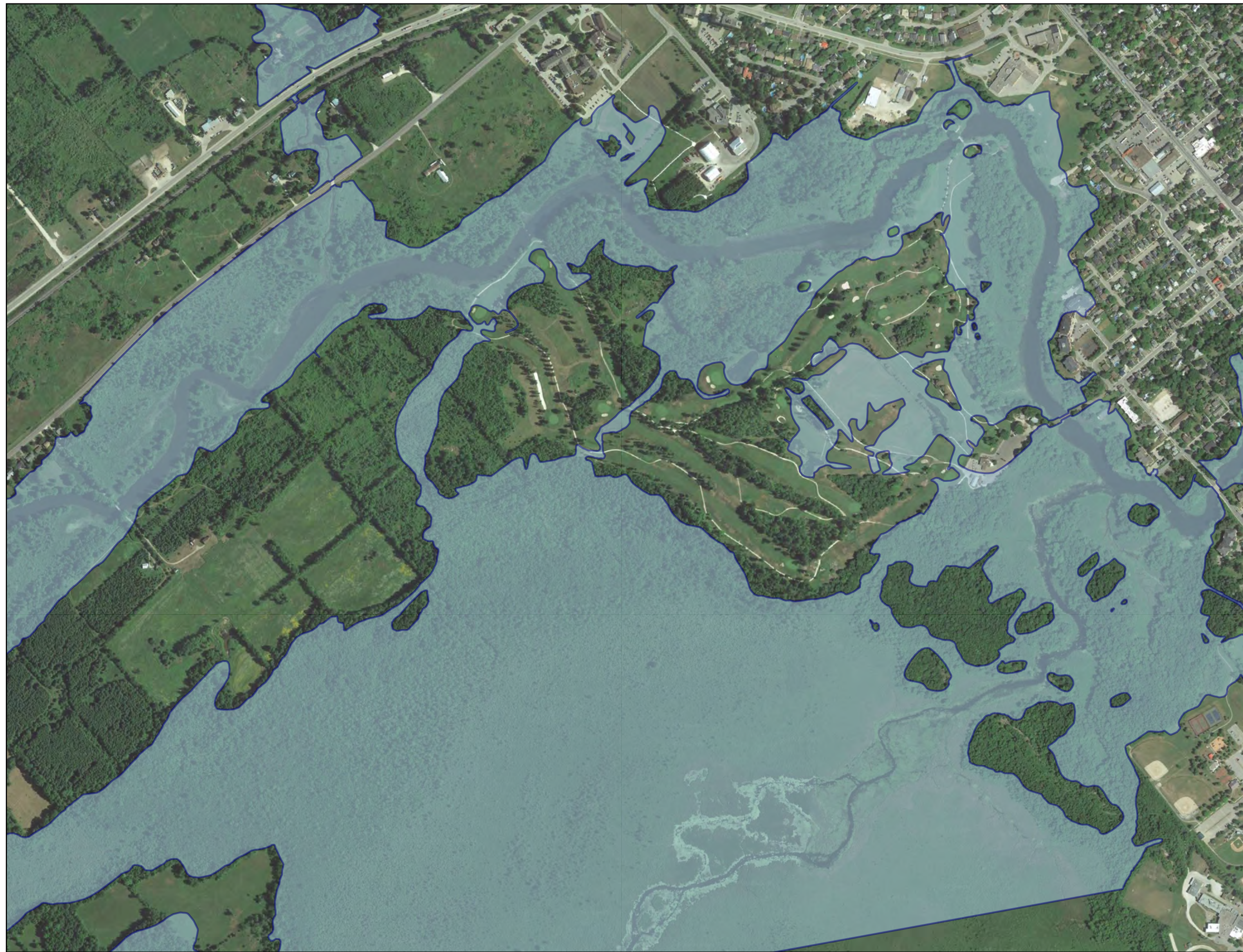
Tay River WSC Gauge Flow

01-Nov-2022 00:00 - 10-Nov-2022 00:00



Appendix C

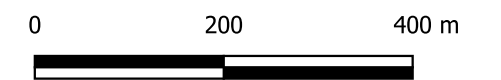
Floodplain Mapping



Legend

 RVCA Floodplain

SCALE: 1:8000



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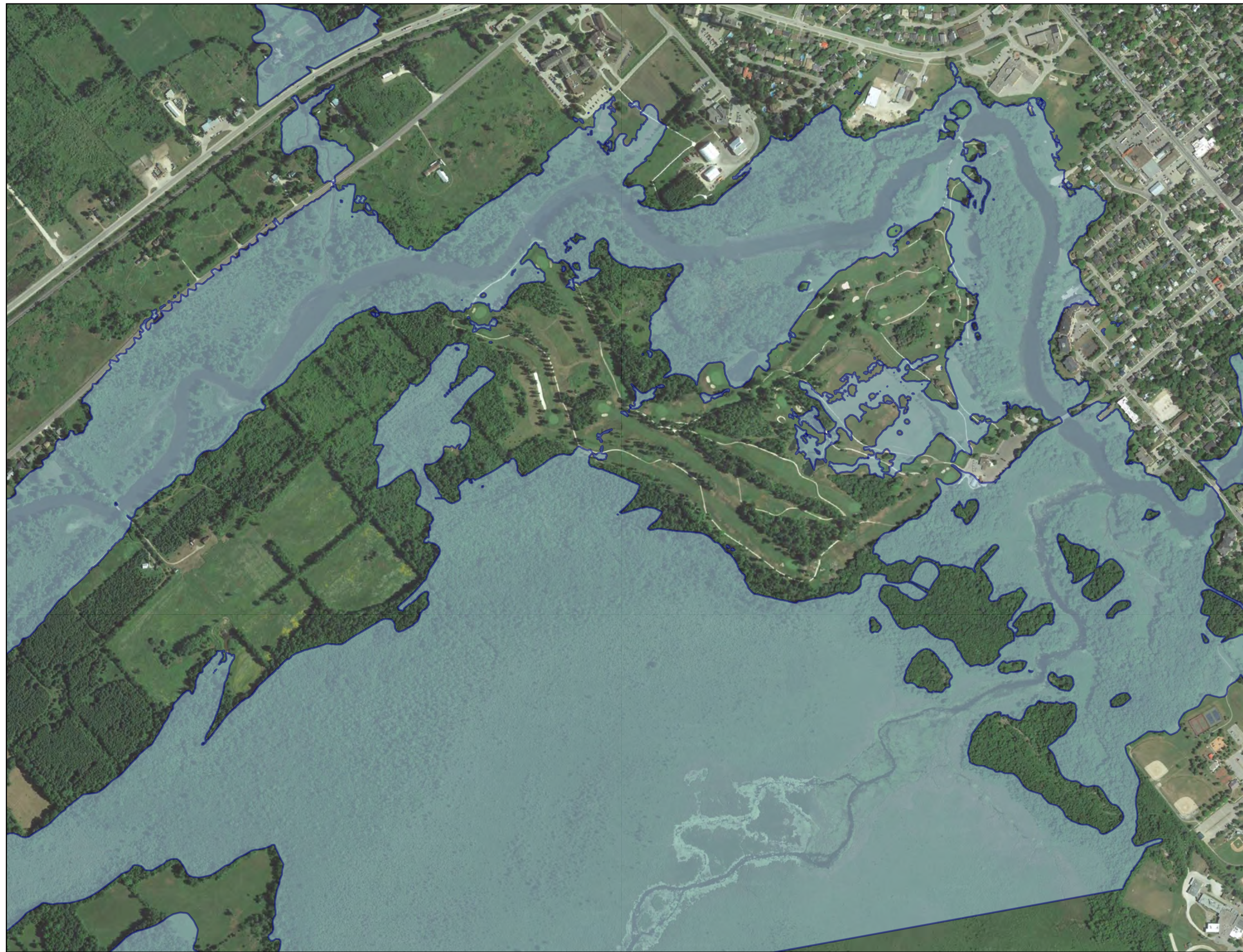
Perth Golf Course

Figure C1: RVCA Floodplain Boundary

PROJECT	2118-21
---------	---------

DRAWN	MP
-------	----

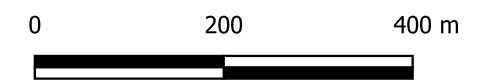
DATE	MAR 2022
------	----------




Legend

 2022 JFSA Floodplain

SCALE: 1:8000



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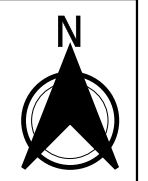
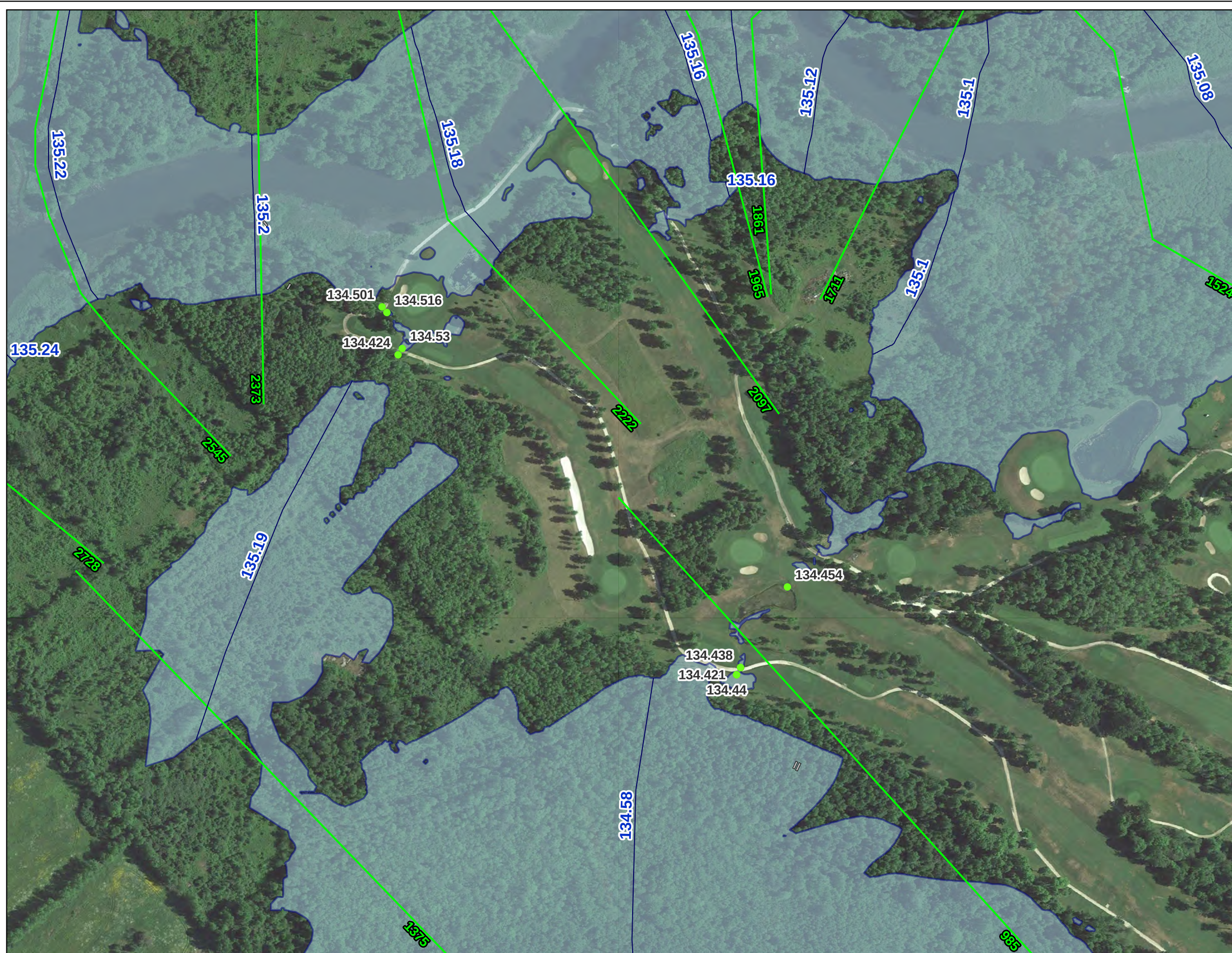
Perth Golf Course

Figure C2: JFSA Floodplain Boundary

PROJECT	2118-21
---------	---------

DRAWN	MP
-------	----

DATE	MAR 2022
------	----------



Legend

- 2022 JFSA Floodplain
- 2 cm Contours (m)
- RVCA Cross Sections
- Culvert Invert Elevation (m)

SCALE: 1:3000

0 50 100 m

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Figure C3: JFSA Flood Plain and Culvert Invert Elevations

PROJECT	2118-21
DRAWN	MP
DATE	MAR 2022

Appendix D

Existing Water Budget

Table D1 - Grants Creek - Pre Development Water Budget

Year	[1]	[1]-[2]-[4]		[2]		[3]	
	Precipitation (mm)	Total Evaporation (mm)	(%)	Total Infiltration (mm)	(%)	Total Runoff (mm)	(%)
1967	386.9	200.9	52%	54.3	14%	131.8	34%
1968	592.8	355.2	60%	85.9	14%	151.7	26%
1969	569.8	343.6	60%	84.4	15%	141.9	25%
1970	558.9	348.8	62%	82.1	15%	128.0	23%
1971	522.1	357.3	68%	72.4	14%	92.4	18%
1972	784.3	423.7	54%	118.1	15%	242.6	31%
1973	744.9	424.3	57%	113.8	15%	206.9	28%
1974	386.2	276.8	72%	48.5	13%	60.9	16%
1975	535.5	339.0	63%	78.1	15%	118.3	22%
1976	492.4	332.9	68%	65.6	13%	93.9	19%
1977	677.6	418.9	62%	99.9	15%	158.8	23%
1978	638.8	400.5	63%	110.6	17%	127.7	20%
1979	866.5	454.5	52%	136.8	16%	275.2	32%
1980	622	395.7	64%	91.6	15%	134.7	22%
1981	936.4	525.2	56%	120.4	13%	290.8	31%
1982	596.1	408.4	69%	83.3	14%	104.5	18%
1983	587.3	401.7	68%	73.4	13%	112.2	19%
1984	459.4	262.8	57%	76.5	17%	120.1	26%
1985	559.9	332.9	59%	105.9	19%	121.1	22%
1986	849.4	478.6	56%	117.8	14%	252.9	30%
1987	639.9	418.9	65%	79.1	12%	141.9	22%
1988	643.2	404.0	63%	87.4	14%	151.8	24%
1989	522.5	351.1	67%	70.9	14%	100.6	19%
1990	727.8	455.5	63%	98.7	14%	173.6	24%
1991	555.8	388.9	70%	62.8	11%	104.2	19%
1992	730.2	446.8	61%	103.3	14%	180.1	25%
1993	721.1	469.7	65%	97.4	14%	154.0	21%
1994	527	312.4	59%	81.8	16%	132.8	25%
1995	321.6	161.3	50%	48.6	15%	111.7	35%
1996	512.2	333.2	65%	66.4	13%	112.7	22%
1997	433.2	283.4	65%	72.0	17%	77.8	18%
1998	440.3	287.8	65%	66.9	15%	85.6	19%
1999	424.4	267.4	63%	71.6	17%	85.4	20%
2000	535.9	336.4	63%	76.1	14%	123.5	23%
2002	551.5	273.2	50%	86.7	16%	191.6	35%
2003	554.6	331.3	60%	76.9	14%	146.4	26%
Average	589.1	361.2	62%	85.2	15%	142.8	24%
Min	321.6	161.3	50%	48.5	11%	60.9	16%
Max	936.4	525.2	72%	136.8	19%	290.8	35%

Table D2 - Tay River - Pre Development Water Budget

Year	[1]	[1]-[2]-[4]		[2]		[3]	
	Precipitation (mm)	Total Evaporation (mm)	(%)	Total Infiltration (mm)	(%)	Total Runoff (mm)	(%)
1967	386.9	200.9	52%	60.6	16%	125.4	32%
1968	592.8	355.2	60%	95.2	16%	142.5	24%
1969	569.8	343.6	60%	93.4	16%	132.8	23%
1970	558.9	348.8	62%	90.5	16%	119.7	21%
1971	522.1	357.3	68%	78.9	15%	85.9	16%
1972	784.3	423.7	54%	131.3	17%	229.4	29%
1973	744.9	424.3	57%	126.5	17%	194.1	26%
1974	386.2	276.8	72%	52.8	14%	56.6	15%
1975	535.5	339.0	63%	85.8	16%	110.7	21%
1976	492.4	332.9	68%	72.0	15%	87.5	18%
1977	677.6	418.9	62%	109.9	16%	148.8	22%
1978	638.8	400.5	63%	120.6	19%	117.7	18%
1979	866.5	454.5	52%	152.2	18%	259.8	30%
1980	622	395.7	64%	100.3	16%	126.0	20%
1981	936.4	525.2	56%	134.0	14%	277.1	30%
1982	596.1	408.4	69%	90.7	15%	97.1	16%
1983	587.3	401.7	68%	80.7	14%	105.0	18%
1984	459.4	262.8	57%	84.3	18%	112.3	24%
1985	559.9	332.9	59%	115.6	21%	111.4	20%
1986	849.4	478.6	56%	130.7	15%	240.1	28%
1987	639.9	418.9	65%	87.2	14%	133.8	21%
1988	643.2	404.0	63%	96.8	15%	142.4	22%
1989	522.5	351.1	67%	77.8	15%	93.6	18%
1990	727.8	455.5	63%	109.2	15%	163.1	22%
1991	555.8	388.9	70%	69.3	12%	97.6	18%
1992	730.2	446.8	61%	114.3	16%	169.1	23%
1993	721.1	469.7	65%	107.2	15%	144.2	20%
1994	527	312.4	59%	90.7	17%	123.9	24%
1995	321.6	161.3	50%	53.8	17%	106.5	33%
1996	512.2	333.2	65%	73.2	14%	105.9	21%
1997	433.2	283.4	65%	78.2	18%	71.6	17%
1998	440.3	287.8	65%	73.2	17%	79.4	18%
1999	424.4	267.4	63%	78.3	18%	78.7	19%
2000	535.9	336.4	63%	83.8	16%	115.7	22%
2002	551.5	273.2	50%	96.3	17%	182.0	33%
2003	554.6	331.3	60%	85.0	15%	138.3	25%
Average	589.1	361.2	62%	93.9	16%	134.0	22%
Min	321.6	161.3	50%	52.8	12%	56.6	15%
Max	936.4	525.2	72%	152.2	21%	277.1	33%


```

20 Metric units / ID Numbers OFF
21 *#*****
22 *# SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
23 *#*****
24 *# Project Name : [Caivan Perth properties]
25 *# Project Number: [2118]
26 *# Date : [2023 JAN 26]
27 *# Modeller : [JB]
28 *# Company : J.F. Sabourin and Associates
29 *# License # : 2549237
30 *#*****
31 *#*****
32 *# Model developed to simulate pre-development water budget
33 *#*****
34
35 START TZERO=[1967.0101], METOUT=[2], NSTORM=[0], NRUN=[67]
36 *% [ " ] <--storm filename, one per line for NSTORM time
37 *%-----|-----
38 *# Ottawa International Airport (1967 - 2003)
39 READ AES DATA AES_FILENAME=[ "6106000.123" ],
40 IELEM=[123], START_DATE=[0], END_DATE=[-364]
41 *%-----|-----
42 COMPUTE API APII=[50], APIK=[0.90]/day
43 *#####
44 *# Pre Development Condition - Using NASHHYD and CN
45 *#####
46 CONTINUOUS NASHYD NHYD=[ "GrantsPre" ], DT=[5]min, AREA=[22.01](ha),
47 DWF=[0](cms), CN/C=[92], IA=[8.75](mm),
48 N=[3], TP=[0.24]hrs,
49 Continuous simulation parameters:
50 IaRECper=[24](hrs),SMIN=[ -1 ](mm), SMAX=[ -1 ](mm),
51 SK=[0.3]/(mm), InterEventTime=[ 12 ](hrs)
52 END=-1
53 *%-----|-----
54
55 CONTINUOUS NASHYD NHYD=[ "TayPre" ], DT=[5]min, AREA=[22.86](ha),
56 DWF=[0](cms), CN/C=[90], IA=[8.75](mm),
57 N=[3], TP=[0.36]hrs,
58 Continuous simulation parameters:
59 IaRECper=[24](hrs),SMIN=[ -1 ](mm), SMAX=[ -1 ](mm),
60 SK=[0.3]/(mm), InterEventTime=[ 12 ](hrs)
61 END=-1
62 *%-----|-----
63 *ADD HYD NHYDsum=[ "Pre" ], NHYDs to add=[ "GrantsPre"+"TayPre" ]
64 *#####
65 *# Pre Development Condition - Using NASHHYD and CN - No INFILTRATION
66 *#####
67 CONTINUOUS NASHYD NHYD=[ "InfGrantsPre" ], DT=[5]min, AREA=[22.01](ha),
68 DWF=[0](cms), CN/C=[99.99], IA=[8.75](mm),
69 N=[3], TP=[0.24]hrs,
70 Continuous simulation parameters:
71 IaRECper=[24](hrs),SMIN=[ 0 ](mm), SMAX=[ 0 ](mm), SK=[0.3]/(mm),
72 InterEventTime=[ 12 ](hrs)
73 END=-1
74 *%-----|-----
75 CONTINUOUS NASHYD NHYD=[ "InfTayPre" ], DT=[5]min, AREA=[22.86](ha),
76 DWF=[0](cms), CN/C=[99.99], IA=[8.75](mm),
77 N=[3], TP=[0.36]hrs,
78 Continuous simulation parameters:
79 IaRECper=[24](hrs),SMIN=[ 0 ](mm), SMAX=[ 0 ](mm), SK=[0.3]/(mm),
80 InterEventTime=[ 12 ](hrs)
81 END=-1
82 *%-----|-----
83 *ADD HYD NHYDsum=[ "InfPre" ], NHYDs to add=[ "InfGrantsPre"+"InfTayPre" ]
84 *%-----|-----
85 *#####
86 *# STORMS
87 *#####

```

```
64 START TZERO=[1968.0101], METOUT=[2], NSTORM=[0], NRUN=[68]
65 *%-----|-----|-----|-----|-----|-----|-----|-----|
66 START TZERO=[1969.0101], METOUT=[2], NSTORM=[0], NRUN=[69]
67 *%-----|-----|-----|-----|-----|-----|-----|-----|
68 START TZERO=[1970.0101], METOUT=[2], NSTORM=[0], NRUN=[70]
69 *%-----|-----|-----|-----|-----|-----|-----|-----|
70 START TZERO=[1971.0101], METOUT=[2], NSTORM=[0], NRUN=[71]
71 *%-----|-----|-----|-----|-----|-----|-----|-----|
72 START TZERO=[1972.0101], METOUT=[2], NSTORM=[0], NRUN=[72]
73 *%-----|-----|-----|-----|-----|-----|-----|-----|
74 START TZERO=[1973.0101], METOUT=[2], NSTORM=[0], NRUN=[73]
75 *%-----|-----|-----|-----|-----|-----|-----|-----|
76 START TZERO=[1974.0101], METOUT=[2], NSTORM=[0], NRUN=[74]
77 *%-----|-----|-----|-----|-----|-----|-----|-----|
78 START TZERO=[1975.0101], METOUT=[2], NSTORM=[0], NRUN=[75]
79 *%-----|-----|-----|-----|-----|-----|-----|-----|
80 START TZERO=[1976.0101], METOUT=[2], NSTORM=[0], NRUN=[76]
81 *%-----|-----|-----|-----|-----|-----|-----|-----|
82 START TZERO=[1977.0101], METOUT=[2], NSTORM=[0], NRUN=[77]
83 *%-----|-----|-----|-----|-----|-----|-----|-----|
84 START TZERO=[1978.0101], METOUT=[2], NSTORM=[0], NRUN=[78]
85 *%-----|-----|-----|-----|-----|-----|-----|-----|
86 START TZERO=[1979.0101], METOUT=[2], NSTORM=[0], NRUN=[79]
87 *%-----|-----|-----|-----|-----|-----|-----|-----|
88 START TZERO=[1980.0101], METOUT=[2], NSTORM=[0], NRUN=[80]
89 *%-----|-----|-----|-----|-----|-----|-----|-----|
90 START TZERO=[1981.0101], METOUT=[2], NSTORM=[0], NRUN=[81]
91 *%-----|-----|-----|-----|-----|-----|-----|-----|
92 START TZERO=[1982.0101], METOUT=[2], NSTORM=[0], NRUN=[82]
93 *%-----|-----|-----|-----|-----|-----|-----|-----|
94 START TZERO=[1983.0101], METOUT=[2], NSTORM=[0], NRUN=[83]
95 *%-----|-----|-----|-----|-----|-----|-----|-----|
96 START TZERO=[1984.0101], METOUT=[2], NSTORM=[0], NRUN=[84]
97 *%-----|-----|-----|-----|-----|-----|-----|-----|
98 START TZERO=[1985.0101], METOUT=[2], NSTORM=[0], NRUN=[85]
99 *%-----|-----|-----|-----|-----|-----|-----|-----|
100 START TZERO=[1986.0101], METOUT=[2], NSTORM=[0], NRUN=[86]
101 *%-----|-----|-----|-----|-----|-----|-----|-----|
102 START TZERO=[1987.0101], METOUT=[2], NSTORM=[0], NRUN=[87]
103 *%-----|-----|-----|-----|-----|-----|-----|-----|
104 START TZERO=[1988.0101], METOUT=[2], NSTORM=[0], NRUN=[88]
105 *%-----|-----|-----|-----|-----|-----|-----|-----|
106 START TZERO=[1989.0101], METOUT=[2], NSTORM=[0], NRUN=[89]
107 *%-----|-----|-----|-----|-----|-----|-----|-----|
108 START TZERO=[1990.0101], METOUT=[2], NSTORM=[0], NRUN=[90]
109 *%-----|-----|-----|-----|-----|-----|-----|-----|
110 START TZERO=[1991.0101], METOUT=[2], NSTORM=[0], NRUN=[91]
111 *%-----|-----|-----|-----|-----|-----|-----|-----|
112 START TZERO=[1992.0101], METOUT=[2], NSTORM=[0], NRUN=[92]
113 *%-----|-----|-----|-----|-----|-----|-----|-----|
114 START TZERO=[1993.0101], METOUT=[2], NSTORM=[0], NRUN=[93]
115 *%-----|-----|-----|-----|-----|-----|-----|-----|
116 START TZERO=[1994.0101], METOUT=[2], NSTORM=[0], NRUN=[94]
117 *%-----|-----|-----|-----|-----|-----|-----|-----|
118 START TZERO=[1995.0101], METOUT=[2], NSTORM=[0], NRUN=[95]
119 *%-----|-----|-----|-----|-----|-----|-----|-----|
120 START TZERO=[1996.0101], METOUT=[2], NSTORM=[0], NRUN=[96]
121 *%-----|-----|-----|-----|-----|-----|-----|-----|
122 START TZERO=[1997.0101], METOUT=[2], NSTORM=[0], NRUN=[97]
123 *%-----|-----|-----|-----|-----|-----|-----|-----|
124 START TZERO=[1998.0101], METOUT=[2], NSTORM=[0], NRUN=[98]
125 *%-----|-----|-----|-----|-----|-----|-----|-----|
126 START TZERO=[1999.0101], METOUT=[2], NSTORM=[0], NRUN=[99]
127 *%-----|-----|-----|-----|-----|-----|-----|-----|
128 START TZERO=[2000.0101], METOUT=[2], NSTORM=[0], NRUN=[100]
129 *%-----|-----|-----|-----|-----|-----|-----|-----|
130 *% MISSING FROM AES RAINFALL DATA
131 *%START TZERO=[2001.0101], METOUT=[2], NSTORM=[0], NRUN=[101]
132 *%-----|-----|-----|-----|-----|-----|-----|-----|
```

```
133  START                TZERO=[2002.0101],  METOUT=[2],  NSTORM=[0],  NRUN=[102]
134  *%-----|-----|
135  START                TZERO=[2003.0101],  METOUT=[2],  NSTORM=[0],  NRUN=[103]
136  *%-----|-----|
137  FINISH
```

00181 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
00182 17 83 44 27 69 48 43 36
00183 Number of events with at least the following durations
00184 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
00185 156 76 49 18 5 0 0 0 0
00186 R0069/C00002-----
00187 COMPUTE API
00188 [APInI= 50.00; APIdkY= 9000; APIdkz= 9956]
00189 [APImax= 67.52; APITavg= 16.69; APInIm= 27]
00190 *****
00191 # Pre Development Condition - Using SHAWHYD and CN
00192 *****
00193 R0068/C00004-----
00194 CONTINUOUS NASHYD 5.0 01:Grantprp 22.01 1.566 1968.081e_5:00 151.71 256 .000
00195 [CN= 92.0; IM= 3.00; Tps= .24]
00196 [IAREC=24.00; SMIN= 10.51; SMAX= 70.09; SK= .300]
00197 [InterEventTime= 12.00]
00198 R0068/C00005-----
00199 CONTINUOUS NASHYD 5.0 01:Traypre 22.86 1.226 1968.081e_5:05 142.46 240 .000
00200 [CN= 90.0; IM= 3.00; Tps= .38]
00201 [IAREC=24.00; SMIN= 12.64; SMAX= 84.28; SK= .300]
00202 [InterEventTime= 12.00]
00203 *****
00204 # Pre Development Condition - Using SHAWHYD and CN - NO INFILTRATION
00205 *****
00206 R0068/C00006-----
00207 CONTINUOUS NASHYD 5.0 01:InfGrantprp 22.01 1.960 1968.081e_5:00 337.63 401 .000
00208 [CN=100.0; IM= 3.00; Tps= .24]
00209 [IAREC=24.00; SMIN= .00; SMAX= .00; SK= .300]
00210 [InterEventTime= 12.00]
00211 R0068/C00007-----
00212 CONTINUOUS NASHYD 5.0 01:InfTraypre 22.86 1.728 1968.081e_5:05 337.63 401 .000
00213 [CN=100.0; IM= 3.00; Tps= .38]
00214 [IAREC=24.00; SMIN= .00; SMAX= .00; SK= .300]
00215 [InterEventTime= 12.00]
00216 *****
00217 *****
00218 *****
00219 ** END OF RUN = 68
00220 *****
00221 *****
00222 *****
00223 *****
00224 *****
00225 *****
00226 *****
00227 *****
00228 R0069/C00001-----
00229 START
00230 [TZERO = .00 hrs on 19670101]
00231 [NETOUT= 2 (1=imperial, 2=metric output)]
00232 [NETSUM= 0]
00233 [NETIN = 069]
00234 *****
00235 # SWMHYD Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
00236 *****
00237 # Project Name : [Caivan Perth properties]
00238 # Project Number: [2118]
00239 # Date : [2023 JAN 26]
00240 # Modeller : [JB]
00241 # Company : J.F. Sabourin and Associates
00242 # License #: 2549237
00243 *****
00244 # Model developed to simulate pre-development water budget
00245 *****
00246 # Ottawa International Airport (1967 - 2003)
00247 *****
00248 R0069/C00002-----
00249 * READ ARE DATA
00250 [Filename = 610600.123]
00251 [Start_date= 1969.0101; End_date= 1969.1231]
00252 [Drs= 60;min; Length= 8984; hrs; Wethrs= 257; Dryhrs= 3727; PTO= 386.90]
00253 Maximum average rainfall intensities over
00254 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs mm/hr
00255 21.10 16.25 19.83 7.78 3.93 2.10 1.40 1.09 .75
00256 21.10 32.50 32.50 46.70 47.20 50.30 50.30 52.10 54.00 mm
00257 19690817 19690817 19690819 19690819 19690819 19690819 19690819 19690819 19690819 date
00258 Number of rainfall events per following interval time
00259 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
00260 187 119 107 92 72 58 49 43 32
00261 Number of events with at least the following durations
00262 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
00263 156 84 58 21 5 0 0 0 0
00264 R0069/C00001-----
00265 COMPUTE API
00266 [APInI= 50.00; APIdkY= 9000; APIdkz= 9956]
00267 [APImax= 56.77; APITavg= 16.04; APInIm= 26]
00268 *****
00269 # Pre Development Condition - Using SHAWHYD and CN
00270 *****
00271 R0069/C00004-----
00272 CONTINUOUS NASHYD 5.0 01:Grantprp 22.01 1.080 1969.081e_2:00 141.98 249 .000
00273 [CN= 92.0; IM= 3.00; Tps= .24]
00274 [IAREC=24.00; SMIN= 10.51; SMAX= 70.09; SK= .300]
00275 [InterEventTime= 12.00]
00276 R0069/C00005-----
00277 CONTINUOUS NASHYD 5.0 01:Traypre 22.86 .939 1969.081e_2:05 132.90 233 .000
00278 [CN= 90.0; IM= 3.00; Tps= .38]
00279 [IAREC=24.00; SMIN= 12.64; SMAX= 84.28; SK= .300]
00280 [InterEventTime= 12.00]
00281 *****
00282 # Pre Development Condition - Using SHAWHYD and CN - NO INFILTRATION
00283 *****
00284 R0069/C00006-----
00285 CONTINUOUS NASHYD 5.0 01:InfGrantprp 22.01 1.284 1969.081e_2:00 226.24 397 .000
00286 [CN=100.0; IM= 3.00; Tps= .24]
00287 [IAREC=24.00; SMIN= .00; SMAX= .00; SK= .300]
00288 [InterEventTime= 12.00]
00289 R0069/C00007-----
00290 CONTINUOUS NASHYD 5.0 01:InfTraypre 22.86 1.259 1969.081e_2:00 226.24 397 .000
00291 [CN=100.0; IM= 3.00; Tps= .38]
00292 [IAREC=24.00; SMIN= .00; SMAX= .00; SK= .300]
00293 [InterEventTime= 12.00]
00294 *****
00295 # STORMS
00296 ** END OF RUN = 69
00297 *****
00298 *****
00299 *****
00300 *****
00301 *****
00302 *****
00303 *****
00304 *****
00305 *****
00306 R0070/C00001-----
00307 STORMS
00308 [TZERO = .00 hrs on 19700101]
00309 [NETOUT= 2 (1=imperial, 2=metric output)]
00310 [NETSUM= 0]
00311 [NETIN = 070]
00312 *****
00313 # SWMHYD Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
00314 *****
00315 # Project Name : [Caivan Perth properties]
00316 # Project Number: [2118]
00317 # Date : [2023 JAN 26]
00318 # Modeller : [JB]
00319 # Company : J.F. Sabourin and Associates
00320 # License #: 2549237
00321 *****
00322 # Model developed to simulate pre-development water budget
00323 *****
00324 # Ottawa International Airport (1967 - 2003)
00325 *****
00326 R0070/C00002-----
00327 * READ ARE DATA
00328 [Filename = 610600.123]
00329 [Start_date= 1970.0101; End_date= 1970.1231]
00330 [Drs= 60;min; Length= 8016; hrs; Wethrs= 373; Dryhrs= 7643; PTO= 558.90]
00331 Maximum average rainfall intensities over
00332 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs mm/hr
00333 35.30 18.30 18.20 6.10 3.63 1.81 1.21 1.46 .99
00334 35.30 36.60 36.60 36.60 43.50 43.50 43.50 43.50 43.50 mm
00335 19700826 19700826 19700827 19700827 19700827 19700827 19700827 19700827 19700827 date
00336 Number of rainfall events per following interval time
00337 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
00338 148 127 109 84 72 60 53 40 29
00339 Number of events with at least the following durations
00340 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
00341 147 79 40 15 3 0 0 0 0
00342 R0070/C00003-----
00343 COMPUTE API
00344 [APInI= 50.00; APIdkY= 9000; APIdkz= 9956]
00345 [APImax= 76.00; APITavg= 11.31; APInIm= 23]
00346 *****
00347 # Pre Development Condition - Using SHAWHYD and CN
00348 *****
00349 R0070/C00004-----
00350 CONTINUOUS NASHYD 5.0 01:Grantprp 22.01 1.671 1970.092e_2:00 328.02 229 .000
00351 [CN= 92.0; IM= 3.00; Tps= .24]
00352 [IAREC=24.00; SMIN= 10.51; SMAX= 70.09; SK= .300]
00353 [InterEventTime= 12.00]
00354 R0070/C00005-----
00355 CONTINUOUS NASHYD 5.0 01:InfTraypre 22.86 1.310 1970.092e_2:05 332.65 214 .000
00356 [CN= 90.0; IM= 3.00; Tps= .38]
00357 [IAREC=24.00; SMIN= 12.64; SMAX= 84.28; SK= .300]
00358 [InterEventTime= 12.00]
00359 *****
00360 # Pre Development Condition - Using SHAWHYD and CN - NO INFILTRATION
00361 *****


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01261 # Ottawa International Airport (1967 - 2003)
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01441 R0884-C0004-----DRAIN-ID:INHVD-----AREHA-QPEARcms-TpeakDate_hh:mm-----Rvum-R.C.--DWfms
01442 CONTINUOUS NASHYD 5.0 01:InfTranPre 22.01 .724 1984.0812, 7:00 120.12 261 .000
01443 [Cm 90.0: N# 3.00: Tp# .24]
01444 [IAREC=24.00: SMIN= 10.51: SMAX= 70.09: SK= .300]
01445 [InterEventTime= 12.00]
01446 R0884-C0005-----DRAIN-ID:INHVD-----AREHA-QPEARcms-TpeakDate_hh:mm-----Rvum-R.C.--DWfms
01447 CONTINUOUS NASHYD 5.0 01:InfTranPre 22.86 .990 1984.0812,16:05 112.33 245 .000
01448 [Cm 90.0: N# 3.00: Tp# .38]
01449 [IAREC=24.00: SMIN= 12.64: SMAX= 84.28: SK= .300]
01450 [InterEventTime= 12.00]
01451 *****
01452 # Pre Development Condition - Using NASHYD and CN - No INFILTRATION
01453 *****
01454 R0884-C0006-----DRAIN-ID:INHVD-----AREHA-QPEARcms-TpeakDate_hh:mm-----Rvum-R.C.--DWfms
01455 CONTINUOUS NASHYD 5.0 01:InfTranPre 22.01 1.059 1984.0812, 7:00 196.45 428 .000
01456 [Cm 100.0: N# 3.00: Tp# .24]
01457 [IAREC=24.00: SMIN= .00: SMAX= .00: SK= .300]
01458 [InterEventTime= 12.00]
01459 R0884-C0007-----DRAIN-ID:INHVD-----AREHA-QPEARcms-TpeakDate_hh:mm-----Rvum-R.C.--DWfms
01460 CONTINUOUS NASHYD 5.0 01:InfTranPre 22.86 .954 1984.0812, 7:05 196.45 428 .000
01461 [Cm 100.0: N# 3.00: Tp# .38]
01462 [IAREC=24.00: SMIN= .00: SMAX= .00: SK= .300]
01463 [InterEventTime= 12.00]
01464 *****
01465 # STORMS
01466 *****
01467 ** END OF RUN : 84
01468 *****
01469 *****
01470 *****
01471 *****
01472 *****
01473 *****
01474 *****
01475 RUN# COMMAND#
01476 R0885-C0001-----
01477 START
01478 [TZERO = .00 hrs on 19850101]
01479 [NETOUT= 2 (1=Imperial, 2=metric output)]
01480 [NETFORM= 0]
01481 [NRUN = 0089]
01482 *****
01483 # SWHMYO Ver:5.02/Jan 2001 <BETA / INPUT DATA FILE
01484 *****
01485 # Project Name : [Caivan Perth properties]
01486 # Project Number : [2118]
01487 # Date : [2023 JAN 26]
01488 # Modeller : [JFB]
01489 # Company : [J.F. Sabourin and Associates]
01490 # License # : [2549237]
01491 *****
01492 # Model developed to simulate pre-development water budget
01493 *****
01494 # Ottawa International Airport (1967 - 2003)
01495 *****
01496 R0885-C0002-----
01497 READ A&S DATA
01498 [Filename = 6106000.123]
01499 [Start_date= 1985.0101: End_date= 1985.1231]
01500 [Dtr= 60.min: Length= 8760.hrs: WetRcs= 884: DryRcs= 8406: PTOF= 559.90]
01501 *****
01502 Maximum average rainfall intensities over
01503 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
01504 15.00 13.60 9.07 5.27 2.63 1.35 1.10 .82 .60 mm/hr
01505 19.00 27.20 20.20 11.60 31.60 32.30 39.60 39.60 43.10 mm
01506 1980716 1980617 1980618 1980619 1980620 1980621 1980622 1980623 1980624 1980625 date
01507 *****
01508 Number of rainfall events per following interval time
01509 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
01510 124 99 96 85 77 57 49 41 31
01511 *****
01512 Number of events with at least the following durations
01513 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
01514 123 70 40 14 5 0 0 0 0
01515 *****
01516 R0885-C0003-----
01517 COMPUTE API
01518 [APIIn= 50.00: APIkdy= .9000: APIkdt= .9956]
01519 [APIOut= 52.83: APIkdy= .9000: APIkdt= .9956]
01520 *****
01521 # Pre Development Condition - Using NASHYD and CN
01522 *****
01523 R0885-C0004-----DRAIN-ID:INHVD-----AREHA-QPEARcms-TpeakDate_hh:mm-----Rvum-R.C.--DWfms
01524 CONTINUOUS NASHYD 5.0 01:InfTranPre 22.01 .719 1985.0617,23:00 121.13 216 .000
01525 [Cm 90.0: N# 3.00: Tp# .24]
01526 [IAREC=24.00: SMIN= 10.51: SMAX= 70.09: SK= .300]
01527 [InterEventTime= 12.00]
01528 R0885-C0005-----DRAIN-ID:INHVD-----AREHA-QPEARcms-TpeakDate_hh:mm-----Rvum-R.C.--DWfms
01529 CONTINUOUS NASHYD 5.0 01:InfTranPre 22.86 .498 1985.0617,23:05 111.44 199 .000
01530 [Cm 90.0: N# 3.00: Tp# .38]
01531 [IAREC=24.00: SMIN= 12.64: SMAX= 84.28: SK= .300]
01532 [InterEventTime= 12.00]
01533 *****
01534 # Pre Development Condition - Using NASHYD and CN - No INFILTRATION
01535 *****
01536 R0885-C0006-----DRAIN-ID:INHVD-----AREHA-QPEARcms-TpeakDate_hh:mm-----Rvum-R.C.--DWfms
01537 CONTINUOUS NASHYD 5.0 01:InfTranPre 22.01 1.026 1985.0716,14:00 227.04 406 .000
01538 [Cm 100.0: N# 3.00: Tp# .24]
01539 [IAREC=24.00: SMIN= .00: SMAX= .00: SK= .300]
01540 [InterEventTime= 12.00]
01541 R0885-C0007-----DRAIN-ID:INHVD-----AREHA-QPEARcms-TpeakDate_hh:mm-----Rvum-R.C.--DWfms
01542 CONTINUOUS NASHYD 5.0 01:InfTranPre 22.86 .899 1985.0617,23:00 227.04 406 .000
01543 [Cm 100.0: N# 3.00: Tp# .38]
01544 [IAREC=24.00: SMIN= .00: SMAX= .00: SK= .300]
01545 [InterEventTime= 12.00]
01546 *****
01547 # STORMS
01548 *****
01549 ** END OF RUN : 87
01550 *****
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01801 # Company : J.F. Sabourin and Associates
01802 # License # : 2549237
01803 # *****
01804 # Model developed to simulate pre-development water budget
01805 # Ottawa International Airport (1967 - 2003)
01806 # *****
01807 # *****
01808 # *****
01809 # READ A&S DATA
01810 [Filename = 6106000.123
01811 [Start_date= 1989.0101; End_date= 1989.1231]
01812 [Dw= 60.min; Length= 8040.hrs; WetHrs= 421; DryHrs= 7619; PTOV= 522.50]
01813 *****
01814 Maximum average rainfall intensities over
01815 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
01816 22.70 12.60 8.60 5.55 4.43 2.25 1.50 1.21 1.06 mm/hr
01817 1989072 1989072 1989072 1989072 1989072 1989072 1989072 1989072 1989072 date
01818 *****
01819 Number of rainfall events per following interevent time
01820 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
01821 170 153 121 94 68 55 47 33
01822 *****
01823 Number of events with at least the following durations
01824 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
01825 224 116 72 30 6 0 0 0 0
01826 *****
01827 # *****
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02161# R0993<C0007>-----DtnIn-ID:INHYD-----AREAb-QPEARcms-TpeaDate_hh:mm-----Rvum-R.C.--DWfms
02162# CONTINUOUS NASHYD -----DtnIn-ID:INHYD-----AREAb-QPEARcms-TpeaDate_hh:mm-----Rvum-R.C.--DWfms
02163# [File Name = 6106000.123 ]
02164# [Start_date = 1994.0101; End_date = 1994.1231 ]
02165# [Dry: 60 min; Length: 6576 hrs; WetHrs: 328; DryHrs: 6248; PTOF: 527.00 ]
02166# Maximum average rainfall intensities over
02167# 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02168# 22.60 11.30 8.43 5.42 3.92 2.92 2.19 1.39 0.99 0.63 mm/hr
02169# 22.60 23.80 25.30 32.50 35.00 42.50 42.50 42.50 82.60 mm/hr
02170# 1994029 1994029 1994029 1994029 1994029 1994029 1994029 1994029 1994029 date
02171# Number of rainfall events per following interval time
02172# 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02173# 131 110 86 76 60 46 37 32 23
02174# Number of events with at least the following durations
02175# 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02176# 130 70 46 12 1 0 0 0 0
02177# *****
02178# R0994<C0001>-----DtnIn-ID:INHYD-----AREAb-QPEARcms-TpeaDate_hh:mm-----Rvum-R.C.--DWfms
02179# START
02180# [ZERO = .00 hrs on 19940101]
02181# [MROUT= 2 (1=imperial, 2=metric output)]
02182# [NSTORE= 0 ]
02183# [NUN = 0094 ]
02184# *****
02185# SWMHYD Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
02186# *****
02187# Project Name : [Calvan Perth properties]
02188# Project Number : [2118]
02189# Date : [2023 JAN 26]
02190# Modeller : [J]
02191# Company : [J.F. Sabourin and Associates]
02192# License # : [2549237]
02193# *****
02194# Model developed to simulate pre-development water budget
02195# *****
02196# Ottawa International Airport (1967 - 2003)
02197# *****
02198# R0994<C0002>-----DtnIn-ID:INHYD-----AREAb-QPEARcms-TpeaDate_hh:mm-----Rvum-R.C.--DWfms
02199# READ AES DATA
02200# [File Name = 6106000.123 ]
02201# [Start_date = 1994.0101; End_date = 1994.1231 ]
02202# [Dry: 60 min; Length: 6576 hrs; WetHrs: 328; DryHrs: 6248; PTOF: 527.00 ]
02203# Maximum average rainfall intensities over
02204# 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02205# 22.60 11.30 8.43 5.42 3.92 2.92 2.19 1.39 0.99 0.63 mm/hr
02206# 22.60 23.80 25.30 32.50 35.00 42.50 42.50 42.50 82.60 mm/hr
02207# 1994029 1994029 1994029 1994029 1994029 1994029 1994029 1994029 1994029 date
02208# Number of rainfall events per following interval time
02209# 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02210# 131 110 86 76 60 46 37 32 23
02211# Number of events with at least the following durations
02212# 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02213# 130 70 46 12 1 0 0 0 0
02214# *****
02215# R0994<C0003>-----DtnIn-ID:INHYD-----AREAb-QPEARcms-TpeaDate_hh:mm-----Rvum-R.C.--DWfms
02216# COMPUTE API
02217# [APtIn= 50.00; APtIdy= 9000; APtIdk= .9956]
02218# [APtMax= 97.84; APtAvg= 19.39; APtMin= .71]
02219# *****
02220# Pre Development Condition - Using NASHYD and CN
02221# *****
02222# R0994<C0004>-----DtnIn-ID:INHYD-----AREAb-QPEARcms-TpeaDate_hh:mm-----Rvum-R.C.--DWfms
02223# CONTINUOUS NASHYD -----DtnIn-ID:INHYD-----AREAb-QPEARcms-TpeaDate_hh:mm-----Rvum-R.C.--DWfms
02224# [File Name = 6106000.123 ]
02225# [Start_date = 1994.0101; End_date = 1994.1231 ]
02226# [Dry: 60 min; Length: 6576 hrs; WetHrs: 328; DryHrs: 6248; PTOF: 527.00 ]
02227# Maximum average rainfall intensities over
02228# 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02229# 22.60 11.30 8.43 5.42 3.92 2.92 2.19 1.39 0.99 0.63 mm/hr
02230# 22.60 23.80 25.30 32.50 35.00 42.50 42.50 42.50 82.60 mm/hr
02231# 1994029 1994029 1994029 1994029 1994029 1994029 1994029 1994029 1994029 date
02232# Number of rainfall events per following interval time
02233# 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02234# 131 110 86 76 60 46 37 32 23
02235# Number of events with at least the following durations
02236# 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02237# 130 70 46 12 1 0 0 0 0
02238# *****
02239# R0994<C0005>-----DtnIn-ID:INHYD-----AREAb-QPEARcms-TpeaDate_hh:mm-----Rvum-R.C.--DWfms
02240# CONTINUOUS NASHYD -----DtnIn-ID:INHYD-----AREAb-QPEARcms-TpeaDate_hh:mm-----Rvum-R.C.--DWfms
02241# [File Name = 6106000.123 ]
02242# [Start_date = 1994.0101; End_date = 1994.1231 ]
02243# [Dry: 60 min; Length: 6576 hrs; WetHrs: 328; DryHrs: 6248; PTOF: 527.00 ]
02244# Maximum average rainfall intensities over
02245# 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02246# 22.60 11.30 8.43 5.42 3.92 2.92 2.19 1.39 0.99 0.63 mm/hr
02247# 22.60 23.80 25.30 32.50 35.00 42.50 42.50 42.50 82.60 mm/hr
02248# 1994029 1994029 1994029 1994029 1994029 1994029 1994029 1994029 1994029 date
02249# Number of rainfall events per following interval time
02250# 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02251# 131 110 86 76 60 46 37 32 23
02252# Number of events with at least the following durations
02253# 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02254# 130 70 46 12 1 0 0 0 0
02255# *****
02256# R0994<C0006>-----DtnIn-ID:INHYD-----AREAb-QPEARcms-TpeaDate_hh:mm-----Rvum-R.C.--DWfms
02257# CONTINUOUS NASHYD -----DtnIn-ID:INHYD-----AREAb-QPEARcms-TpeaDate_hh:mm-----Rvum-R.C.--DWfms
02258# [File Name = 6106000.123 ]
02259# [Start_date = 1994.0101; End_date = 1994.1231 ]
02260# [Dry: 60 min; Length: 6576 hrs; WetHrs: 328; DryHrs: 6248; PTOF: 527.00 ]
02261# Maximum average rainfall intensities over
02262# 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02263# 22.60 11.30 8.43 5.42 3.92 2.92 2.19 1.39 0.99 0.63 mm/hr
02264# 22.60 23.80 25.30 32.50 35.00 42.50 42.50 42.50 82.60 mm/hr
02265# 1994029 1994029 1994029 1994029 1994029 1994029 1994029 1994029 1994029 date
02266# Number of rainfall events per following interval time
02267# 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02268# 131 110 86 76 60 46 37 32 23
02269# Number of events with at least the following durations
02270# 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02271# 130 70 46 12 1 0 0 0 0
02272# *****
02273# R0994<C0007>-----DtnIn-ID:INHYD-----AREAb-QPEARcms-TpeaDate_hh:mm-----Rvum-R.C.--DWfms
02274# CONTINUOUS NASHYD -----DtnIn-ID:INHYD-----AREAb-QPEARcms-TpeaDate_hh:mm-----Rvum-R.C.--DWfms
02275# [File Name = 6106000.123 ]
02276# [Start_date = 1994.0101; End_date = 1994.1231 ]
02277# [Dry: 60 min; Length: 6576 hrs; WetHrs: 328; DryHrs: 6248; PTOF: 527.00 ]
02278# Maximum average rainfall intensities over
02279# 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02280# 22.60 11.30 8.43 5.42 3.92 2.92 2.19 1.39 0.99 0.63 mm/hr
02281# 22.60 23.80 25.30 32.50 35.00 42.50 42.50 42.50 82.60 mm/hr
02282# 1994029 1994029 1994029 1994029 1994029 1994029 1994029 1994029 1994029 date
02283# Number of rainfall events per following interval time
02284# 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02285# 131 110 86 76 60 46 37 32 23
02286# Number of events with at least the following durations
02287# 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02288# 130 70 46 12 1 0 0 0 0
02289# *****
02290# R0994<C0008>-----DtnIn-ID:INHYD-----AREAb-QPEARcms-TpeaDate_hh:mm-----Rvum-R.C.--DWfms
02291# CONTINUOUS NASHYD -----DtnIn-ID:INHYD-----AREAb-QPEARcms-TpeaDate_hh:mm-----Rvum-R.C.--DWfms
02292# [File Name = 6106000.123 ]
02293# [Start_date = 1994.0101; End_date = 1994.1231 ]
02294# [Dry: 60 min; Length: 6576 hrs; WetHrs: 328; DryHrs: 6248; PTOF: 527.00 ]
02295# Maximum average rainfall intensities over
02296# 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02297# 22.60 11.30 8.43 5.42 3.92 2.92 2.19 1.39 0.99 0.63 mm/hr
02298# 22.60 23.80 25.30 32.50 35.00 42.50 42.50 42.50 82.60 mm/hr
02299# 1994029 1994029 1994029 1994029 1994029 1994029 1994029 1994029 1994029 date
02300# Number of rainfall events per following interval time
02301# 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02302# 131 110 86 76 60 46 37 32 23
02303# Number of events with at least the following durations
02304# 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02305# 130 70 46 12 1 0 0 0 0
02306# *****
02307# R0994<C0009>-----DtnIn-ID:INHYD-----AREAb-QPEARcms-TpeaDate_hh:mm-----Rvum-R.C.--DWfms
02308# CONTINUOUS NASHYD -----DtnIn-ID:INHYD-----AREAb-QPEARcms-TpeaDate_hh:mm-----Rvum-R.C.--DWfms
02309# [File Name = 6106000.123 ]
02310# [Start_date = 1994.0101; End_date = 1994.1231 ]
02311# [Dry: 60 min; Length: 6576 hrs; WetHrs: 328; DryHrs: 6248; PTOF: 527.00 ]
02312# Maximum average rainfall intensities over
02313# 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02314# 22.60 11.30 8.43 5.42 3.92 2.92 2.19 1.39 0.99 0.63 mm/hr
02315# 22.60 23.80 25.30 32.50 35.00 42.50 42.50 42.50 82.60 mm/hr
02316# 1994029 1994029 1994029 1994029 1994029 1994029 1994029 1994029 1994029 date
02317# Number of rainfall events per following interval time
02318# 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02319# 131 110 86 76 60 46 37 32 23
02320# Number of events with at least the following durations
02321# 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02322# 130 70 46 12 1 0 0 0 0
02323# *****
02324# R0994<C0010>-----DtnIn-ID:INHYD-----AREAb-QPEARcms-TpeaDate_hh:mm-----Rvum-R.C.--DWfms
02325# CONTINUOUS NASHYD -----DtnIn-ID:INHYD-----AREAb-QPEARcms-TpeaDate_hh:mm-----Rvum-R.C.--DWfms
02326# [File Name = 6106000.123 ]
02327# [Start_date = 1994.0101; End_date = 1994.1231 ]
02328# [Dry: 60 min; Length: 6576 hrs; WetHrs: 328; DryHrs: 6248; PTOF: 527.00 ]
02329# Maximum average rainfall intensities over
02330# 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02331# 22.60 11.30 8.43 5.42 3.92 2.92 2.19 1.39 0.99 0.63 mm/hr
02332# 22.60 23.80 25.30 32.50 35.00 42.50 42.50 42.50 82.60 mm/hr
02333# 1994029 1994029 1994029 1994029 1994029 1994029 1994029 1994029 1994029 date
02334# Number of rainfall events per following interval time
02335# 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02336# 131 110 86 76 60 46 37 32 23
02337# Number of events with at least the following durations
02338# 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02339# 130 70 46 12 1 0 0 0 0
02340# *****

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02341# SWMHYD Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
02342# *****
02343# Project Name : [Calvan Perth properties]
02344# Project Number : [2118]
02345# Date : [2023 JAN 26]
02346# Modeller : [J]
02347# Company : [J.F. Sabourin and Associates]
02348# License # : [2549237]
02349# *****
02350# Model developed to simulate pre-development water budget
02351# *****
02352# Ottawa International Airport (1967 - 2003)
02353# *****
02354# R0996<C0002>-----DtnIn-ID:INHYD-----AREAb-QPEARcms-TpeaDate_hh:mm-----Rvum-R.C.--DWfms
02355# READ AES DATA
02356# [File Name = 6106000.123 ]
02357# [Start_date = 1994.0101; End_date = 1994.1231 ]
02358# [Dry: 60 min; Length: 6552 hrs; WetHrs: 387; DryHrs: 6165; PTOF: 512.20 ]
02359# Maximum average rainfall intensities over
02360# 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02361# 18.50 13.55 9.03 5.42 3.93 2.93 2.19 1.32 0.92 0.70 mm/hr
02362# 18.50 21.10 23.10 29.50 32.10 44.10 47.50 49.00 80.30 mm/hr
02363# 19960731 19960731 19960731 19960731 19961109 19961109 19961109 19961109 19961109 date
02364# Number of rainfall events per following interval time
02365# 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02366# 132 104 93 71 59 43 36 31 24
02367# Number of events with at least the following durations
02368# 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02369# 131 72 50 19 12 2 1 0 0 0
02370# *****
02371# R0996<C0003>-----DtnIn-ID:INHYD-----AREAb-QPEARcms-TpeaDate_hh:mm-----Rvum-R.C.--DWfms
02372# COMPUTE API
02373# [APtIn= 50.00; APtIdy= 9000; APtIdk= .9956]
02374# [APtMax= 63.22; APtAvg= 19.39; APtMin= .71]
02375# *****
02376# Pre Development Condition - Using NASHYD and CN
02377# *****
02378# R0996<C0004>-----DtnIn-ID:INHYD-----AREAb-QPEARcms-TpeaDate_hh:mm-----Rvum-R.C.--DWfms
02379# CONTINUOUS NASHYD -----DtnIn-ID:INHYD-----AREAb-QPEARcms-TpeaDate_hh:mm-----Rvum-R.C.--DWfms
02380# [File Name = 6106000.123 ]
02381# [Start_date = 1994.0101; End_date = 1994.1231 ]
02382# [Dry: 60 min; Length: 6552 hrs; WetHrs: 387; DryHrs: 6165; PTOF: 512.20 ]
02383# Maximum average rainfall intensities over
02384# 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02385# 18.50 13.55 9.03 5.42 3.93 2.93 2.19 1.32 0.92 0.70 mm/hr
02386# 18.50 21.10 23.10 29.50 32.10 44.10 47.50 49.00 80.30 mm/hr
02387# 19960731 19960731 19960731 19960731 19961109 19961109 19961109 19961109 19961109 date
02388# Number of rainfall events per following interval time
02389# 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02390# 132 104 93 71 59 43 36 31 24
02391# Number of events with at least the following durations
02392# 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02393# 131 72 50 19 12 2 1 0 0 0
02394# *****
02395# R0996<C0005>-----DtnIn-ID:INHYD-----AREAb-QPEARcms-TpeaDate_hh:mm-----Rvum-R.C.--DWfms
02396# CONTINUOUS NASHYD -----DtnIn-ID:INHYD-----AREAb-QPEARcms-TpeaDate_hh:mm-----Rvum-R.C.--DWfms
02397# [File Name = 6106000.123 ]
02398# [Start_date = 1994.0101; End_date = 1994.1231 ]
02399# [Dry: 60 min; Length: 6552 hrs; WetHrs: 387; DryHrs: 6165; PTOF: 512.20 ]
02400# Maximum average rainfall intensities over
02401# 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02402# 18.50 13.55 9.03 5.42 3.93 2.93 2.19 1.32 0.92 0.70 mm/hr
02403# 18.50 21.10 23.10 29.50 32.10 44.10 47.50 49.00 80.30 mm/hr
02404# 19960731 19960731 19960731 19960731 19961109 19961109 19961109 19961109 19961109 date
02405# Number of rainfall events per following interval time
02406# 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02407# 132 104 93 71 59 43 36 31 24
02408# Number of events with at least the following durations
02409# 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02410# 131 72 50 19 12 2 1 0 0 0
02411# *****
02412# R0997<C0000>-----DtnIn-ID:INHYD-----AREAb-QPEARcms-TpeaDate_hh:mm-----Rvum-R.C.--DWfms
02413# START
02414# [ZERO = .00 hrs on 19970101]
02415# [MROUT= 2 (1=imperial, 2=metric output)]
02416# [NSTORE= 0 ]
02417# [NUN = 0094 ]
02418# *****
02419# SWMHYD Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
02420# *****
02421# Project Name : [Calvan Perth properties]
02422# Project Number : [2118]
02423# Date : [2023 JAN 26]
02424# Modeller : [J]
02425# Company : [J.F. Sabourin and Associates]
02426# License # : [2549237]
02427# *****
02428# Model developed to simulate pre-development water budget
02429# *****
02430# Ottawa International Airport (1967 - 2003)
02431# *****
02432# R0997<C0001>-----DtnIn-ID:INHYD-----AREAb-QPEARcms-TpeaDate_hh:mm-----Rvum-R.C.--DWfms
02433# READ AES DATA
02434# [File Name = 6106000.123 ]
02435# [Start_date = 1997.0101; End_date = 1997.1231 ]
02436# [Dry: 60 min; Length: 8040 hrs; WetHrs: 379; DryHrs: 7661; PTOF: 433.20 ]
02437# Maximum average rainfall intensities over
02438# 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02439# 12.50 7.60 5.67 4.43 3.91 2.91 2.18 1.12 .84 .63 mm/hr
02440# 12.50 15.20 17.00 26.60 34.30 40.40 40.40 40.40 45.30 mm/hr
02441# 19970622 19970622 19970622 19970622 19970622 19970622 19970622 19970622 19970622 date
02442# Number of rainfall events per following interval time
02443# 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02444# 113 82 83 67 61 55 48 43 30
02445# Number of events with at least the following durations
02446# 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02447# 112 62 4 0 0 0 0 0 0
02448# *****
02449# R0997<C0002>-----DtnIn-ID:INHYD-----AREAb-QPEARcms-TpeaDate_hh:mm-----Rvum-R.C.--DWfms
02450# COMPUTE API
02451# [APtIn= 50.00; APtIdy= 9000; APtIdk= .9956]
02452# [APtMax= 50.00; APtAvg= 13.66; APtMin= .27]
02453# *****
02454# Pre Development Condition - Using NASHYD and CN
02455# *****
02456# R0997<C0003>-----DtnIn-ID:INHYD-----AREAb-QPEARcms-TpeaDate_hh:mm-----Rvum-R.C.--DWfms
02457# CONTINUOUS NASHYD -----DtnIn-ID:INHYD-----AREAb-QPEARcms-TpeaDate_hh:mm-----Rvum-R.C.--DWfms
02458# [File Name = 6106000.123 ]
02459# [Start_date = 1997.0101; End_date = 1997.1231 ]
02460# [Dry: 60 min; Length: 8040 hrs; WetHrs: 379; DryHrs: 7661; PTOF: 433.20 ]
02461# Maximum average rainfall intensities over
02462# 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02463# 12.50 7.60 5.67 4.43 3.91 2.91 2.18 1.12 .84 .63 mm/hr
02464# 12.50 15.20 17.00 26.60 34.30 40.40 40.40 40.40 45.30 mm/hr
02465# 19970622 19970622 19970622 19970622 19970622 19970622 19970622 19970622 19970622 date
02466# Number of rainfall events per following interval time
02467# 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02468# 113 82 83 67 61 55 48 43 30
02469# Number of events with at least the following durations
02470# 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02471# 112 62 4 0 0 0 0 0 0
02472# *****
02473# R0997<C0004>-----DtnIn-ID:INHYD-----AREAb-QPEARcms-TpeaDate_hh:mm-----Rvum-R.C.--DWfms
02474# CONTINUOUS NASHYD -----DtnIn-ID:INHYD-----AREAb-QPEARcms-TpeaDate_hh:mm-----Rvum-R.C.--DWfms
02475# [File Name = 6106000.123 ]
02476# [Start_date = 1997.0101; End_date = 1997.1231 ]
02477# [Dry: 60 min; Length: 8040 hrs; WetHrs: 379; DryHrs: 7661; PTOF: 433.20 ]
02478# Maximum average rainfall intensities over
02479# 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02480# 12.50 7.60 5.67 4.43 3.91 2.91 2.18 1.12 .84 .63 mm/hr
02481# 12.50 15.20 17.00 26.60 34.30 40.40 40.40 40.40 45.30 mm/hr
02482# 19970622 19970622 19970622 19970622 19970622 19970622 19970622 19970622 19970622 date
02483# Number of rainfall events per following interval time
02484# 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02485# 113 82 83 67 61 55 48 43 30
02486# Number of events with at least the following durations
02487# 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02488# 112 62 4 0 0 0 0 0 0
02489# *****
02490# R0998<C0001>-----DtnIn-ID:INHYD-----AREAb-QPEARcms-TpeaDate_hh:mm-----Rvum-R.C.--DWfms
02491# START
02492# [ZERO = .00 hrs on 19980101]
02493# [MROUT= 2 (1=imperial, 2=metric output)]
02494# [NSTORE= 0 ]
02495# [NUN = 0094 ]
02496# *****
02497# SWMHYD Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
02498# *****
02499# Project Name : [Calvan Perth properties]
02500# Project Number : [2118]
02501# Date : [2023 JAN 26]
02502# Modeller : [J]
02503# Company : [J.F. Sabourin and Associates]
02504# License # : [2549237]
02505# *****
02506# Model developed to simulate pre-development water budget
02507# *****
02508# Ottawa International Airport (1967 - 2003)
02509# *****
02510# R0998<C0002>-----DtnIn-ID:INHYD-----AREAb-QPEARcms-TpeaDate_hh:mm-----Rvum-R.C.--DWfms
02511# READ AES DATA
02512# [File Name = 6106000.123 ]
02513# [Start_date = 1998.0101; End_date = 1998.1231 ]
02514# [Dry: 60 min; Length: 5088 hrs; WetHrs: 291; DryHrs: 4797; PTOF: 440.30 ]
02515# Maximum average rainfall intensities over
02516# 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02517# 15.80 11.80 9.60 6.60 4.00 2.54 1.92 1.27 .95 .76 mm/hr
02518# 15.80 17.80 22.80 24.00 30.50 43.60 45.80 45.80 54.60 mm/hr
02519# 19980716 19980716 19980716 19980716 19980716 19980716 19980716 19980716 19980716 date
02520# Number of rainfall events per following interval time

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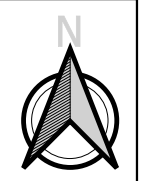
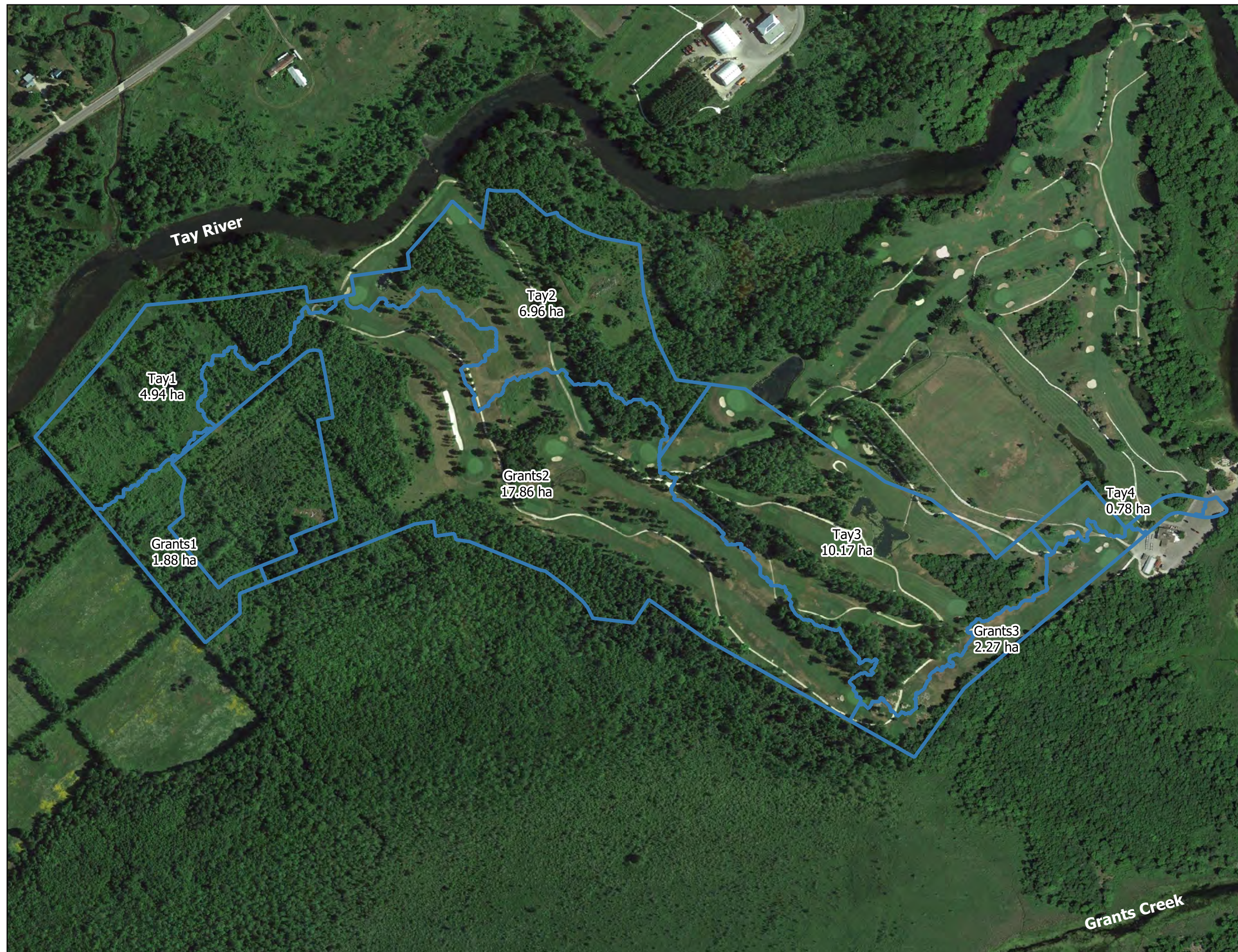
02521 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02522 1.26 1.04 0.82 0.62 0.42 0.27 0.21 0.15 0.11
02523 Number of events with at least the following durations
02524 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02525 1.26 1.04 0.82 0.62 0.42 0.27 0.21 0.15 0.11
02526 R0098:CO0003-----
02527 *****
02528 [APIIn= 50.00; APIkdy= 9000; APIkdt= 1995]
02529 [APIMax= 57.22; APIAvg= 21.28; APImin= 1.60]
02530 *****
02531 # Pre Development Condition - Using NASHYD and CN
02532 *****
02533 R0098:CO0004-----
02534 *****
02535 [CM= 92.0; N= 3.00; Tp= .24]
02536 [IAR=24.00; SMIN= 10.51; SMAX= 70.09; SK= .300]
02537 [InterEventTime= 12.00]
02538 R0098:CO0005-----
02539 *****
02540 [CM= 92.0; N= 3.00; Tp= .24]
02541 [IAR=24.00; SMIN= 12.64; SMAX= 84.28; SK= .300]
02542 *****
02543 *****
02544 # Pre Development Condition - Using NASHYD and CN - No INFILTRATION
02545 *****
02546 R0098:CO0006-----
02547 *****
02548 [CM=100.0; N= 3.00; Tp= .24]
02549 [IAR=24.00; SMIN= .00; SMAX= .00; SK= .300]
02550 [InterEventTime= 12.00]
02551 R0098:CO0007-----
02552 *****
02553 [CM=100.0; N= 3.00; Tp= .38]
02554 [IAR=24.00; SMIN= .00; SK= .300]
02555 [InterEventTime= 12.00]
02556 *****
02557 # STORMS
02558 *****
02559 ** END OF RUN : 98
02560 *****
02561 *****
02562 *****
02563 *****
02564 *****
02565 *****
02566 *****
02567 R0099:CO0001-----
02568 *****
02569 START
02570 [TZERO = .00 hrs on 20000101]
02571 [MRTYPE= 2 (1=Imperial, 2=metric output)]
02572 [MRTIME= 0]
02573 [NIN= 0099]
02574 *****
02575 # SWHYMO Ver:5.02/Jan 2001 <BETA> INPUT DATA FILE
02576 *****
02577 # Project Name : [Caivan Perth properties]
02578 # Project Number : [2118]
02579 # Date : [2023 JAN 26]
02580 # Modeller : [JB]
02581 # Company : [J.F. Sabourin and Associates]
02582 # License # : [2549237]
02583 *****
02584 # Model developed to simulate pre-development water budget
02585 # Ottawa International Airport (1967 - 2003)
02586 R0099:CO0002-----
02587 *****
02588 *****
02589 * READ AER DATA
02590 [Filename = 6106000.123 ]
02591 [Start_date= 1999.0101; End_date= 1999.1231]
02592 [DTP= 60.min; Length= 4440.hrs; WetHrs= 247; DryHrs= 4193; PTOT= 424.40]
02593 *****
02594 Maximum average rainfall intensities over
02595 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02596 17.50 12.10 9.03 6.57 4.31 1.65 1.45 1.22 .87 mm/hr
02597 17.50 20.20 27.10 39.40 39.70 39.70 52.20 56.60 69.50 mm
02598 19990717 19990717 19990906 19990906 19990908 19990908 19990908 19990908 19990908 date
02599 *****
02600 Number of rainfall events per following interval time
02601 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02602 102 80 70 63 56 39 31 28 18
02603 *****
02604 # Pre Development Condition - Using NASHYD and CN
02605 *****
02606 R0099:CO0003-----
02607 *****
02608 [APIIn= 50.00; APIkdy= 9000; APIkdt= 1995]
02609 [APIMax= 69.51; APIAvg= 23.97; APImin= 2.13]
02610 *****
02611 # Pre Development Condition - Using NASHYD and CN
02612 *****
02613 R0099:CO0004-----
02614 *****
02615 [CM= 92.0; N= 3.00; Tp= .24]
02616 [IAR=24.00; SMIN= 10.51; SMAX= 70.09; SK= .300]
02617 [InterEventTime= 12.00]
02618 R0099:CO0005-----
02619 *****
02620 [CM= 92.0; N= 3.00; Tp= .38]
02621 [IAR=24.00; SMIN= 12.64; SMAX= 84.28; SK= .300]
02622 [InterEventTime= 12.00]
02623 *****
02624 # Pre Development Condition - Using NASHYD and CN - No INFILTRATION
02625 *****
02626 R0099:CO0006-----
02627 *****
02628 [CM=100.0; N= 3.00; Tp= .24]
02629 [IAR=24.00; SMIN= .00; SMAX= .00; SK= .300]
02630 [InterEventTime= 12.00]
02631 R0099:CO0007-----
02632 *****
02633 [CM=100.0; N= 3.00; Tp= .38]
02634 [IAR=24.00; SMIN= .00; SK= .300]
02635 [InterEventTime= 12.00]
02636 *****
02637 # STORMS
02638 *****
02639 ** END OF RUN : 99
02640 *****
02641 *****
02642 *****
02643 *****
02644 *****
02645 *****
02646 *****
02647 R0100:CO0001-----
02648 *****
02649 START
02650 [TZERO = .00 hrs on 20000101]
02651 [MRTYPE= 2 (1=Imperial, 2=metric output)]
02652 [MRTIME= 0]
02653 [NIN= 0100]
02654 *****
02655 # SWHYMO Ver:5.02/Jan 2001 <BETA> INPUT DATA FILE
02656 *****
02657 # Project Name : [Caivan Perth properties]
02658 # Project Number : [2118]
02659 # Date : [2023 JAN 26]
02660 # Modeller : [JB]
02661 # Company : [J.F. Sabourin and Associates]
02662 # License # : [2549237]
02663 *****
02664 # Model developed to simulate pre-development water budget
02665 # Ottawa International Airport (1967 - 2003)
02666 R0100:CO0002-----
02667 *****
02668 *****
02669 * READ AER DATA
02670 [Filename = 6106000.123 ]
02671 [Start_date= 2000.0101; End_date= 2000.1231]
02672 [DTP= 60.min; Length= 4440.hrs; WetHrs= 406; DryHrs= 4034; PTOT= 554.60]
02673 *****
02674 Maximum average rainfall intensities over
02675 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02676 14.70 9.60 8.03 6.43 3.89 1.95 1.30 1.03 .84 mm/hr
02677 14.70 19.20 24.10 38.60 46.70 46.70 46.80 49.30 60.40 mm
02678 20000625 20000625 20000625 20000625 20000626 20000626 20000626 20000626 20000627 date
02679 *****
02680 Number of rainfall events per following interval time
02681 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02682 156 125 110 86 67 46 34 30 23
02683 *****
02684 # Pre Development Condition - Using NASHYD and CN - No INFILTRATION
02685 *****
02686 R0100:CO0003-----
02687 *****
02688 [CM= 92.0; N= 3.00; Tp= .24]
02689 [IAR=24.00; SMIN= 10.51; SMAX= 70.09; SK= .300]
02690 [InterEventTime= 12.00]
02691 R0100:CO0004-----
02692 *****
02693 [CM= 92.0; N= 3.00; Tp= .38]
02694 [IAR=24.00; SMIN= 12.64; SMAX= 84.28; SK= .300]
02695 [InterEventTime= 12.00]
02696 *****
02697 # STORMS
02698 *****
02699 ** END OF RUN : 100
02700 *****
02701 *****
02702 *****
02703 *****
02704 *****
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02709 *****
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```

02881 *** WARNING: Missing rainfall increments were set to 0.
02882 *** WARNING: Requested start date is less than start date in file.
02883 *** WARNING: Missing rainfall increments were set to 0.
02884 *** WARNING: Missing rainfall increments were set to 0.
02885 *** WARNING: Missing rainfall increments were set to 0.
02886 *** WARNING: Missing rainfall increments were set to 0.
02887 *** WARNING: Missing rainfall increments were set to 0.
02888 *** WARNING: Missing rainfall increments were set to 0.
02889 *** WARNING: Missing rainfall increments were set to 0.
02890 *** WARNING: Requested start date is less than start date in file.
02891 *** WARNING: Missing rainfall increments were set to 0.
02892 *** WARNING: Missing rainfall increments were set to 0.
02893 *** WARNING: Missing rainfall increments were set to 0.
02894 *** WARNING: Missing rainfall increments were set to 0.
02895 *** WARNING: Missing rainfall increments were set to 0.
02896 *** WARNING: Missing rainfall increments were set to 0.
02897 *** WARNING: Missing rainfall increments were set to 0.
02898 *** WARNING: Missing rainfall increments were set to 0.
02899 *** WARNING: Missing rainfall increments were set to 0.
02900 *** WARNING: Missing rainfall increments were set to 0.
02901 *** WARNING: Requested start date is less than start date in file.
02902 *** WARNING: Missing rainfall increments were set to 0.
02903 *** WARNING: Missing rainfall increments were set to 0.
02904 *** WARNING: Missing rainfall increments were set to 0.
02905 *** WARNING: Requested start date is less than start date in file.
02906 *** WARNING: Missing rainfall increments were set to 0.
02907 *** WARNING: Missing rainfall increments were set to 0.
02908 *** WARNING: Missing rainfall increments were set to 0.
02909 *** WARNING: Missing rainfall increments were set to 0.
02910 *** WARNING: Missing rainfall increments were set to 0.
02911 *** WARNING: Missing rainfall increments were set to 0.
02912 *** WARNING: Requested start date is less than start date in file.
02913 *** WARNING: Missing rainfall increments were set to 0.
02914 *** WARNING: Missing rainfall increments were set to 0.
02915 *** WARNING: Requested start date is less than start date in file.
02916 *** WARNING: Missing rainfall increments were set to 0.
02917 *** WARNING: Requested start date is less than start date in file.
02918 *** WARNING: Missing rainfall increments were set to 0.
02919 *** WARNING: Requested start date is less than start date in file.
02920 *** WARNING: Missing rainfall increments were set to 0.
02921 *** WARNING: Requested start date is less than start date in file.
02922 *** WARNING: Missing rainfall increments were set to 0.
02923 *** WARNING: Requested start date is less than start date in file.
02924 *** WARNING: Specified end date is beyond the end date in file.
02925 *** WARNING: Missing rainfall increments were set to 0.
02926 Simulation ended on 2023-02-14 at 17:44:01
02927 *****
02928

Appendix E

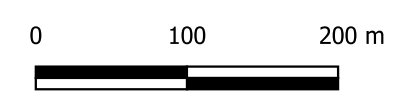
Preliminary SWM Pond Sizing



Legend

- Drainage Area
[Name]
[Area]

SCALE: 1:5000



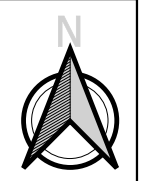
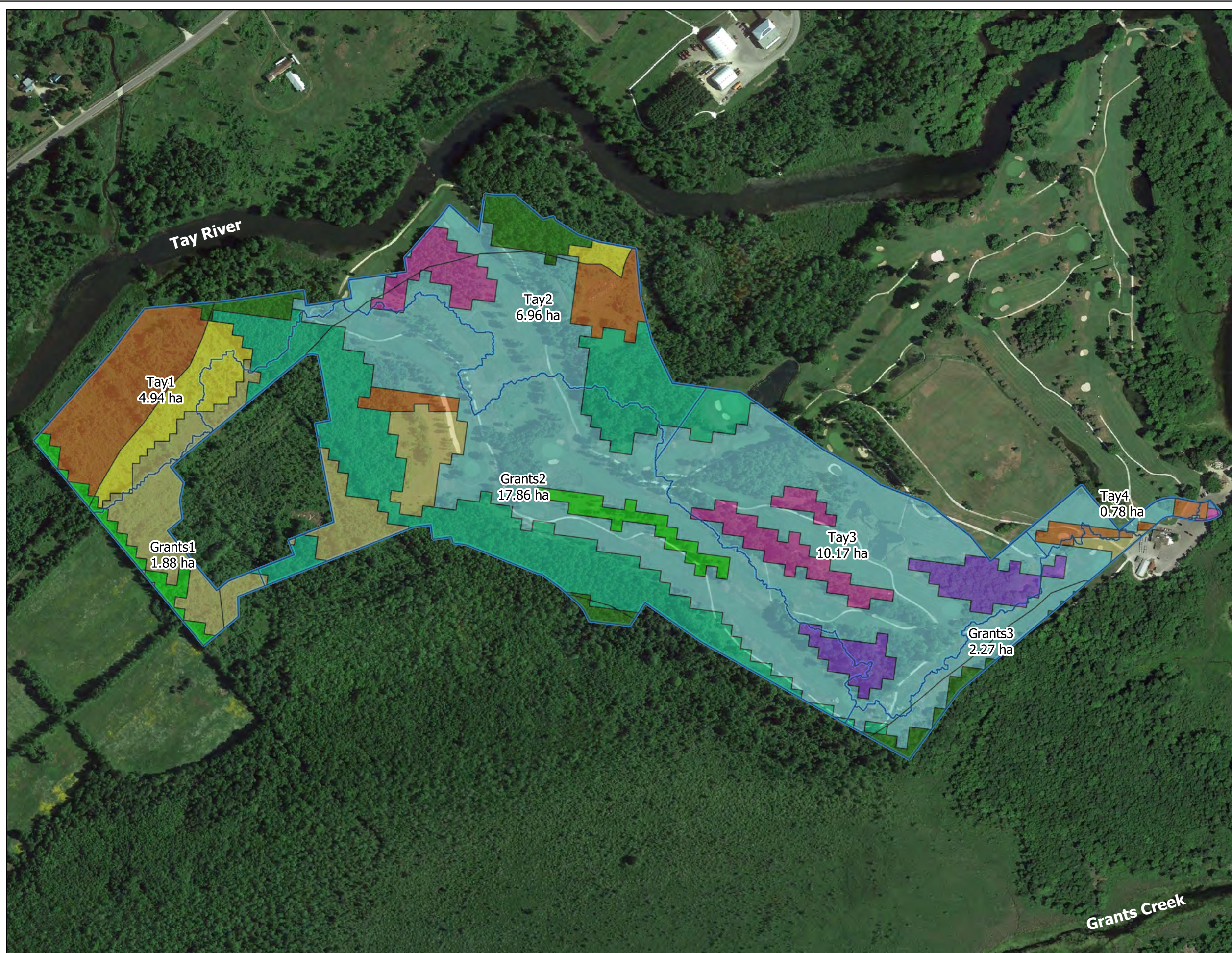
J.F. Sabourin and Associates Inc.
 WATER RESOURCES AND ENVIRONMENTAL CONSULTANTS
 52 Springbrook Drive (613) 836-3884
 Ottawa, ON, K2S 1B9 www.jfsa.com

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Figure E1: Pre-Development Drainage Area

PROJECT	2118-21
DRAWN	BT
DATE	February 2023



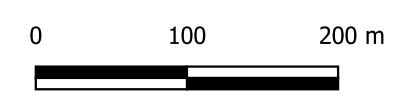
Legend

Drainage Area
[Name]
[Area]

Land Use

- Built Up Area - Pervious
- Deciduous Forest
- Fallow
- Forest
- Hedge Rows
- Mixed Forest
- Plantation
- Tilled
- Transportation
- Treed Swamp

SCALE: 1:5000



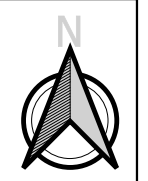
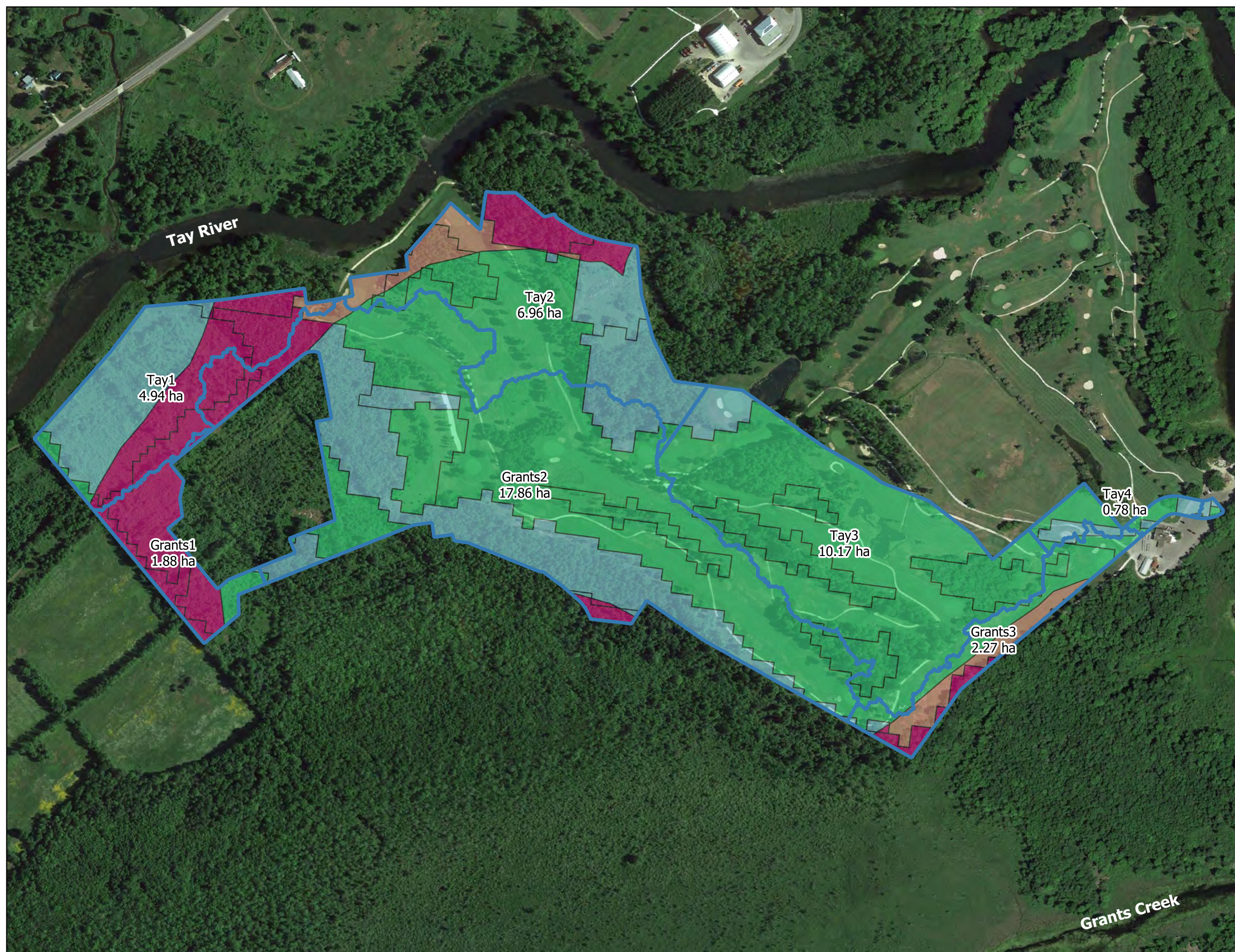
J.F. Sabourin and Associates Inc.
WATER RESOURCES AND ENVIRONMENTAL CONSULTANTS
52 Springbrook Drive
Ottawa, ON, K2S 1B9
(613) 836-3884
www.jfsa.com

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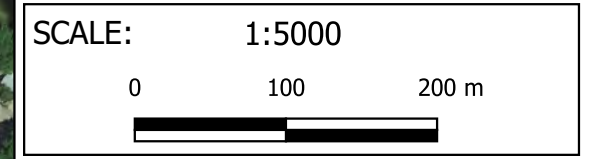
Figure E2: Pre-Development Land Use

PROJECT	2118-21
DRAWN	BT
DATE	February 2023



Legend

- Drainage Area
[Name]
[Area]
- Soil Types
- Monteagle (SCS Type B)
- Monteagle Sandy Loam (SCS Type B)
- Muck (SCS Type D)
- North Gower (SCS Type D)
- Water (N)



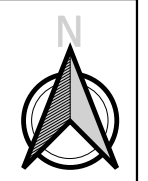
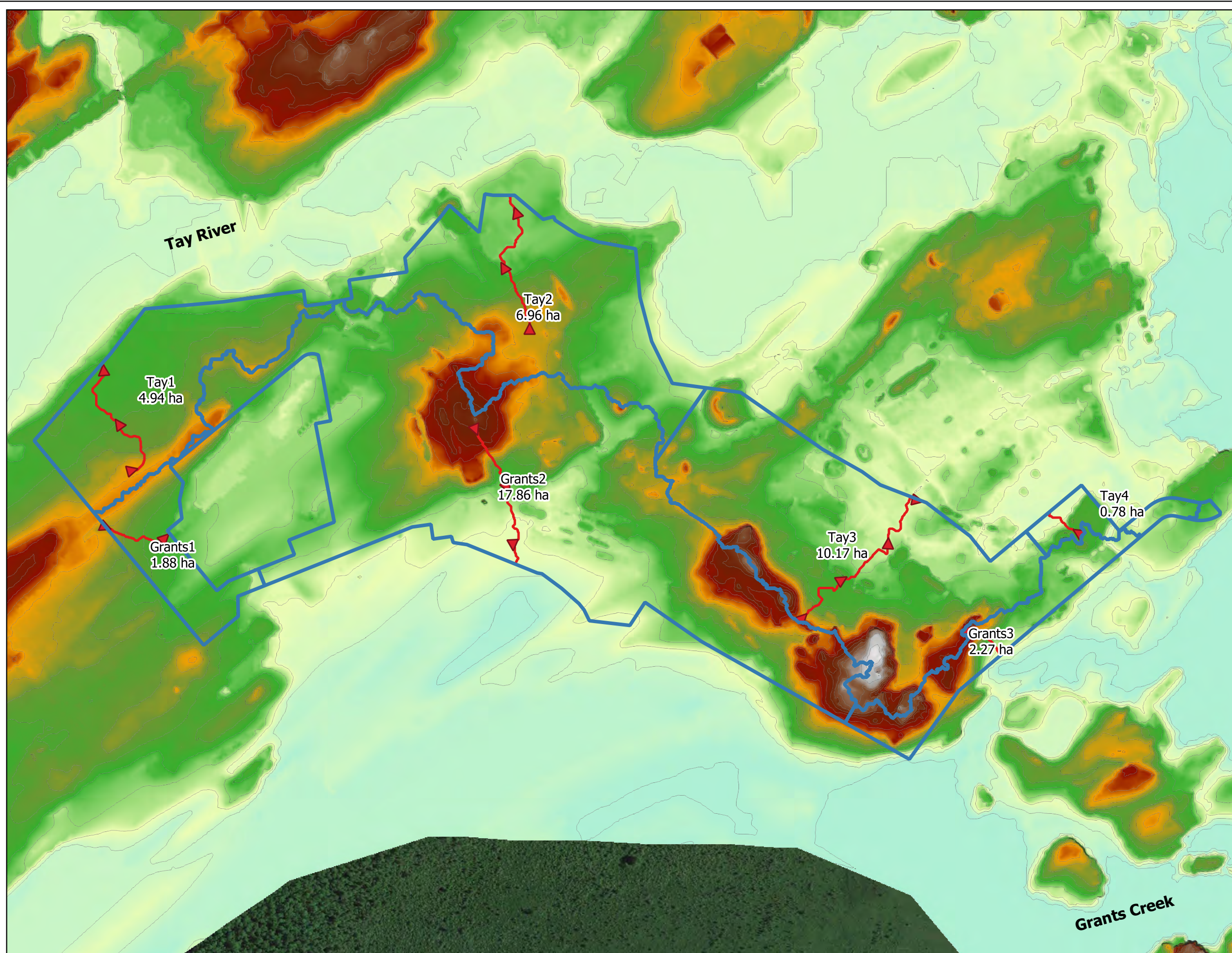
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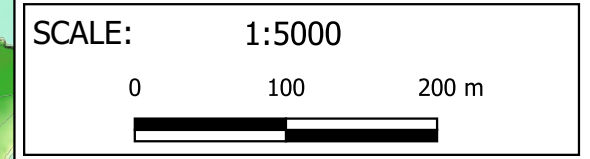
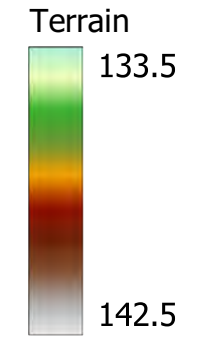
Figure E3: Pre-Development Soils

PROJECT	2118-21
DRAWN	BT
DATE	February 2023



Legend

- Drainage Area
[Name]
[Ares]
- ▶ Flow Lengths



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Figure E4: Pre-Development Flow Paths

PROJECT	2118-21
DRAWN	BT
DATE	February 2023

Table E1: Calculation of SCS Curve Number (CN)

Tay River

Area (ha)	Land Type	Soil Name	Soil		CN	% of Catchment	Weighted CN
			Condition	Soil Group			
0.608	Built Up Area - Pervious	NORTH GOWER	D	Fair	84	2.7%	2.2
0.407	Plantation	MUCK	D	Fair	79	1.8%	1.4
0.138	Hedge Rows	MONTEAGLE	B	Fair	56	0.6%	0.3
1.266	Fallow	MUCK	D	Fair	94	5.5%	5.2
0.023	Hedge Rows	MUCK	D	Fair	77	0.1%	0.1
0.468	Deciduous Forest	MUCK	D	Fair	79	2.0%	1.6
0.056	Treed Swamp	MONTEAGLE SANDY LOAM	B	Fair	50	0.2%	0.1
3.558	Tilled	MONTEAGLE SANDY LOAM	B	Fair	78	15.6%	12.1
0.943	Treed Swamp	MUCK	D	Fair	50	4.1%	2.1
1.626	Forest	MONTEAGLE	B	Fair	60	7.1%	4.3
0.344	Forest	NORTH GOWER	D	Fair	79	1.5%	1.2
1.640	Deciduous Forest	MONTEAGLE SANDY LOAM	B	Fair	60	7.2%	4.3
10.611	Built Up Area - Pervious	MONTEAGLE	B	Fair	69	46.4%	32.0
1.143	Mixed Forest	MONTEAGLE	B	Fair	60	5.0%	3.0
0.025	Plantation	MONTEAGLE	B	Fair	60	0.1%	0.1
						CN	70

Grants Creek

Area (ha)	Land Type	Soil Name	Soil		CN	% of Catchment	Weighted CN
			Condition	Soil Group			
1.550	Plantation	MUCK	D	Fair	79	7.0%	5.6
2.093	Plantation	MONTEAGLE	B	Fair	60	9.5%	5.7
0.322	Fallow	MUCK	D	Fair	94	1.5%	1.4
0.354	Hedge Rows	MUCK	D	Fair	77	1.6%	1.2
5.266	Deciduous Forest	MONTEAGLE SANDY LOAM	B	Fair	60	23.9%	14.4
0.041	Forest	MONTEAGLE	B	Fair	60	0.2%	0.1
0.781	Built Up Area - Pervious	NORTH GOWER	D	Fair	84	3.5%	3.0
0.341	Mixed Forest	MONTEAGLE	B	Fair	60	1.5%	0.9
0.631	Hedge Rows	MONTEAGLE	B	Fair	56	2.9%	1.6
0.375	Deciduous Forest	MUCK	D	Fair	79	1.7%	1.3
0.032	Treed Swamp	MONTEAGLE SANDY LOAM	B	Fair	50	0.1%	0.1
0.384	Tilled	MONTEAGLE SANDY LOAM	B	Fair	78	1.7%	1.4
9.425	Built Up Area - Pervious	MONTEAGLE	B	Fair	69	42.8%	29.5
0.403	Treed Swamp	MUCK	D	Fair	50	1.8%	0.9
0.002	Forest	WATER	N	Fair	98	0.0%	0.0
0.008	Transportation	MONTEAGLE SANDY LOAM	B	Fair	98	0.0%	0.0
						CN	67

Table E2: Time to Peak Calculations

Parameter	Units	Grants	Tay
Area	ha	22.01	22.86
CN	-	67	70
Ptotal to calc C from CN, use 2 yr 3 hr Chicago stom	P(mm)	31.9	31.9
	la(mm)	5.00	5.00
	RV(mm)	4.75	5.3
Ptotal to calc C from CN, use 2 yr 24 hr SCS stom	P(mm)	48.46	48.46
	RV(mm)	11.2	12.4
C (From Chicago storm)	-	0.149	0.167
C (From SCS storm)	-	0.231	0.256
Length of Channel	m	231	304
	ft	758	996
Elevation of Head Water	m	139.35	139.46
	ft	457	458
Elevation of Outlet	m	134.30	135.42
	ft	441	444
Average Slope	m/m	2.18%	1.33%
	ft/ft	2.18%	1.33%
Kirpich			
Time of Concentration	mins	6	8
Time to Peak	min	4	6
Time to Peak	Hours	0.06	0.09
FAA (From Chicago storm)			
Time of Concentration	mins	36	48
Time to Peak	mins	24	32
Time to Peak	Hours	0.40	0.54
FAA (From SCS storm)			
Time of Concentration	mins	33	44
Time to Peak	mins	22	29
Time to Peak	Hours	0.37	0.48
Barnsby Williams			
Time of Concentration	mins	8	12
Time to Peak	mins	6	8
Time to Peak	Hours	0.09	0.13
SCS			
Time of Concentration	mins	25	37
Time to Peak	mins	17	24
Time to Peak	Hours	0.28	0.41
Selected Method			
FAA (From SCS storm)			
Time to Peak	min	22	29
Time to Peak	Hours	0.37	0.48

Note:

All methods calculated as per Appendix A of the SWMHYMO manual

Time to Peak calculated as 2/3 Time of concentration

```

1  20    Metric units / ID numbers OFF
2  *#*****
   *****
3  *#  SWMHYMO  /  INPUT DATA FILE
4  *#*****
   *****
5  *#  Project Name  : [Caivan Perth properties]
6  *#  Project Number: [2118]
7  *#  Date          : [2023 JAN 26]
8  *#  Modeller     : [JB]
9  *#  Company      : J.F. Sabourin and Associates
10 *#  License #    : 2549237
11 *#*****
   *****
12 *# Model developed to simulate runoff from subcatchments under pre development conditions
13 *#*****
   *****
14 START          TZERO=[0.0],  METOUT=[2],  NSTORM=[1],  NRUN=[001]
15 [ "25MMC3H.stm" ] <--storm filename, one per line for NSTORM time
16 *%-----|-----|
17 READ STORM    STORM_FILENAME=[ "STORM.001" ]
18 *%-----|-----|
19 *#*****
   *****
20 *# Grants Creek
21 *#*****
   *****
22 CALIB NASHYD   NHYD=[ "Grants" ], DT=[1]min, AREA=[22.01](ha),
23 DWF=[0](cms), CN/C=[67], IA=[5.0](mm),
24 N=[3], TP=[0.37]hrs,
25 RAINFALL[ , , -1]
26 *#*****
   *****
27 *# TAY RIVER
28 *#*****
   *****
29 CALIB NASHYD   NHYD=[ "Tay" ], DT=[1]min, AREA=[22.86](ha),
30 DWF=[0](cms), CN/C=[70], IA=[5.0](mm),
31 N=[3], TP=[0.48]hrs,
32 RAINFALL[ , , -1]
33
34 *%-----|-----|
35 ADD HYD       NHYDsum=[ "Total" ], NHYDs to add=[ "Grants"+"Tay" ]
36 *#####
37 *# STORMS
38 *#####
39 *% 25 mm Storm based on 2-Year, 3-Hour Chicago Storm
40 *%START          TZERO=[0.0],  METOUT=[2],  NSTORM=[1],  NRUN=[001]
41 *%              [ "25MMC3H.stm" ] <--storm filename, one per line for NSTORM time
42 *%-----|-----|
43 *% 2-Year, 3-Hour Chicago Storm
44 START          TZERO=[0.0],  METOUT=[2],  NSTORM=[1],  NRUN=[002]
45 [ "002YRCHI3HR.stm" ] <--storm filename, one per line for NSTORM time
46 *%-----|-----|
47 *% 5-Year, 3-Hour Chicago Storm
48 START          TZERO=[0.0],  METOUT=[2],  NSTORM=[1],  NRUN=[005]
49 [ "005YRCHI3HR.stm" ] <--storm filename, one per line for NSTORM time
50 *%-----|-----|
51 *% 10-Year, 3-Hour Chicago Storm
52 START          TZERO=[0.0],  METOUT=[2],  NSTORM=[1],  NRUN=[010]
53 [ "010YRCHI3HR.stm" ] <--storm filename, one per line for NSTORM time
54 *%-----|-----|
55 *% 25-Year, 3-Hour Chicago Storm
56 START          TZERO=[0.0],  METOUT=[2],  NSTORM=[1],  NRUN=[025]
57 [ "025YRCHI3HR.stm" ] <--storm filename, one per line for NSTORM time
58 *%-----|-----|
59 *% 50-Year, 3-Hour Chicago Storm
60 START          TZERO=[0.0],  METOUT=[2],  NSTORM=[1],  NRUN=[050]
61 [ "050YRCHI3HR.stm" ] <--storm filename, one per line for NSTORM time

```

```

62  *%-----|-----
63  *% 100-Year, 3-Hour Chicago Storm
64  START      TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[099]
65            ["100YRCHI3HR.stm"] <--storm filename, one per line for NSTORM time
66  *%-----|-----
67  *% 2-Year, 24-Hour SCS Storm
68  START      TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[102]
69            ["002YRSCS24HR.stm"] <--storm filename, one per line for NSTORM time
70  *%-----|-----
71  *% 5-Year, 24-Hour SCS Storm
72  START      TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[105]
73            ["005YRSCS24HR.stm"] <--storm filename, one per line for NSTORM time
74  *%-----|-----
75  *% 10-Year, 24-Hour SCS Storm
76  START      TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[110]
77            ["010YRSCS24HR.stm"] <--storm filename, one per line for NSTORM time
78  *%-----|-----
79  *% 25-Year, 24-Hour SCS Storm
80  START      TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[125]
81            ["025YRSCS24HR.stm"] <--storm filename, one per line for NSTORM time
82  *%-----|-----
83  *% 50-Year, 24-Hour SCS Storm
84  START      TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[150]
85            ["050YRSCS24HR.stm"] <--storm filename, one per line for NSTORM time
86  *%-----|-----
87  *% 100-Year, 24-Hour SCS Storm
88  START      TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[199]
89            ["100YRSCS24HR.stm"] <--storm filename, one per line for NSTORM time
90  *%-----|-----
91  *% 100-Year, 24-Hour SCS Storm + 20%
92  *START      TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[998]
93  *%          ["SC24100x+.stm"] <--storm filename, one per line for NSTORM time
94  *%-----|-----
95  *% 100-Year, 3-Hour Chicago Storm + 20%
96  *START      TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[999]
97  *          ["100YRCHI3HR+.stm"] <--storm filename, one per line for NSTORM time
98  *%-----|-----
99  FINISH
100

```

```

00001 [SDT=10.00:SDR= 3.00:PTOT= 37.67]
00002 *****
00003 SSSS W W M M H H Y Y M M O O 222 000 11 5555
00004 S W W M M M M H H Y Y M M M O O 2 0 0 11 5
00005 SSSS W W M M M M H H Y Y M M M O O 2 0 0 11 5 Ver 5.500
00006 S W W M M M H H Y Y M M O O 222 0 0 11 555 FEB 2015
00007 SSSS W W M M H H Y Y M M O O 2 0 0 11 5
00008 2 0 0 11 5 # 2549237
00009 StormWater Management Hydrologic Model 222 000 11 555 *****
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00361 #
00362 # Company : J.F. Sabourin and Associates
00363 # License # : 2549237
00364 # Model developed to simulate runoff from subcatchments under pre development conditions
00365 # CN based on continuous simulation results with CN from water budget converted from AMCIII to AMCII
00366 # for summer design storms. Note TP per FFA method is directly determined by CN
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00720 #

```

```

00721> R0199:000004-----DRAIN-ID:MSVD-----AREAAb-QPEAKcms-TpeakDate_jh:mm-----RVMm-R.C-----DWFcms
00722> CALIB MSVD 1.0 01:7day 22.86 1.800 No_date 12:23 57.25 487 .000
00723> [CM= 70.0; N= 3.00; Tp= .48]
00724> R0199:000005-----DRAIN-ID:MSVD-----AREAAb-QPEAKcms-TpeakDate_jh:mm-----RVMm-R.C-----DWFcms
00725> ADD STD 1.0 02:6days 22.01 1.932 No_date 12:16 53.14 n/a .000
00726> + 1.0 02:7day 22.86 1.800 No_date 12:23 57.25 n/a .000
00727> SUM= 1.0 01:7total 44.87 3.694 No_date 12:19 55.33 n/a .000
00728> #####
00729> # STOPS
00730> #####
00731> R0199:000002-----
00732> FINISH
00733>
00734>
00735> WARNINGS / ERRORS / NOTES
00736>
00737> Simulation ended on 2023-02-15 at 16:23:19
00738>
00739>

```



```

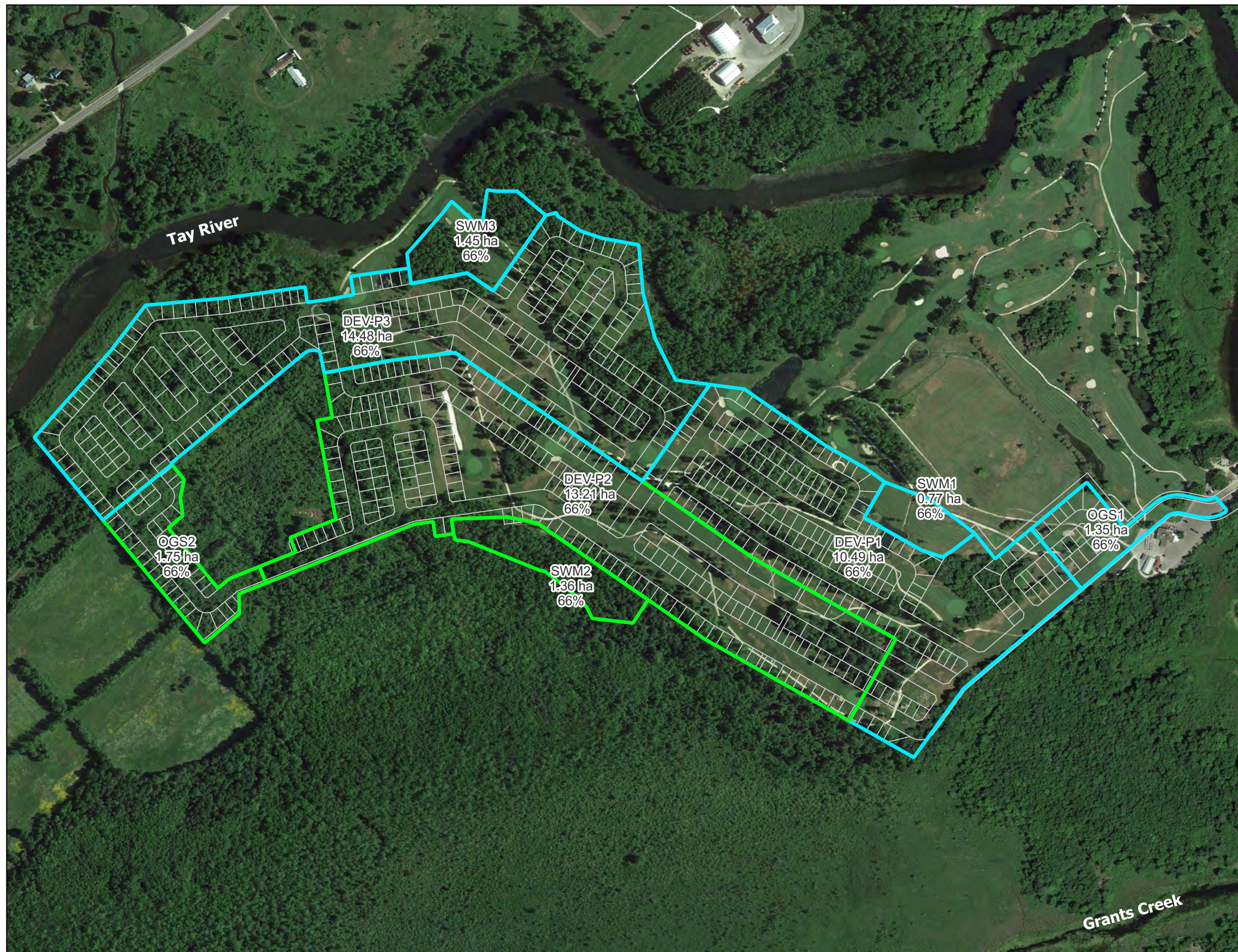
1  20    Metric units / ID numbers OFF
2  *#*****
   *****
3  *#  SWMHYMO  /  INPUT DATA FILE
4  *#*****
   *****
5  *#  Project Name  : [Caivan Perth properties]
6  *#  Project Number: [2118]
7  *#  Date          : [2023 JAN 26]
8  *#  Modeller     : [JB]
9  *#  Company      : J.F. Sabourin and Associates
10 *#  License #    : 2549237
11 *#*****
   *****
12 *# Model developed to simulate runoff from subcatchments under post development
   conditions and to size SWM ponds
13 *#*****
   *****
14 START          TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[001]
15 [ "25MMC3H.stm" ] <--storm filename, one per line for NSTORM time
16 *              [ "100YRSCS24HR.stm" ] <--storm filename, one per line for NSTORM time
17 *              [ "100YRCHI3HR.stm" ] <--storm filename, one per line for NSTORM time
18
19 *%-----|-----|
20 READ STORM      STORM_FILENAME=[ "STORM.001" ]
21 *%-----|-----|
   -----|
22 *#*****
   *****
23 *# TAY RIVER
24 *#*****
   *****
25 CALIB STANDHYD  NHYD=[ "Dev-P1" ], DT=[1](min), AREA=[10.493](ha), XIMP=[0.56],
   TIMP=[0.66], DWF=[0](cms),
26 LOSS=[1] Horton Equ: Fo=[76.2](mm/hr), Fc=[13.2](mm/hr),
   DCAY=[4.14](/hr), F=[0.00](mm),
27 Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
   MNP=[0.25], SCP=[0](min),
28 Impervious areas: IAimp=[1.57](mm), SLPI=[0.5](%), LGI=[264](m),
   MNI=[0.013], SCI=[0](min),
29 RAINFALL=[ , , -1](mm/hr)
30 *%-----|-----|
   -----|
31 CALIB STANDHYD  NHYD=[ "SWM1" ], DT=[1](min), AREA=[0.767](ha), XIMP=[0.56],
   TIMP=[0.66], DWF=[0](cms),
32 LOSS=[1] Horton Equ: Fo=[76.2](mm/hr), Fc=[13.2](mm/hr),
   DCAY=[4.14](/hr), F=[0.00](mm),
33 Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
   MNP=[0.25], SCP=[0](min),*
34 Impervious areas: IAimp=[1.57](mm), SLPI=[0.5](%), LGI=[71](m),
   MNI=[0.013], SCI=[0](min),
35 RAINFALL=[ , , -1](mm/hr)
36 *%-----|-----|
   -----|
37 CALIB STANDHYD  NHYD=[ "OGS1" ], DT=[1](min), AREA=[1.353](ha), XIMP=[0.56],
   TIMP=[0.66], DWF=[0](cms),
38 LOSS=[1] Horton Equ: Fo=[76.2](mm/hr), Fc=[13.2](mm/hr),
   DCAY=[4.14](/hr), F=[0.00](mm),
39 Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
   MNP=[0.25], SCP=[0](min),
40 Impervious areas: IAimp=[1.57](mm), SLPI=[0.5](%), LGI=[95](m),
   MNI=[0.013], SCI=[0](min),
41 RAINFALL=[ , , -1](mm/hr)
42 *%-----|-----|
   -----|
43 ADD HYD        NHYDsum=[ "Pond1-In" ], NHYDs to add=[ "Dev-P1"+"SWM1"+"OGS1" ]
44 *%-----|-----|
   -----|
45 ROUTE RESERVOIR NHYDout=[ "Pond1-Out" ], NHYDin=[ "Pond1-In" ], RDT=[1](min),

```

```

46             TABLE of ( OUTFLOW-STORAGE ) values
47             (cms) - (ha-m)
48             [ 0.0 , 0.0 ]
49             [ 0.001 , 0.0505 ]
50             [ 0.056 , 0.14763 ]
51             [ 0.066 , 0.17252 ]
52             [ 0.126 , 0.23392 ]
53             [ 0.174 , 0.27454 ]
54             [ 0.196 , 0.2805 ]
55             [ 0.241 , 0.3297 ]
56             [ 0.296 , 0.3725 ]
57             [ 0.331 , 0.3745 ]
58             [ 0.355 , 0.41417 ]
59             [ 0.436 , 0.43417 ]
60             [ 0.574 , 0.50267 ]
61             [ 0.683 , 0.55377 ]
62             [ 0.795 , 0.6051 ]
63             [ -1 , -1 ]
64             NHYDovf=[ "Pond1-Over" ],
65 *%-----|-----
66 CALIB STANDHYD NHYD=[ "Dev-P3" ], DT=[1](min), AREA=[14.479](ha), XIMP=[0.56],
TIMP=[0.66], DWF=[0](cms),
67 LOSS=[1] Horton Equ: Fo=[76.2](mm/hr), Fc=[13.2](mm/hr),
DCAy=[4.14](/hr), F=[0.00](mm),
68 Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.25], SCP=[0](min),
69 Impervious areas: IAimp=[1.57](mm), SLPI=[0.5](%), LGI=[311](m),
MNI=[0.013], SCI=[0](min),
70 RAINFALL=[ , , -1](mm/hr)
71 *%-----|-----
72 CALIB STANDHYD NHYD=[ "SWM3" ], DT=[1](min), AREA=[1.452](ha), XIMP=[0.56],
TIMP=[0.66], DWF=[0](cms),
73 LOSS=[1] Horton Equ: Fo=[76.2](mm/hr), Fc=[13.2](mm/hr),
DCAy=[4.14](/hr), F=[0.00](mm),
74 Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.25], SCP=[0](min),
75 Impervious areas: IAimp=[1.57](mm), SLPI=[0.5](%), LGI=[98](m),
MNI=[0.013], SCI=[0](min),
76 RAINFALL=[ , , -1](mm/hr)
77 *%-----|-----
78 ADD HYD NHYDsum=[ "Pond3-In" ], NHYDs to add=[ "Dev-P3"+"SWM3" ]
79 *%-----|-----
80 ROUTE RESERVOIR NHYDout=[ "Pond3-Out" ], NHYDin=[ "Pond3-In" ], RDT=[1](min),
81 TABLE of ( OUTFLOW-STORAGE ) values
82 (cms) - (ha-m)
83 [ 0.0 , 0.0 ]
84 [ 0.002 , 0.0637 ]
85 [ 0.07 , 0.18661 ]
86 [ 0.084 , 0.2178 ]
87 [ 0.159 , 0.2954 ]
88 [ 0.219 , 0.3466 ]
89 [ 0.248 , 0.3528 ]
90 [ 0.305 , 0.4156 ]
91 [ 0.373 , 0.470 ]
92 [ 0.419 , 0.4712 ]
93 [ 0.449 , 0.5221 ]
94 [ 0.55 , 0.54615 ]
95 [ 0.724 , 0.6326 ]
96 [ 0.862 , 0.69617 ]
97 [ 1.005 , 0.761 ]
98 [ -1 , -1 ]
99 NHYDovf=[ "Pond1-Over" ],
100 *%-----|-----
101 *ADD HYD NHYDsum=[ "Tay" ], NHYDs to

```



Legend

Drainage Area

[Name]

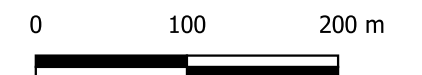
[Area]

[% Imp]

Drains to Tay River

Drains to Grants Creek

SCALE: 1:5000



J.F. Sabourin and Associates Inc.
 WATER RESOURCES AND ENVIRONMENTAL CONSULTANTS
 52 Springbrook Drive Ottawa, ON, K2S 1B9 (613) 836-3884 www.jfsa.com

CAIVAN
 COMMUNITIES

Perth Golf Course

Figure E5: Post-Development Drainage Area

PROJECT	2118-21
DRAWN	BT
DATE	February 2023

```

102 add=["Pond1-Out"+"Pond1-Over"+"Pond3-Out"+"Pond3-Over"]
103 *%-----|-----
104 *#*****
105 *# GRANTS CREEK
106 *#*****
106 CALIB STANDHYD      NHYD=["DEV-P2"], DT=[1](min), AREA=[13.211](ha), XIMP=[0.56],
107 TIMP=[0.66], DWF=[0](cms),
108 LOSS=[1] Horton Equ: Fo=[76.2](mm/hr), Fc=[13.2](mm/hr),
109 DCAY=[4.14](/hr), F=[0.00](mm),
110 Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
111 MNP=[0.25], SCP=[0](min),
112 Impervious areas: IAimp=[1.57](mm), SLPI=[0.5](%), LGI=[297](m),
113 MNI=[0.013], SCI=[0](min),
114 RAINFALL=[ , , -1](mm/hr)
115 *%-----|-----
116 CALIB STANDHYD      NHYD=["SWM2"], DT=[1](min), AREA=[1.355](ha), XIMP=[0.56],
117 TIMP=[0.66], DWF=[0](cms),
118 LOSS=[1] Horton Equ: Fo=[76.2](mm/hr), Fc=[13.2](mm/hr),
119 DCAY=[4.14](/hr), F=[0.00](mm),
120 Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
121 MNP=[0.25], SCP=[0](min),
122 Impervious areas: IAimp=[1.57](mm), SLPI=[0.5](%), LGI=[95](m),
123 MNI=[0.013], SCI=[0](min),
124 RAINFALL=[ , , -1](mm/hr)
125 *%-----|-----
126 CALIB STANDHYD      NHYD=["OGS2"], DT=[1](min), AREA=[1.754](ha), XIMP=[0.56],
127 TIMP=[0.66], DWF=[0](cms),
128 LOSS=[1] Horton Equ: Fo=[76.2](mm/hr), Fc=[13.2](mm/hr),
129 DCAY=[4.14](/hr), F=[0.00](mm),
130 Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
131 MNP=[0.25], SCP=[0](min),
132 Impervious areas: IAimp=[1.57](mm), SLPI=[0.5](%), LGI=[108](m),
133 MNI=[0.013], SCI=[0](min),
134 RAINFALL=[ , , -1](mm/hr)
135 *%-----|-----
136 ADD HYD              NHYDsum=["Pond2-In"], NHYDs to add=["DEV-P2"+"SWM2"+"OGS2"]
137 *%-----|-----
138 ROUTE RESERVOIR     NHYDout=["Pond2-Out"], NHYDin=["Pond2-In"], RDT=[1](min),
139 TABLE of ( OUTFLOW-STORAGE ) values
140 (cms) - (ha-m)
141 [ 0 , 0 ]
142 [ 0.002 , 0.0653 ]
143 [ 0.125 , 0.1723 ]
144 [ 0.149 , 0.1974 ]
145 [ 0.288 , 0.26845 ]
146 [ 0.399 , 0.3151 ]
147 [ 0.559 , 0.3773 ]
148 [ 0.688 , 0.4223 ]
149 [ 0.83 , 0.4678 ]
150 [ 1.382 , 0.54086 ]
151 [ 1.653 , 0.5874 ]
152 [ 1.932 , 0.6343 ]
153 [ -1 , -1 ]
154 NHYDovf=["Pond2-Over"],
155 *%-----|-----
156 *SAVE HYD           NHYD=["OGSGrant"], # OF PCYCLES=[-1], ICASEsh=[1]
157 *                   HYD_COMMENT=["Overflows to Grants Creek from uncontrolled"]
158 *%-----|-----
159 *ADD HYD            NHYDsum=["Grant"], NHYDs to add=["Pond2-Out"+"Pond2-Over"]
160 *%-----|-----

```

```

-----|
149 *ADD HYD          NHYDsum=["Total"], NHYDs to add=["Tay"+"Grant"]
150 *%-----|-----
-----|
151 *#####
152 *# STORMS
153 *#####
154 *% 25 mm Storm based on 2-Year, 3-Hour Chicago Storm
155 *%START          TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[001]
156 *%              ["25MMC3H.stm"] <--storm filename, one per line for NSTORM time
157 *%-----|-----
158 *% 2-Year, 3-Hour Chicago Storm
159 START          TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[002]
160 ["002YRCHI3HR.stm"] <--storm filename, one per line for NSTORM time
161 *%-----|-----
162 *% 5-Year, 3-Hour Chicago Storm
163 START          TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[005]
164 ["005YRCHI3HR.stm"] <--storm filename, one per line for NSTORM time
165 *%-----|-----
166 *% 10-Year, 3-Hour Chicago Storm
167 START          TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[010]
168 ["010YRCHI3HR.stm"] <--storm filename, one per line for NSTORM time
169 *%-----|-----
170 *% 25-Year, 3-Hour Chicago Storm
171 START          TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[025]
172 ["025YRCHI3HR.stm"] <--storm filename, one per line for NSTORM time
173 *%-----|-----
174 *% 50-Year, 3-Hour Chicago Storm
175 START          TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[050]
176 ["050YRCHI3HR.stm"] <--storm filename, one per line for NSTORM time
177 *%-----|-----
178 *% 100-Year, 3-Hour Chicago Storm
179 START          TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[099]
180 ["100YRCHI3HR.stm"] <--storm filename, one per line for NSTORM time
181 *%-----|-----
182 *% 2-Year, 24-Hour SCS Storm
183 START          TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[102]
184 ["002YRSCS24HR.stm"] <--storm filename, one per line for NSTORM time
185 *%-----|-----
186 *% 5-Year, 24-Hour SCS Storm
187 START          TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[105]
188 ["005YRSCS24HR.stm"] <--storm filename, one per line for NSTORM time
189 *%-----|-----
190 *% 10-Year, 24-Hour SCS Storm
191 START          TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[110]
192 ["010YRSCS24HR.stm"] <--storm filename, one per line for NSTORM time
193 *%-----|-----
194 *% 25-Year, 24-Hour SCS Storm
195 START          TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[125]
196 ["025YRSCS24HR.stm"] <--storm filename, one per line for NSTORM time
197 *%-----|-----
198 *% 50-Year, 24-Hour SCS Storm
199 START          TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[150]
200 ["050YRSCS24HR.stm"] <--storm filename, one per line for NSTORM time
201 *%-----|-----
202 *% 100-Year, 24-Hour SCS Storm
203 START          TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[199]
204 ["100YRSCS24HR.stm"] <--storm filename, one per line for NSTORM time
205 *%-----|-----
206 *% 100-Year, 24-Hour SCS Storm + 20%
207 *%START          TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[998]
208 *%              ["SC24l00x+.stm"] <--storm filename, one per line for NSTORM time
209 *%-----|-----
210 *% 100-Year, 3-Hour Chicago Storm + 20%
211 *%START          TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[999]
212 *%              ["100YRCHI3HR+.stm"] <--storm filename, one per line for NSTORM time
213 *%-----|-----
214 FINISH
215

```

00001 *****
00002 *****
00003 SSSSS W W M M H H Y Y M M O O 222 000 11 5555 *****
00004 S W W M M M M H H Y Y M M O O 2 0 0 11 5 *****
00005 SSSSS W W M M M M M M M M O O 222 000 11 555 Ver 5.500 *****
00006 S W W M M M H H Y Y M M O O 222 000 11 555 FEB 2015 *****
00007 SSSSS W W M M H H Y Y M M O O 2 0 0 11 5 *****
00008 *****
00009 *****
00010 StormWater Management Hydrologic Model 222 000 11 555 *****
00011 *****
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03621 [Model used: 2954E=00 m3, TotOvVol=0.0000E+00 m3, N-Ovfl= 0, TotDurOvfl= 0 hrs]
03622 *****
03623 # GRANTS CREEK
03624 [XIMP: 56;TIMP: 66]
03625 [Horton parameters: Fw = 76.20;Frc = 13.20;DCAY4:1.41; Fc = .00]
03626 [Previous area: IArea= 4.67;SLPP=2.00;LDP= 40.0;MP= 250;SCP= .0]
03627 [Impervious area: IAlmp = 1.57;SLPI= .50;LGI= 98.0;MI= .013;SCL= .0]

04841 R025:CO0002-----DtmIn-ID:NHYD-----AREHA-QP:ARcm=PeakDate_hh:mm-----RvM-R-C-----DWFms
04842 [XIMP: 56;TIMP: 66]
04843 [Horton parameters: Fw = 76.20;Frc = 13.20;DCAY4:1.41; Fc = .00]
04844 [Previous area: IArea= 4.67;SLPP=2.00;LDP= 40.0;MP= 250;SCP= .0]
04845 [Impervious area: IAlmp = 1.57;SLPI= .50;LGI= 98.0;MI= .013;SCL= .0]

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00721 [XMP# 56;TIMP# 66]
00722 [Horton parameters: P# 76.20;F# 13.20;DCA#4.14; F# 0.0]
00723 [Previous area: I#APE# 4.67;SLP# 2.00;LSD# 40.0;MP# 250;SCP# 0]
00724 [Impervious area: I#AIP# 1.57;SLIP# 50;L#I# 297.0;MI# 0.13;S#C# 0]
00725 R0505-C00101-----D#AIN-ID#HYD-----AREA#A-#PE#A#C#m#T#p#k#Date_hh:mm-----R#M#R-C-----DW#F#
00726 CALIS STANHYD 1.0 01;SWM2 1.36 .377 No.date 1:00 40.85 714 .000
00727 [XMP# 56;TIMP# 66]
00728 [Horton parameters: P# 76.20;F# 13.20;DCA#4.14; F# 0.0]
00729 [Previous area: I#APE# 4.67;SLP# 2.00;LSD# 40.0;MP# 250;SCP# 0]
00730 [Impervious area: I#AIP# 1.57;SLIP# 50;L#I# 95.0;MI# 0.13;S#C# 0]
00731 R0505-C00101-----D#AIN-ID#HYD-----AREA#A-#PE#A#C#m#T#p#k#Date_hh:mm-----R#M#R-C-----DW#F#
00732 CALIS STANHYD 1.0 01;SWM2 1.75 .483 No.date 1:00 40.85 714 .000
00733 [XMP# 56;TIMP# 66]
00734 [Horton parameters: P# 76.20;F# 13.20;DCA#4.14; F# 0.0]
00735 [Previous area: I#APE# 4.67;SLP# 2.00;LSD# 40.0;MP# 250;SCP# 0]
00736 [Impervious area: I#AIP# 1.57;SLIP# 50;L#I# 108.0;MI# 0.13;S#C# 0]
00737 R0505-C00101-----D#AIN-ID#HYD-----AREA#A-#PE#A#C#m#T#p#k#Date_hh:mm-----R#M#R-C-----DW#F#
00738 ADD HYD 1.0 02;DEV-P2 13.21 3.017 No.date 1:02 40.85 n/a .000
00739 * 1.0 02;SWM2 1.36 .377 No.date 1:00 40.85 n/a .000
00740 * 1.0 02;OS2S 1.75 .483 No.date 1:00 40.85 n/a .000
00741 * 1.0 01;Pond3-in 16.32 3.812 No.date 1:01 40.85 n/a .000
00742 R0505-C00101-----D#AIN-ID#HYD-----AREA#A-#PE#A#C#m#T#p#k#Date_hh:mm-----R#M#R-C-----DW#F#
00743 ROUTE RESERVOIR -> 1.0 03;Pond2-in 16.32 3.812 No.date 1:01 40.85 n/a .000
00744 out <= 1.0 03;Pond2-out 16.32 .688 No.date 1:29 40.84 n/a .000
00745 * 1.0 03;Pond2-Over 0.00 .000 No.date 0:00 .00 n/a .000
00746 [M#otUsed# 4223E+00 n3, TotOfVol# 0.000E+00 m3, N-Ov# 0, TotDurOfV# 0.hrs]
00747 #####
00748 # STORMS
00749 *****
00750 ** END OF RUN # 98
00751
00752
00753
00754
00755
00756
00757
00758 RUN#COMMAND#
00759 R0999-C00010-----
00760 START
00761 [T#R#O = .00 hrs on 0]
00762 [M#T#O#T = 2 (Imperial, 2-metric output)]
00763 [N#T#O#W = 1]
00764 [S#M#Y#N#O = 1]
00765 *****
00766 # SWMHYD / INPUT DATA FILE
00767 # *****
00768 # Project Name : [Caivan Perth properties]
00769 # Project Number: [2118]
00770 # Date : [2023 JAN 26]
00771 # Modeller : [JB]
00772 # Company : [J.F. Sabourin and Associates]
00773 # License # : 2549237
00774 *****
00775 # Model developed to simulate runoff from subcatchments under post development conditions and to size SWM ponds
00776 *****
00777 R0999-C00020-----
00778 READ STORM
00779 Filename = STORM.001
00780 Comment = 100VRSCH248R-Perth MTO IDP
00781 [S#T#I#10.0;S#D#R# 3.00;P#T#O# 53.12]
00782 *****
00783 # TAY RIVER
00784 R0999-C00030-----D#AIN-ID#HYD-----AREA#A-#PE#A#C#m#T#p#k#Date_hh:mm-----R#M#R-C-----DW#F#
00785 CALIS STANHYD 1.0 01;DEV-P1 10.49 2.815 No.date 1:02 46.06 731 .000
00786 [XMP# 56;TIMP# 66]
00787 [Horton parameters: P# 76.20;F# 13.20;DCA#4.14; F# 0.0]
00788 [Previous area: I#APE# 4.67;SLP# 2.00;LSD# 40.0;MP# 250;SCP# 0]
00789 [Impervious area: I#AIP# 1.57;SLIP# 50;L#I# 264.0;MI# 0.13;S#C# 0]
00790 R0999-C00040-----D#AIN-ID#HYD-----AREA#A-#PE#A#C#m#T#p#k#Date_hh:mm-----R#M#R-C-----DW#F#
00791 CALIS STANHYD 1.0 01;SWM2 1.77 .250 No.date 1:00 46.06 731 .000
00792 [XMP# 56;TIMP# 66]
00793 [Horton parameters: P# 76.20;F# 13.20;DCA#4.14; F# 0.0]
00794 [Previous area: I#APE# 4.67;SLP# 2.00;LSD# 40.0;MP# 250;SCP# 0]
00795 [Impervious area: I#AIP# 1.57;SLIP# 50;L#I# 71.0;MI# 0.13;S#C# 0]
00796 R0999-C00050-----D#AIN-ID#HYD-----AREA#A-#PE#A#C#m#T#p#k#Date_hh:mm-----R#M#R-C-----DW#F#
00797 CALIS STANHYD 1.0 01;SWM3 1.35 .432 No.date 1:00 46.06 731 .000
00798 [XMP# 56;TIMP# 66]
00799 [Horton parameters: P# 76.20;F# 13.20;DCA#4.14; F# 0.0]
00800 [Previous area: I#APE# 4.67;SLP# 2.00;LSD# 40.0;MP# 250;SCP# 0]
00801 [Impervious area: I#AIP# 1.57;SLIP# 50;L#I# 311.0;MI# 0.13;S#C# 0]
00802 R0999-C00060-----D#AIN-ID#HYD-----AREA#A-#PE#A#C#m#T#p#k#Date_hh:mm-----R#M#R-C-----DW#F#
00803 CALIS STANHYD 1.0 01;DEV-P1 10.49 2.815 No.date 1:02 46.06 731 .000
00804 ADD HYD + 1.0 02;DEV-P1 10.49 2.815 No.date 1:02 46.06 n/a .000
00805 * 1.0 02;OS2S 1.75 .483 No.date 1:00 46.06 n/a .000
00806 * 1.0 02;OS2S 1.75 .432 No.date 1:00 46.06 n/a .000
00807 * 1.0 01;Pond3-in 12.61 3.439 No.date 1:01 46.06 n/a .000
00808 R0999-C00070-----D#AIN-ID#HYD-----AREA#A-#PE#A#C#m#T#p#k#Date_hh:mm-----R#M#R-C-----DW#F#
00809 ROUTE RESERVOIR -> 1.0 02;Pond2-in 12.61 3.439 No.date 1:01 46.06 n/a .000
00810 out <= 1.0 02;Pond2-out 12.61 .643 No.date 1:43 46.03 n/a .000
00811 overflow <= 1.0 03;Pond2-Over 0.00 .000 No.date 0:00 .00 n/a .000
00812 [M#otUsed# 1411E+00 n3, TotOfVol# 0.000E+00 m3, N-Ov# 0, TotDurOfV# 0.hrs]
00813 R0999-C00080-----D#AIN-ID#HYD-----AREA#A-#PE#A#C#m#T#p#k#Date_hh:mm-----R#M#R-C-----DW#F#
00814 CALIS STANHYD 1.0 01;DEV-P3 14.48 3.792 No.date 1:02 46.06 731 .000
00815 [XMP# 56;TIMP# 66]
00816 [Horton parameters: P# 76.20;F# 13.20;DCA#4.14; F# 0.0]
00817 [Previous area: I#APE# 4.67;SLP# 2.00;LSD# 40.0;MP# 250;SCP# 0]
00818 [Impervious area: I#AIP# 1.57;SLIP# 50;L#I# 311.0;MI# 0.13;S#C# 0]
00819 R0999-C00090-----D#AIN-ID#HYD-----AREA#A-#PE#A#C#m#T#p#k#Date_hh:mm-----R#M#R-C-----DW#F#
00820 CALIS STANHYD 1.0 01;SWM3 1.45 .462 No.date 1:00 46.06 731 .000
00821 [XMP# 56;TIMP# 66]
00822 [Horton parameters: P# 76.20;F# 13.20;DCA#4.14; F# 0.0]
00823 [Previous area: I#APE# 4.67;SLP# 2.00;LSD# 40.0;MP# 250;SCP# 0]
00824 [Impervious area: I#AIP# 1.57;SLIP# 50;L#I# 99.0;MI# 0.13;S#C# 0]
00825 R0999-C00100-----D#AIN-ID#HYD-----AREA#A-#PE#A#C#m#T#p#k#Date_hh:mm-----R#M#R-C-----DW#F#
00826 ADD HYD + 1.0 02;DEV-P2 14.48 3.792 No.date 1:02 46.06 n/a .000
00827 * 1.0 01;Pond3-in 15.93 4.211 No.date 1:02 46.06 n/a .000
00828 R0999-C00110-----D#AIN-ID#HYD-----AREA#A-#PE#A#C#m#T#p#k#Date_hh:mm-----R#M#R-C-----DW#F#
00829 ROUTE RESERVOIR -> 1.0 02;Pond2-in 15.93 4.211 No.date 1:02 46.06 n/a .000
00830 out <= 1.0 03;Pond2-out 15.93 .449 No.date 1:44 46.03 n/a .000
00831 overflow <= 1.0 03;Pond2-Over 0.00 .000 No.date 0:00 .00 n/a .000
00832 [M#otUsed# 5221E+00 n3, TotOfVol# 0.000E+00 m3, N-Ov# 0, TotDurOfV# 0.hrs]
00833 R0999-C00120-----D#AIN-ID#HYD-----AREA#A-#PE#A#C#m#T#p#k#Date_hh:mm-----R#M#R-C-----DW#F#
00834 CALIS STANHYD 1.0 01;DEV-P2 13.21 3.485 No.date 1:02 46.06 731 .000
00835 [XMP# 56;TIMP# 66]
00836 [Horton parameters: P# 76.20;F# 13.20;DCA#4.14; F# 0.0]
00837 [Previous area: I#APE# 4.67;SLP# 2.00;LSD# 40.0;MP# 250;SCP# 0]
00838 [Impervious area: I#AIP# 1.57;SLIP# 50;L#I# 311.0;MI# 0.13;S#C# 0]
00839 R0999-C00130-----D#AIN-ID#HYD-----AREA#A-#PE#A#C#m#T#p#k#Date_hh:mm-----R#M#R-C-----DW#F#
00840 CALIS STANHYD 1.0 01;SWM3 1.36 .432 No.date 1:00 46.06 731 .000
00841 [XMP# 56;TIMP# 66]
00842 [Horton parameters: P# 76.20;F# 13.20;DCA#4.14; F# 0.0]
00843 [Previous area: I#APE# 4.67;SLP# 2.00;LSD# 40.0;MP# 250;SCP# 0]
00844 [Impervious area: I#AIP# 1.57;SLIP# 50;L#I# 95.0;MI# 0.13;S#C# 0]
00845 R0999-C00140-----D#AIN-ID#HYD-----AREA#A-#PE#A#C#m#T#p#k#Date_hh:mm-----R#M#R-C-----DW#F#
00846 CALIS STANHYD 1.0 01;SWM2 1.75 .483 No.date 1:00 46.06 731 .000
00847 [XMP# 56;TIMP# 66]
00848 [Horton parameters: P# 76.20;F# 13.20;DCA#4.14; F# 0.0]
00849 [Previous area: I#APE# 4.67;SLP# 2.00;LSD# 40.0;MP# 250;SCP# 0]
00850 [Impervious area: I#AIP# 1.57;SLIP# 50;L#I# 95.0;MI# 0.13;S#C# 0]
00851 R0999-C00150-----D#AIN-ID#HYD-----AREA#A-#PE#A#C#m#T#p#k#Date_hh:mm-----R#M#R-C-----DW#F#
00852 CALIS STANHYD 1.0 01;OS2S 1.75 .484 No.date 1:00 46.06 731 .000
00853 [Previous area: I#APE# 4.67;SLP# 2.00;LSD# 40.0;MP# 250;SCP# 0]
00854 [Impervious area: I#AIP# 1.57;SLIP# 50;L#I# 108.0;MI# 0.13;S#C# 0]
00855 R0999-C00160-----D#AIN-ID#HYD-----AREA#A-#PE#A#C#m#T#p#k#Date_hh:mm-----R#M#R-C-----DW#F#
00856 ADD HYD + 1.0 02;DEV-P2 13.21 3.485 No.date 1:02 46.06 n/a .000
00857 * 1.0 02;OS2S 1.75 .554 No.date 1:00 46.06 n/a .000
00858 * 1.0 01;Pond3-in 16.32 4.404 No.date 1:01 46.06 n/a .000
00859 R0999-C00170-----D#AIN-ID#HYD-----AREA#A-#PE#A#C#m#T#p#k#Date_hh:mm-----R#M#R-C-----DW#F#
00860 ROUTE RESERVOIR -> 1.0 02;Pond2-in 16.32 4.404 No.date 1:01 46.06 n/a .000
00861 out <= 1.0 03;Pond2-out 16.32 .830 No.date 1:27 46.05 n/a .000
00862 overflow <= 1.0 03;Pond2-Over 0.00 .000 No.date 0:00 .00 n/a .000
00863 [M#otUsed# 4678E+00 n3, TotOfVol# 0.000E+00 m3, N-Ov# 0, TotDurOfV# 0.hrs]
00864 #####
00865 # STORMS
00866 *****
00867 ** END OF RUN # 101
00868
00869
00870
00871
00872
00873
00874
00875
00876 RUN#COMMAND#
00877 R0102-C00010-----
00878 START
00879 [T#R#O = .00 hrs on 0]
00880 [M#T#O#T = 2 (Imperial, 2-metric output)]
00881 [N#T#O#W = 1]
00882 [S#M#Y#N#O = 1]
00883 *****
00884 # SWMHYD / INPUT DATA FILE
00885 # *****
00886 # Project Name : [Caivan Perth properties]
00887 # Project Number: [2118]
00888 # Date : [2023 JAN 26]
00889 # Modeller : [JB]
00890 # Company : [J.F. Sabourin and Associates]
00891 # License # : 2549237
00892 *****
00893 # Model developed to simulate runoff from subcatchments under post development conditions and to size SWM ponds
00894 *****
00895 R0102-C00020-----
00896 READ STORM
00897 Filename = STORM.001
00898 Comment = 002VRSCH248R-Perth MTO IDP
00899 [S#T#I#10.0;S#D#R# 3.00;P#T#O# 53.12]
00900 *****
00901 # TAY RIVER
00902 R0102-C00030-----D#AIN-ID#HYD-----AREA#A-#PE#A#C#m#T#p#k#Date_hh:mm-----R#M#R-C-----DW#F#
00903 CALIS STANHYD 1.0 01;DEV-P2 14.48 3.792 No.date 1:02 42.82 677 .000
00904 [XMP# 56;TIMP# 66]
00905 [Horton parameters: P# 76.20;F# 13.20;DCA#4.14; F# 0.0]
00906 [Previous area: I#APE# 4.67;SLP# 2.00;LSD# 40.0;MP# 250;SCP# 0]
00907 [Impervious area: I#AIP# 1.57;SLIP# 50;L#I# 264.0;MI# 0.13;S#C# 0]
00908 R0102-C00040-----D#AIN-ID#HYD-----AREA#A-#PE#A#C#m#T#p#k#Date_hh:mm-----R#M#R-C-----DW#F#
00909 CALIS STANHYD 1.0 01;SWM3 1.35 .432 No.date 1:00 42.82 677 .000
00910 [XMP# 56;TIMP# 66]
00911 [Horton parameters: P# 76.20;F# 13.20;DCA#4.14; F# 0.0]
00912 [Previous area: I#APE# 4.67;SLP# 2.00;LSD# 40.0;MP# 250;SCP# 0]
00913 [Impervious area: I#AIP# 1.57;SLIP# 50;L#I# 71.0;MI# 0.13;S#C# 0]
00914 R0102-C00050-----D#AIN-ID#HYD-----AREA#A-#PE#A#C#m#T#p#k#Date_hh:mm-----R#M#R-C-----DW#F#
00915 CALIS STANHYD 1.0 01;SWM3 1.36 .432 No.date 1:00 42.82 677 .000
00916 [XMP# 56;TIMP# 66]
00917 [Horton parameters: P# 76.20;F# 13.20;DCA#4.14; F# 0.0]
00918 [Previous area: I#APE# 4.67;SLP# 2.00;LSD# 40.0;MP# 250;SCP# 0]
00919 [Impervious area: I#AIP# 1.57;SLIP# 50;L#I# 95.0;MI# 0.13;S#C# 0]
00920 R0102-C00060-----D#AIN-ID#HYD-----AREA#A-#PE#A#C#m#T#p#k#Date_hh:mm-----R#M#R-C-----DW#F#
00921 CALIS STANHYD 1.0 01;OS2S 1.75 .483 No.date 1:00 42.82 677 .000
00922 ADD HYD + 1.0 02;SWM1 1.77 .099 No.date 12:00 34.58 n/a .000
00923 * 1.0 02;SWM1 1.35 .170 No.date 12:00 34.58 n/a .000
00924 * 1.0 01;Pond3-in 12.61 3.378 No.date 12:01 34.58 n/a .000
00925 R0102-C00070-----D#AIN-ID#HYD-----AREA#A-#PE#A#C#m#T#p#k#Date_hh:mm-----R#M#R-C-----DW#F#
00926 CALIS STANHYD 1.0 01;Pond3-in 12.61 3.378 No.date 12:01 34.58 n/a .000
00927 ROUTE RESERVOIR -> 1.0 02;Pond3-in 12.61 3.378 No.date 12:01 34.58 n/a .000
00928 out <= 1.0 03;Pond3-out 12.61 .196 No.date 12:37 34.57 n/a .000
00929 overflow <= 1.0 03;Pond3-Over 0.00 .000 No.date 0:00 .00 n/a .000
00930 [M#otUsed# 3835E+00 n3, TotOfVol# 0.000E+00 m3, N-Ov# 0, TotDurOfV# 0.hrs]
00931 R0102-C00080-----D#AIN-ID#HYD-----AREA#A-#PE#A#C#m#T#p#k#Date_hh:mm-----R#M#R-C-----DW#F#
00932 CALIS STANHYD 1.0 01;DEV-P3 14.48 3.792 No.date 12:02 34.58 651 .000
00933 [XMP# 56;TIMP# 66]
00934 [Horton parameters: P# 76.20;F# 13.20;DCA#4.14; F# 0.0]
00935 [Previous area: I#APE# 4.67;SLP# 2.00;LSD# 40.0;MP# 250;SCP# 0]
00936 [Impervious area: I#AIP# 1.57;SLIP# 50;L#I# 311.0;MI# 0.13;S#C# 0]
00937 R0102-C00090-----D#AIN-ID#HYD-----AREA#A-#PE#A#C#m#T#p#k#Date_hh:mm-----R#M#R-C-----DW#F#
00938 CALIS STANHYD 1.0 01;SWM3 1.45 .462 No.date 12:00 34.58 651 .000
00939 [XMP# 56;TIMP# 66]
00940 [Horton parameters: P# 76.20;F# 13.20;DCA#4.14; F# 0.0]
00941 [Previous area: I#APE# 4.67;SLP# 2.00;LSD# 40.0;MP# 250;SCP# 0]
00942 [Impervious area: I#AIP# 1.57;SLIP# 50;L#I# 98.0;MI# 0.13;S#C# 0]
00943 R0102-C00100-----D#AIN-ID#HYD-----AREA#A-#PE#A#C#m#T#p#k#Date_hh:mm-----R#M#R-C-----DW#F#
00944 ADD HYD + 1.0 02;DEV-P3 14.48 3.792 No.date 12:02 34.58 n/a .000
00945 * 1.0 02;OS2S 1.75 .483 No.date 12:00 34.58 n/a .000
00946 * 1.0 01;Pond3-in 15.93 4.194 No.date 12:02 34.58 n/a .000
00947 R0102-C00110-----D#AIN-ID#HYD-----AREA#A-#PE#A#C#m#T#p#k#Date_hh:mm-----R#M#R-C-----DW#F#
00948 ROUTE RESERVOIR -> 1.0 02;Pond3-in 15.93 4.194 No.date 12:02 34.58 n/a .000
00949 out <= 1.0 03;Pond3-out 15.93 .248 No.date 12:36 34.58 n/a .000
00950 overflow <= 1.0 03;Pond3-Over 0.00 .000 No.date 0:00 .00 n/a .000
00951 [M#otUsed# 3528E+00 n3, TotOfVol# 0.000E+00 m3, N-Ov# 0, TotDurOfV# 0.hrs]
00952 #####
00953 # GRANTS CREEK
00954 *****
00955 R0102-C00120-----D#AIN-ID#HYD-----AREA#A-#PE#A#C#m#T#p#k#Date_hh:mm-----R#M#R-C-----DW#F#
00956 CALIS STANHYD 1.0 01;DEV-P2 13.21 3.396 No.date 12:02 34.58 651 .000
00957 [XMP# 56;TIMP# 66]
00958 [Horton parameters: P# 76.20;F# 13.20;DCA#4.14; F# 0.0]
00959 [Previous area: I#APE# 4.67;SLP# 2.00;LSD# 40.0;MP# 250;SCP# 0]
00960 [Impervious area: I#AIP# 1.57;SLIP# 50;L#I# 297.0;MI# 0.13;S#C# 0]
00961 R0102-C00130-----D#AIN-ID#HYD-----AREA#A-#PE#A#C#m#T#p#k#Date_hh:mm-----R#M#R-C-----DW#F#
00962 CALIS STANHYD 1.0 01;SWM2 1.36 .377 No.date 12:00 34.58 651 .000
00963 [XMP# 56;TIMP# 66]
00964 [Horton parameters: P# 76.20;F# 13.20;DCA#4.14; F# 0.0]
00965 [Previous area: I#APE# 4.67;SLP# 2.00;LSD# 40.0;MP# 250;SCP# 0]
00966 [Impervious area: I#AIP# 1.57;SLIP# 50;L#I# 95.0;MI# 0.13;S#C# 0]
00967 R0102-C00140-----D#AIN-ID#HYD-----AREA#A-#PE#A#C#m#T#p#k#Date_hh:mm-----R#M#R-C-----DW#F#
00968 CALIS STANHYD 1.0 01;OS2S 1.75 .216 No.date 12:00 34.58 651 .000
00969 [XMP# 56;TIMP# 66]
00970 [Horton parameters: P# 76.20;F# 13.20;DCA#4.14; F# 0.0]
00971 [Previous area: I#APE# 4.67;SLP# 2.00;LSD# 40.0;MP# 250;SCP# 0]
00972 [Impervious area: I#AIP# 1.57;SLIP# 50;L#I# 264.0;MI# 0.13;S#C# 0]
00973 R0102-C00150-----D#AIN-ID#HYD-----AREA#A-#PE#A#C#m#T#p#k#Date_hh:mm-----R#M#R-C-----DW#F#
00974 ADD HYD + 1.0 02;DEV-P2 13.21 3.396 No.date 12:02 34.58 n/a .000
00975 * 1.0 02;SWM1 1.35 .171 No.date 12:00 34.58 n/a .000
00976 * 1.0 02;OS2S 1.75 .216 No.date 12:00 34.58 n/a .000
00977 * 1.0 01;Pond3-in 16.32 4.169 No.date 12:01 34.58 n/a .000
00978 R0102-C00160-----D#AIN-ID#HYD-----AREA#A-#PE#A#C#m#T#p#k#Date_hh:mm-----R#M#R-C-----DW#F#
00979 ROUTE RESERVOIR -> 1.0 02;Pond2-in 16.32 4.169 No.date 12:02 34.58 n/a .000
00980 out <= 1.0 03;Pond2-out 16.32 1.785 No.date 12:02 34.58 n/a .000
00981 overflow <= 1.0 03;Pond2-Over 0.00 .000 No.date 0:00 .00 n/a .000
00982 [M#otUsed# 4110E+00 n3, TotOfVol# 0.000E+00 m3, N-Ov# 0, TotDurOfV# 0.hrs]
00983 #####
00984 # STORMS
00985 *****
00986 ** END OF RUN # 104
00987
00988
00989
00990
00991
00992
00993
00994 RUN#COMMAND#
00995 START
00996 [T#R#O = .00 hrs on 0]
00997 [M#T#O#T = 2 (Imperial, 2-metric output)]
00998 [N#T#O#W = 1]
00999 [S#M#Y#N#O = 1]
01000 *****
01001 # SWMHYD / INPUT DATA FILE
01002 # *****
01003 # Project Name : [Caivan Perth properties]
01004 # Project Number: [2118]
01005 # Date : [2023 JAN 26]
01006 # Modeller : [JB]
01007 # Company : [J.F. Sabourin and Associates]
01008 # License # : 2549237
01009 *****
01010 # Model developed to simulate runoff from subcatchments under post development conditions and to size SWM ponds
01011 *****
01012 R0105-C00000-----
01013 READ STORM
01014 Filename = STORM.001
01015 Comment = 005VRSCH248R-Perth MTO IDP
01016 [S#T#I#10.0;S#D#R# 3.00;P#T#O# 53.12]
01017 *****
01018 # TAY RIVER
01019 R0105-C00010-----D#AIN-ID#HYD-----AREA#A-#PE#A#C#m#T#p#k#Date_hh:mm-----R#M#R-C-----DW#F#
01020 CALIS STANHYD 1.0 01;DEV-P1 10.49 1.884 No.date 12:02 47.59 677 .000
01021 [XMP# 56;TIMP# 66]
01022 [Horton parameters: P# 76.20;F# 13.20;DCA#4.14; F# 0.0]
01023 [Previous area: I#APE# 4.67;SLP# 2.00;LSD# 40.0;MP# 250;SCP# 0]
01024 [Impervious area: I#AIP# 1.57;SLIP# 50;L#I# 264.0;MI# 0.13;S#C# 0]
01025 R0105-C00020-----D#AIN-ID#HYD-----AREA#A-#PE#A#C#m#T#p#k#Date_hh:mm-----R#M#R-C-----DW#F#
01026 CALIS STANHYD 1.0 01;SWM1 1.77 .144 No.date 12:00 47.59 677 .000
01027 [XMP# 56;TIMP# 66]
01028 [Horton parameters: P# 76.20;F# 13.20;DCA#4.14; F# 0.0]
01029 [Previous area: I#APE# 4.67;SLP# 2.00;LSD# 40.0;MP# 250;SCP# 0]
01030 [Impervious area: I#AIP# 1.57;SLIP# 50;L#I# 95.0;MI# 0.13;S#C# 0]
01031 R0105-C00030-----D#AIN-ID#HYD-----AREA#A-#PE#A#C#m#T#p#k#Date_hh:mm-----R#M#R-C-----DW#F#
01032 CALIS STANHYD 1.0 01;OS2S 1.75 .250 No.date 12:00 47.59 677 .000
01033 R0105-C00040-----D#AIN-ID#HYD-----AREA#A-#PE#A#C#m#T#p#k#Date_hh:mm-----R#M#R-C-----DW#F#
01034 CALIS STANHYD 1.0 01;OS2S 1.75 .250 No.date 12:00 47.59 677 .000
01035 [XMP# 56;TIMP# 66]
01036 [Horton parameters: P# 76.20;F# 13.20;DCA#4.14; F# 0.0]
01037 [Previous area: I#APE# 4.67;SLP# 2.00;LSD# 40.0;MP# 250;SCP# 0]
01038 [Impervious area: I#AIP# 1.57;SLIP# 50;L#I# 95.0;MI# 0.13;S#C# 0]
01039 R0105-C00050-----D#AIN-ID#HYD-----AREA#A-#PE#A#C#m#T#p#k#Date_hh:mm-----R#M#R-C-----DW#F#
01040 ADD HYD + 1.0 02;SWM1 1.77 .144 No.date 12:00 47.59 n/a .000
01041 * 1.0 02;SWM1 1.35 .242 No.date 12:00 47.59 n/a .000
01042 * 1.0 01;Pond3-in 12.61 3.263 No.date 12:01 47.59 n/a .000
01043 R0105-C00060-----D#AIN-ID#HYD-----AREA#A-#PE#A#C#m#T#p#k#Date_hh:mm-----R#M#R-C-----DW#F#
01044 ROUTE RESERVOIR -> 1.0 02;Pond2-in 12.61 3.263 No.date 12:01 47.59 n/a .000
01045 out <= 1.0 03;Pond2-out 12.61 .331 No.date 12:31 47.58 n/a .000
01046 overflow <= 1.0 03;Pond2-Over 0.00 .000 No.date 0:00 .00 n/a .000
01047 [M#otUsed# 3745E+00 n3, TotOfVol# 0.000E+00 m3, N-Ov# 0, TotDurOfV# 0.hrs]
01048 R0105-C00070-----D#AIN-ID#HYD-----AREA#A-#PE#A#C#m#T#p#k#Date_hh:mm-----R#M#
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01081 [XIMP:56:TIMP:66]
01082 [Horton parameters: Fw= 76.20:Fpc= 13.20:DCAV4:14: F= .00]
01083 [Previous area: IApex= 4.67:SLPP=2.00:LDW= 40.0:MPD= 250:SCP= .0]
01084 [Impervious area: IApex= 1.57:SLPI= .50:LSL= 98.0:MMI= .013:ICI= .0]
01085 R015/C0011-----DRAIN-ID:INHYD-----AREAA-GPEARcm=PeakDate_hh:mm-----Rvwm-R.C-----DWPMs
01086 CALIB STANBYHD 1.0 01:00S2 1.75 .317 No.Date 12:00 47.59 677 .000
01087 [XIMP:56:TIMP:66]
01088 [Horton parameters: Fw= 76.20:Fpc= 13.20:DCAV4:14: F= .00]
01089 [Previous area: IApex= 4.67:SLPP=2.00:LDW= 40.0:MPD= 250:SCP= .0]
01090 [Impervious area: IApex= 1.57:SLPI= .50:LSL= 98.0:MMI= .013:ICI= .0]
01091 R015/C0011-----DRAIN-ID:INHYD-----AREAA-GPEARcm=PeakDate_hh:mm-----Rvwm-R.C-----DWPMs
01092 ADD HYD + 1.0 02:DEV1 1.36 .250 No.Date 12:00 47.59 n/a .000
01093 SIMM + 1.0 02:POSD2 1.36 .250 No.Date 12:00 47.59 n/a .000
01094 [Previous area: IApex= 4.67:SLPP=2.00:LDW= 40.0:MPD= 250:SCP= .0]
01095 [Impervious area: IApex= 1.57:SLPI= .50:LSL= 98.0:MMI= .013:ICI= .0]
01096 R015/C0011-----DRAIN-ID:INHYD-----AREAA-GPEARcm=PeakDate_hh:mm-----Rvwm-R.C-----DWPMs
01097 ROUTE RESERVOIR -> 1.0 02:POSD2-in 16.32 2.413 No.Date 12:01 47.59 n/a .000
01098 out <= 1.0 03:POSD2-out 16.32 .672 No.Date 12:22 47.58 n/a .000
01099 overlow <= 1.0 03:POSD2-over 0.00 .000 No.Date 0:00 .00 n/a .000
01100 [MstOfUsed= 4187E+00 m3, TotOfVol= 0.000E+00 m3, N-OfV= 0, TotDurOfV= 0 hrs]
01101 *****
01102 ** STORMS *****
01103 *****
01104 ** END OF RUN : 109 *****
01105 *****
01106 *****
01107 *****
01108 *****
01109 *****
01110 *****
01111 *****
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01441 [XIMP=.56;TIMP=.66]
01442 [Horton parameters: Fw= 76.20;Pc= 13.20;DCAY=4.14; Fw=.00]
01443 [Previous area: IArea= 4.67;SLPP=2.00;LDP= 40.;NMP=.250;SCP=.0]
01444 [Impervious area: IAlmp= 1.57;SLPI=.50;LGI= 108.;NMI=.013;SCI=.0]
01445 R0150:CO001-----Dhain-ID:IRVYD-----AREAb-QPEARcMs-TpeakDate_hh:mm-----RvM-R-C-----DWPFcms
01446 ADD HYD + 1.0 02:DEV-P2 13.21 3.554 Mo_date 12:01 75.82 n/a .000
01447 + 1.0 02:RMSL 1.36 .460 Mo_date 12:00 84.07 n/a .000
01448 + 1.0 02:OOS2 1.75 .527 Mo_date 12:00 75.81 n/a .000
01449 SIM+ 1.0 01:Pond2-In 16.32 4.464 Mo_date 12:01 75.82 n/a .000
01450 R0150:CO001-----Dhain-ID:IRVYD-----AREAb-QPEARcMs-TpeakDate_hh:mm-----RvM-R-C-----DWPFcms
01451 ROUTE RESERVOIR -> 1.0 02:Pond2-In 16.32 4.464 Mo_date 12:01 75.82 n/a .000
01452 out <= 1.0 01:Pond2-Out 16.32 1.652 Mo_date 12:13 75.80 n/a .000
01453 overflow <= 1.0 03:Pond2-Over .00 .000 Mo_date 0:00 .00 n/a .000
01454 [MsdToSeed=.5874E+00 n3, TotDvVol=.0000E+00 n3, N-Ovfl= 0, TotDurDvfl= 0.hrs]
01455 #####
01456 # STORMS
01457 #####
01458 ** END OF RUN : 198
01459
01460 -----
01461
01462
01463
01464
01465
01466 RUN:COMMANDS
01467 R0159:CO002-----Dhain-ID:IRVYD-----AREAb-QPEARcMs-TpeakDate_hh:mm-----RvM-R-C-----DWPFcms
01468 START
01469 [TZERO=.00 hrs on 0]
01470 [METOPT= 2 (1=imperial, 2=metric output)]
01471 [NETFORM= 1]
01472 [NMIN= 0.19]
01473 #####
01474 # SWMHYMO // INPUT DATA FILE
01475 #####
01476 # Project Name : [Calvin Perth properties]
01477 # Project Number : [2118]
01478 # Date : [2023 JAN 26]
01479 # Modeler : [JFS]
01480 # Company : [J.F. Sabourin and Associates]
01481 # License # : [2549237]
01482 #####
01483 # Model developed to simulate runoff from subcatchments under post development conditions and to size SWM ponds
01484 #####
01485 R0159:CO002-----Dhain-ID:IRVYD-----AREAb-QPEARcMs-TpeakDate_hh:mm-----RvM-R-C-----DWPFcms
01486 READ STORM
01487 File name = STORM.001
01488 Comment = 100YRSC24HR-Perth MTD IDF
01489 [IDF=10.00;IDDR= 24.00;IDDT= 117.60]
01490 #####
01491 # TAY RIVER
01492 #####
01493 R0159:CO003-----Dhain-ID:IRVYD-----AREAb-QPEARcMs-TpeakDate_hh:mm-----RvM-R-C-----DWPFcms
01494 CALIB STANDHYD 1.0 01:DEV-P1 10.49 3.184 Mo_date 12:01 84.07 .715 .000
01495 [XIMP=.56;TIMP=.66]
01496 [Horton parameters: Fw= 76.20;Pc= 13.20;DCAY=4.14; Fw=.00]
01497 [Previous area: IArea= 4.67;SLPP=2.00;LDP= 40.;NMP=.250;SCP=.0]
01498 [Impervious area: IAlmp= 1.57;SLPI=.50;LGI= 264.;NMI=.013;SCI=.0]
01499 R0159:CO004-----Dhain-ID:IRVYD-----AREAb-QPEARcMs-TpeakDate_hh:mm-----RvM-R-C-----DWPFcms
01500 CALIB STANDHYD 1.0 01:RMSL 10.49 3.184 Mo_date 12:01 84.07 .715 .000
01501 [XIMP=.56;TIMP=.66]
01502 [Horton parameters: Fw= 76.20;Pc= 13.20;DCAY=4.14; Fw=.00]
01503 [Previous area: IArea= 4.67;SLPP=2.00;LDP= 40.;NMP=.250;SCP=.0]
01504 [Impervious area: IAlmp= 1.57;SLPI=.50;LGI= 71.;NMI=.013;SCI=.0]
01505 R0159:CO005-----Dhain-ID:IRVYD-----AREAb-QPEARcMs-TpeakDate_hh:mm-----RvM-R-C-----DWPFcms
01506 CALIB STANDHYD 1.0 01:OOS1 10.49 3.184 Mo_date 12:01 84.07 .715 .000
01507 [XIMP=.56;TIMP=.66]
01508 [Horton parameters: Fw= 76.20;Pc= 13.20;DCAY=4.14; Fw=.00]
01509 [Previous area: IArea= 4.67;SLPP=2.00;LDP= 40.;NMP=.250;SCP=.0]
01510 [Impervious area: IAlmp= 1.57;SLPI=.50;LGI= 95.;NMI=.013;SCI=.0]
01511 R0159:CO006-----Dhain-ID:IRVYD-----AREAb-QPEARcMs-TpeakDate_hh:mm-----RvM-R-C-----DWPFcms
01512 ADD HYD + 1.0 02:DEV-P1 10.49 3.184 Mo_date 12:01 84.06 n/a .000
01513 + 1.0 02:RMSL 1.36 .460 Mo_date 12:00 84.07 n/a .000
01514 + 1.0 02:OOS1 1.75 .527 Mo_date 12:00 75.81 n/a .000
01515 SIM+ 1.0 01:Pond1-In 12.61 3.672 Mo_date 12:01 84.07 n/a .000
01516 R0159:CO007-----Dhain-ID:IRVYD-----AREAb-QPEARcMs-TpeakDate_hh:mm-----RvM-R-C-----DWPFcms
01517 ROUTE RESERVOIR -> 1.0 01:Pond1-In 12.61 3.672 Mo_date 12:01 84.07 n/a .000
01518 out <= 1.0 01:Pond1-Out 12.61 .795 Mo_date 12:22 84.05 n/a .000
01519 overflow <= 1.0 03:Pond1-Over .00 .000 Mo_date 0:00 .00 n/a .000
01520 [MsdToSeed=.601E+00 n3, TotDvVol=.0000E+00 n3, N-Ovfl= 0, TotDurDvfl= 0.hrs]
01521 R0159:CO008-----Dhain-ID:IRVYD-----AREAb-QPEARcMs-TpeakDate_hh:mm-----RvM-R-C-----DWPFcms
01522 CALIB STANDHYD 1.0 01:DEV-P3 14.48 4.320 Mo_date 12:01 84.07 .715 .000
01523 [XIMP=.56;TIMP=.66]
01524 [Horton parameters: Fw= 76.20;Pc= 13.20;DCAY=4.14; Fw=.00]
01525 [Previous area: IArea= 4.67;SLPP=2.00;LDP= 40.;NMP=.250;SCP=.0]
01526 [Impervious area: IAlmp= 1.57;SLPI=.50;LGI= 311.;NMI=.013;SCI=.0]
01527 R0159:CO009-----Dhain-ID:IRVYD-----AREAb-QPEARcMs-TpeakDate_hh:mm-----RvM-R-C-----DWPFcms
01528 CALIB STANDHYD 1.0 01:RMSL 14.48 4.320 Mo_date 12:00 84.07 .715 .000
01529 [XIMP=.56;TIMP=.66]
01530 [Horton parameters: Fw= 76.20;Pc= 13.20;DCAY=4.14; Fw=.00]
01531 [Previous area: IArea= 4.67;SLPP=2.00;LDP= 40.;NMP=.250;SCP=.0]
01532 [Impervious area: IAlmp= 1.57;SLPI=.50;LGI= 95.;NMI=.013;SCI=.0]
01533 R0159:CO010-----Dhain-ID:IRVYD-----AREAb-QPEARcMs-TpeakDate_hh:mm-----RvM-R-C-----DWPFcms
01534 ADD HYD + 1.0 02:DEV-P3 14.48 4.320 Mo_date 12:01 84.07 n/a .000
01535 + 1.0 02:RMSL 1.36 .460 Mo_date 12:00 84.06 n/a .000
01536 + 1.0 02:OOS2 1.75 .527 Mo_date 12:00 75.81 n/a .000
01537 SIM+ 1.0 01:Pond3-In 15.93 4.797 Mo_date 12:01 84.07 n/a .000
01538 R0159:CO011-----Dhain-ID:IRVYD-----AREAb-QPEARcMs-TpeakDate_hh:mm-----RvM-R-C-----DWPFcms
01539 ROUTE RESERVOIR -> 1.0 02:Pond3-In 15.93 4.797 Mo_date 12:01 84.07 n/a .000
01540 out <= 1.0 01:Pond3-Out 15.93 1.005 Mo_date 12:23 84.06 n/a .000
01541 overflow <= 1.0 03:Pond3-Over .00 .000 Mo_date 0:00 .00 n/a .000
01542 [MsdToSeed=.7610E+00 n3, TotDvVol=.0000E+00 n3, N-Ovfl= 0, TotDurDvfl= 0.hrs]
01543 #####
01543 # GRANTS CREEK
01544 #####
01545 R0159:CO012-----Dhain-ID:IRVYD-----AREAb-QPEARcMs-TpeakDate_hh:mm-----RvM-R-C-----DWPFcms
01546 CALIB STANDHYD 1.0 01:DEV-P2 13.21 3.562 Mo_date 12:01 84.07 .715 .000
01547 [XIMP=.56;TIMP=.66]
01548 [Horton parameters: Fw= 76.20;Pc= 13.20;DCAY=4.14; Fw=.00]
01549 [Previous area: IArea= 4.67;SLPP=2.00;LDP= 40.;NMP=.250;SCP=.0]
01550 [Impervious area: IAlmp= 1.57;SLPI=.50;LGI= 297.;NMI=.013;SCI=.0]
01551 R0159:CO013-----Dhain-ID:IRVYD-----AREAb-QPEARcMs-TpeakDate_hh:mm-----RvM-R-C-----DWPFcms
01552 CALIB STANDHYD 1.0 01:RMSL 13.21 3.562 Mo_date 12:00 84.07 .715 .000
01553 [XIMP=.56;TIMP=.66]
01554 [Horton parameters: Fw= 76.20;Pc= 13.20;DCAY=4.14; Fw=.00]
01555 [Previous area: IArea= 4.67;SLPP=2.00;LDP= 40.;NMP=.250;SCP=.0]
01556 [Impervious area: IAlmp= 1.57;SLPI=.50;LGI= 95.;NMI=.013;SCI=.0]
01557 R0159:CO014-----Dhain-ID:IRVYD-----AREAb-QPEARcMs-TpeakDate_hh:mm-----RvM-R-C-----DWPFcms
01558 CALIB STANDHYD 1.0 01:OOS2 1.75 .586 Mo_date 12:00 84.07 .715 .000
01559 [XIMP=.56;TIMP=.66]
01560 [Horton parameters: Fw= 76.20;Pc= 13.20;DCAY=4.14; Fw=.00]
01561 [Previous area: IArea= 4.67;SLPP=2.00;LDP= 40.;NMP=.250;SCP=.0]
01562 [Impervious area: IAlmp= 1.57;SLPI=.50;LGI= 108.;NMI=.013;SCI=.0]
01563 R0159:CO015-----Dhain-ID:IRVYD-----AREAb-QPEARcMs-TpeakDate_hh:mm-----RvM-R-C-----DWPFcms
01564 ADD HYD + 1.0 02:DEV-P2 13.21 3.562 Mo_date 12:01 84.07 n/a .000
01565 + 1.0 02:RMSL 1.36 .460 Mo_date 12:00 84.07 n/a .000
01566 + 1.0 02:OOS2 1.75 .586 Mo_date 12:00 84.07 n/a .000
01567 SIM+ 1.0 01:Pond2-In 16.32 4.975 Mo_date 12:01 84.07 n/a .000
01568 R0159:CO016-----Dhain-ID:IRVYD-----AREAb-QPEARcMs-TpeakDate_hh:mm-----RvM-R-C-----DWPFcms
01569 ROUTE RESERVOIR -> 1.0 02:Pond2-In 16.32 4.975 Mo_date 12:01 84.07 n/a .000
01570 out <= 1.0 01:Pond2-Out 16.32 1.930 Mo_date 12:13 84.06 n/a .000
01571 overflow <= 1.0 03:Pond2-Over .00 .000 Mo_date 0:00 .00 n/a .000
01572 [MsdToSeed=.643E+00 n3, TotDvVol=.0000E+00 n3, N-Ovfl= 0, TotDurDvfl= 0.hrs]
01573 #####
01573 # STORMS
01574 #####
01575 #####
01576 R0159:CO002-----Dhain-ID:IRVYD-----AREAb-QPEARcMs-TpeakDate_hh:mm-----RvM-R-C-----DWPFcms
01577 FINISH
01578
01579
01580 WARNINGS / ERRORS / NOTES
01581
01582 Simulation ended on 2023-02-16 at 15:31:37
01583
01584

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